

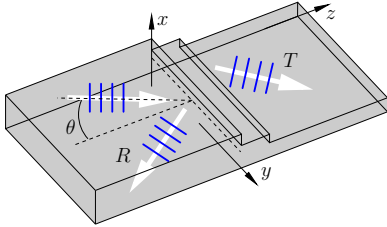
Oblique quasi-lossless excitation of a thin silicon slab waveguide

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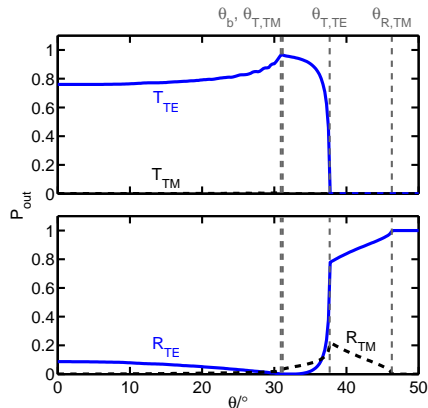
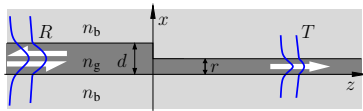
1 A guided-wave-variant of an anti-reflection coating

Guided waves traversing an abrupt interface between different slab waveguides typically generate pronounced reflections and scattering losses. The conventional 2-D framework corresponds to normal incidence of the laterally infinite waves on the interface. Applying a semi-analytical vectorial mode expansion solver [1, 2] for the effective 2-D problems, we investigate, for high-contrast silicon slabs, what happens when the waves come in at oblique angles. Arguments based on a variant of Snell's law, adapted to the present case of polarized semi-guided waves, predict critical angles of incidence, beyond which all scattering losses are suppressed. In that regime, for our particular parameters with TE-incidence, the transmittance is already raised to about 95%. The waves, however, are still partly reflected, mainly into the backwards TM mode.



Motivated by the traditional technique of reflection suppression, we introduce a short waveguide segment of intermediate thickness at the former interface. Optimization of the transmittance through varying the height and width of that segment leads to a configuration with a guided-wave TE-to-TE transmittance above 99.5%. Rigorous finite-element simulations (COMSOL, [3]) confirm these findings.

2 Abrupt junction, transmittance

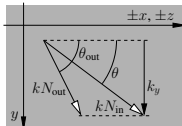


3 Parameters

refractive index, cladding: $n_b = 1.45$,
 refractive index, cores: $n_g = 3.45$,
 larger core thickness: $d = 0.22 \mu\text{m}$,
 lower core thickness: $r = 0.05 \mu\text{m}$,
 vacuum wavelength: $\lambda = 1.55 \mu\text{m}$,
 excitation: TE_0 ,
 angle of incidence: θ ,
 thickness, coating segment: $h = 0.16 \mu\text{m}^*$,
 width, coating segment: $w = 0.40 \mu\text{m}^*$,
 critical angles:
 $\theta_b = 30.9^\circ$,
 $\theta_{T, \text{TM}} = 31.2^\circ$,
 $\theta_{T, \text{TE}} = 37.7^\circ$,
 $\theta_{R, \text{TM}} = 46.3^\circ$.

* optimized for $\theta = 33^\circ$.

4 Critical angles



Uniform $k_y = k N_{\text{in}} \sin \theta$,
 related to incoming mode (N_{in})
 & incidence angle θ :

Outgoing modes (N_{out}) leave at angles θ_{out} with $k_y = k N_{\text{out}} \sin \theta_{\text{out}}$,
 different for every outgoing mode;
 generalized Snell's law: $N_{\text{out}} \sin \theta_{\text{out}} = N_{\text{in}} \sin \theta$,

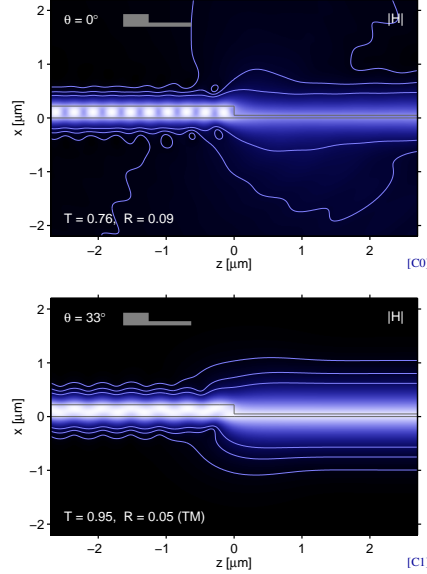
applicable to all (reflected, transmitted, up- or downwards scattered) outgoing propagating modes.

Outgoing modes with $N_{\text{out}} \leq N_{\text{crit}}$ become evanescent for incidence angles $\theta \geq \theta_{\text{crit}}$ with $\sin \theta_{\text{crit}} = N_{\text{crit}}/N_{\text{in}}$, i.e. these modes do not carry power away.

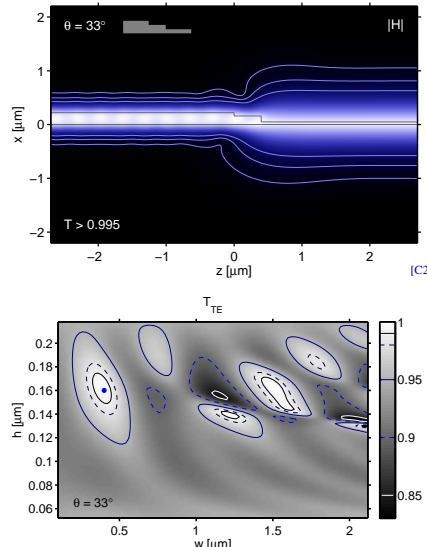
Relevant values for the present examples:

- $\sin \theta_b = n_b/N_{\text{TE}_0}$, no forward/backward power loss into the cladding for $\theta \geq \theta_b$,
- $\sin \theta_{T, \text{TM}} = N_{\text{TM}_0}/N_{\text{TE}_0}$, no power transmitted to the TM_0 mode for $\theta \geq \theta_{T, \text{TM}}$,
- $\sin \theta_{T, \text{TE}} = N_{\text{TE}_0}/N_{\text{TE}_0}$, no power transmitted to the TE_0 mode for $\theta \geq \theta_{T, \text{TE}}$,
- $\sin \theta_{R, \text{TM}} = N_{\text{TM}_0}/N_{\text{TE}_0}$, no power reflected into the TM_0 mode for $\theta \geq \theta_{R, \text{TM}}$.

5 Abrupt junction, fields



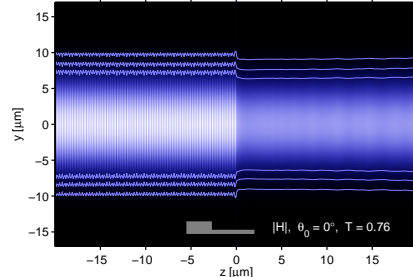
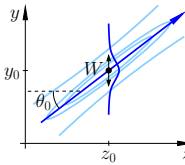
6 Anti-reflection coating



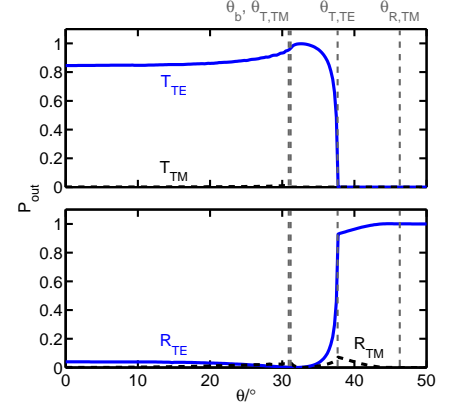
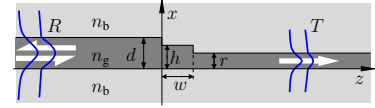
7 Semi-guided wave packets

Superimpose the former 2-D solutions for a range of k_x -values / a range of angles θ , such that the input field resembles a vertically (x) guided, laterally (y, z) localized Gaussian beam.

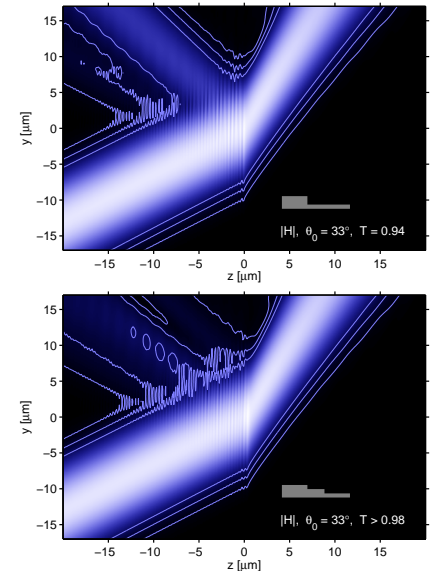
Parameters:
 focus (y_0, z_0) at the origin,
 primary angle θ_0 ,
 full 1/e-width along y , at focus:
 $W = 10 \mu\text{m}$.



8 Coated junction, transmittance



9 Propagation of semi-guided Gaussian beams



10 Numerical benchmark

	T _{TE}	R _{TE}	T _{TM}	R _{TM}	
[C0] $\theta = 0^\circ$, bare	0.760	0.087	0	0	vQUEP [1] COMSOL [3]
[C1] $\theta = 33^\circ$, bare	0.945	0.001	0	0.053	vQUEP [1] COMSOL [3]
[C2] $\theta = 33^\circ$, coated	0.996	0.003	0	0.001	vQUEP [1] COMSOL [3]

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Acknowledgements

Support by the Deutsche Forschungsgemeinschaft (DFG, Transregional Collaborative Research Center TRR 142, and project HA7314/1) is gratefully acknowledged.

