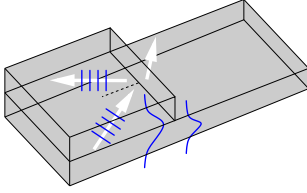


Reflection of semi-guided plane waves at angled thin-film transitions

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1 2-D optics

Classical concepts [1, 2] for integrated optical components like lenses [3, 4], mirrors [5], prisms [6], but also for complex lens-systems [7], or entire spectrometers [8, 9], rely on the effects that a — tapered or step-like — transition between regions with different layering, specifically different core thickness, has on thin-film guided, in-plane unguided light. Results for the reflection and refraction of 1-D guided plane waves at such a discontinuity may form the basis for a description of the in-plane propagation by geometrical optics [1, 2, 8].



Aim: As a step beyond the classical effective index picture, we will discuss and compare two approaches on how this problem can be tackled — at least partly — by state-of-the-art tools for integrated optics design.

- Accepting the scalar approximation, using an ansatz of a uniform harmonic field dependence on the interface coordinate, the 3-D problem reduces to a 2-D Helmholtz problem, for guided wave input and transparent boundaries, where the permittivity depends on the incidence angle.
- One complements the structure with a mirrored interface, such that the 2-D cross section of a wide multimode rib channel emerges. Constraints for transverse resonance permit to translate the propagation constants of its polarized modes into discrete samples of the phase changes experienced by an in-plane guided wave upon total internal reflection at the sidewalls.

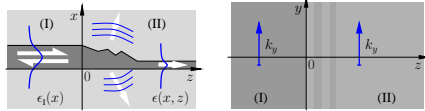
2 Formal problem

- Homogeneous Maxwell equations, frequency domain, linear dielectric media,

$$\text{curl } \vec{E} = -i\omega\mu_0\vec{H}, \quad \text{curl } \vec{H} = i\omega\epsilon_0\vec{E}$$

for electric and magnetic fields \vec{E}, \vec{H} , oscillating $\sim \exp(i\omega t)$ in time with frequency $\omega = kc = 2\pi c/\lambda$, for vacuum wavenumber k , wavelength λ , speed of light c , permittivity ϵ_0 , and permeability μ_0 .

- Relative permittivity $\epsilon = n^2$:



- $\partial_x \epsilon = 0$ everywhere

$$\vec{E} = \begin{pmatrix} \vec{E} \\ \vec{H} \end{pmatrix} (x, y, z) = \begin{pmatrix} \vec{E} \\ \vec{H} \end{pmatrix} (x, z) e^{-ik_y y},$$

k_y : a given parameter (\leftrightarrow incidence angle).

- The components of \vec{E}, \vec{H} satisfy the equations:

$$\left(\partial_x^2 - \partial_x \epsilon + \partial_z^2 - \partial_x \frac{1}{\epsilon} \partial_x \epsilon - \partial_z \partial_x \right) \begin{pmatrix} E_x \\ E_z \end{pmatrix} + (k^2 \epsilon - k_y^2) \begin{pmatrix} E_x \\ E_z \end{pmatrix} = 0,$$

or

$$\left(\partial_x^2 + \partial_z^2 - \partial_x \frac{1}{\epsilon} \partial_x \epsilon - \partial_z \partial_x \frac{1}{\epsilon} \partial_x \epsilon \right) \begin{pmatrix} H_x \\ H_z \end{pmatrix} + (k^2 \epsilon - k_y^2) \begin{pmatrix} H_x \\ H_z \end{pmatrix} = 0,$$

& equivalent variants, formally identical to the vectorial equations for guided modes.

- Region I: $\partial_x \epsilon = 0$ & $\partial_z \epsilon = 0$

separable planar solutions with principal components of the form

$$E(x, z) = \Psi_{TE}(x) e^{-i\beta_{TE} z}, \quad \partial_x^2 \Psi_{TE} + (k^2 \epsilon_1 - \beta_{TE}^2) \Psi_{TE} = 0 \quad (\text{TE})$$

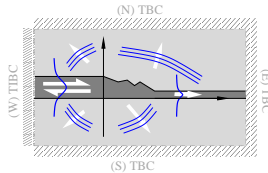
$$H(x, z) = \Psi_{TM}(x) e^{-i\beta_{TM} z}, \quad \partial_x \partial_x \frac{1}{\epsilon} \Psi_{TM} + (k^2 \epsilon_1 - \beta_{TM}^2) \Psi_{TM} = 0, \quad (\text{TM})$$

& other components (vectorial fields),
& rotated fields, in-plane propagation under arbitrary angles.

\leftrightarrow Specification of incident waves.

- Effective 2-D problem, vectorial, "effective permittivity" dependent on k_y .

- Boundary Conditions (T)DBC's:

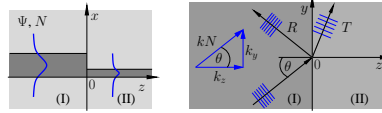


(W): Influx of polarized plane guided wave, rotated for given angle of incidence & Transparency for reflected outgoing guided and nonguided waves.

(N, E, S): Transparency for outgoing guided and nonguided waves.

Existing solver ?

3 Scalar theory



- Neglect of polarization effects from permittivity gradients / interfaces

\leftrightarrow scalar Helmholtz equation

$$(\partial_x^2 + \partial_z^2 + \partial_y^2) \vec{E} + k^2 \epsilon \vec{E} = 0.$$

- $\partial_y \epsilon = 0 \leftrightarrow \vec{E}(x, y, z) = E(x, z) e^{-ik_y y}$.

- Region I, $z < 0$: incoming guided wave, incidence angle θ ,

$$\vec{E}_{in}(x, y, z) = \Psi(x) e^{-ikN(\sin \theta y + \cos \theta z)}, \quad \partial_x^2 \Psi + k^2 (\epsilon_1 - N^2) \Psi = 0.$$

\leftrightarrow Choose $k_y = kN \sin \theta$.

- Effective 2-D problem:

$$(\partial_x^2 + \partial_z^2) E + k^2 \epsilon_{eff} E = 0, \quad \text{with } \epsilon_{eff}(x, z) = \epsilon(x, z) - N^2 \sin^2 \theta.$$

- Solution: Quasi-analytic 2-D QUEP solver [10], TE, staircase approximation; result: guided wave reflectance R and transmittance T .

- Field in region I:

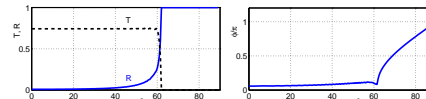
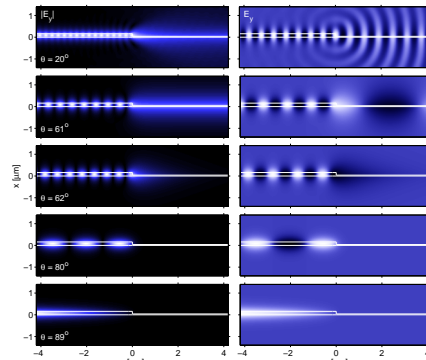
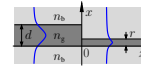
$$\vec{E}(x, y, z) = \left\{ \Psi(x) \left(e^{-ikN \cos \theta z} + \rho e^{ikN \cos \theta z} \right) + \chi(x, z) \right\} e^{-ikN \sin \theta y},$$

χ a remainder, $\chi \perp \Psi$,

reflection coefficient $\rho = \rho_0 e^{i\phi}$, $R = \rho_0^2$, phase change upon reflection ϕ .

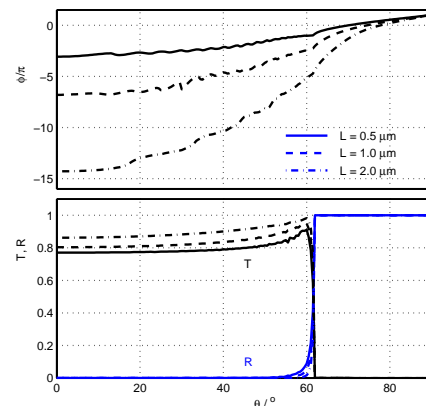
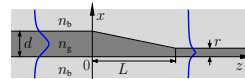
4 Step discontinuity

$n_g = 2.0081$, $n_b = 1.4524$,
 $d = 160$ nm, $r = 40$ nm, $\lambda = 850$ nm.

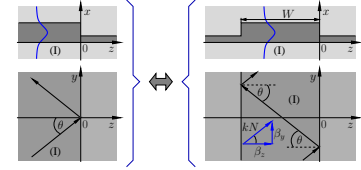


5 Tapered transition

$n_g = 2.0081$, $n_b = 1.4524$,
 $d = 160$ nm, $r = 40$ nm,
 $\lambda = 850$ nm.



6 Transverse resonance



- Extend the structure by a mirrored interface, with some arbitrary width W

\leftrightarrow 2-D cross section of a channel waveguide.

- Available: Guided modes of that channel, of vertical (x) fundamental order; set of mode indices m and propagation constants β_m , TE / QTE polarization.

- In the core region $-W < z < 0$, with $\epsilon(x, z) = \epsilon_1(x)$, the equation

$$(\partial_x^2 + \partial_z^2) E + (k^2 \epsilon_1 - \beta_m^2) E = 0.$$

holds for the principal electric component E of the mode profile.

- Assumption: Separable $E(x, z) = \Psi(x) \zeta(z)$, at least approximately, in region I;

Ψ : 1-D TE mode of the central slab, $\partial_x^2 \Psi + k^2 (\epsilon_1 - N^2) \Psi = 0$.

ζ : $\partial_z^2 \zeta + (k^2 N^2 - \beta_m^2) \zeta = 0$, $\zeta(z) = \zeta_0 e^{\pm i\beta_m z}$, $\beta_m^2 = k^2 N^2 - \beta_g^2$.

1-D slab mode problem for the lateral shape ζ .

- Associated mode angle θ given by $\sin \theta = \beta_m / (kN)$

θ : sample value for an angle of incidence on the channel sidewalls.

- Lateral wave propagation with constant $\beta_m = kN \cos \theta$,

m : Lateral order of the 2-D profile E & mode index of ζ .

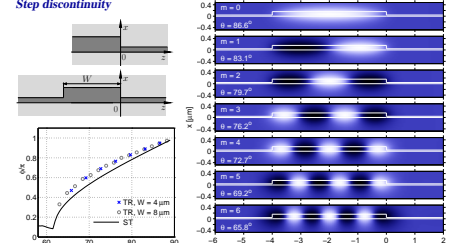
- Transverse resonance condition associated with the profile for ζ :

$$-m 2\pi = -W \beta_m + \phi - W \beta_m + \phi, \quad \text{or } \phi = -m\pi + W k N \cos \theta.$$

\leftrightarrow Estimate for the phase change ϕ upon reflection under incidence angle θ .

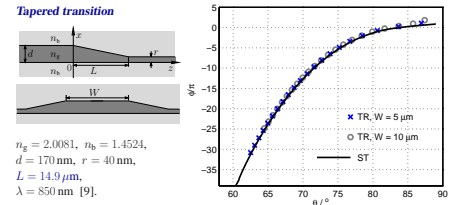
Guided 3-D modes \leftrightarrow Total internal reflection at the sidewalls only.

Step discontinuity



TR: transverse resonance, WMM solver, QTE [11]; ST: scalar theory.

Tapered transition



$n_g = 2.0081$, $n_b = 1.4524$,
 $d = 170$ nm, $r = 40$ nm,
 $L = 14.9$ μm ,
 $\lambda = 850$ nm [9].

TR: transverse resonance, Phoenix solver [12]; ST: scalar theory.

7 Acknowledgements

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8 References

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