Resonant evanescent excitation of OAM modes in a high-contrast circular step-index fiber

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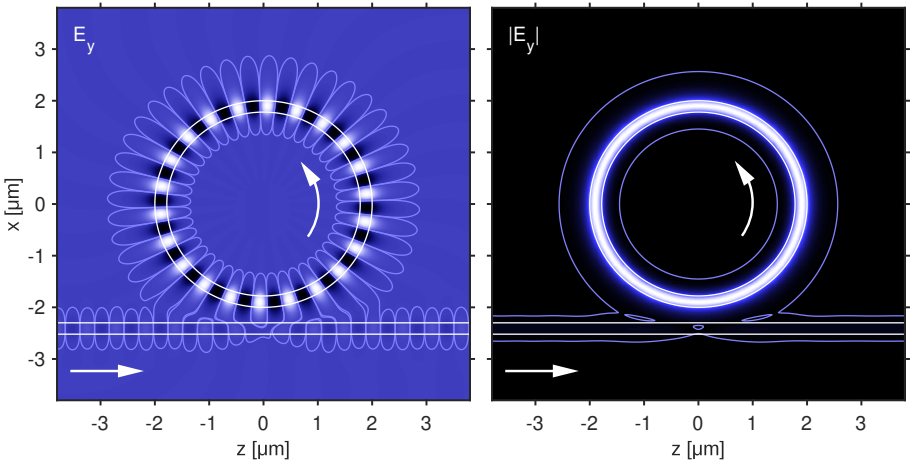
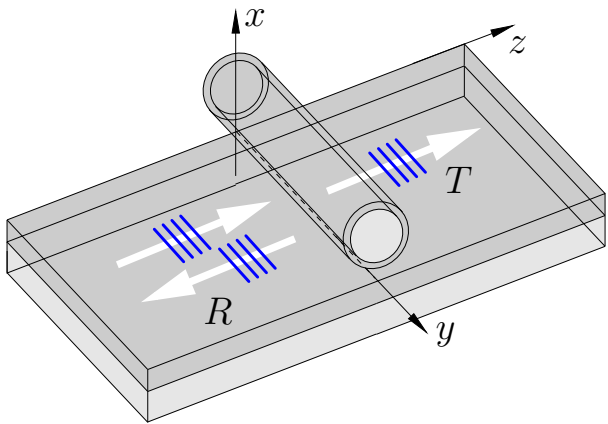
A circular integrated optical microresonator

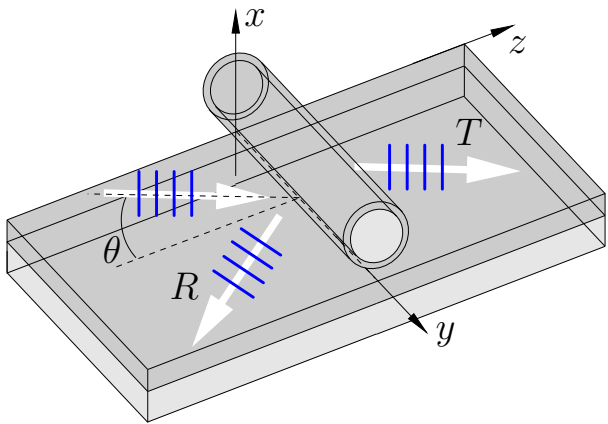


2-D, radius 2 μm, core thickness 0.22 μm, gap 0.3 μm, refractive indices 3.45 : 1.45, wavelength 1.531 μm, in: TE_0.

(2-D) $\partial_y \epsilon = 0,\ \partial_y(\boldsymbol{E}, \boldsymbol{H}) = 0$

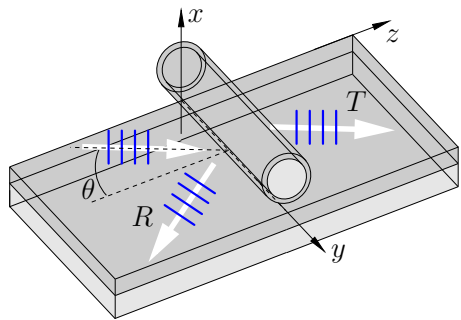


(2.5-D) $\partial_y \epsilon = 0,\ (\boldsymbol{E}, \boldsymbol{H}) \sim \exp(-\mathrm{i} k_y y),\ k_y \sim \sin\theta$

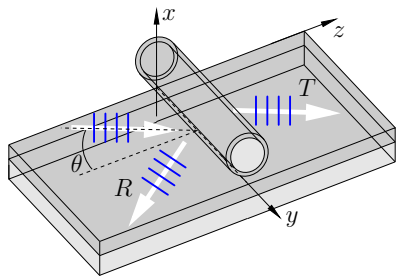


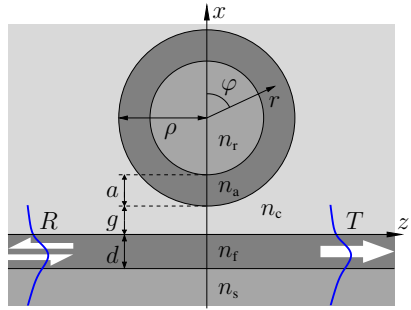
Overview

- Oblique incidence of semi-guided waves
- Fiber resonator, HCMT model
- OAM modes of the fiber
- Resonance properties
- Bundles of semi-guided waves



High-contrast slab & fiber

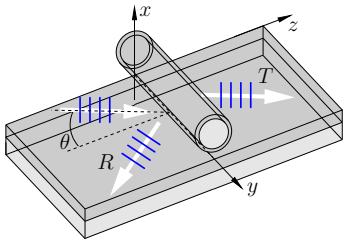


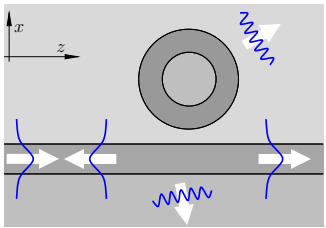


$n_s = 1.45,\ n_f = 3.45,\ n_c = 1.0,\ d = 0.22\,\mu m;\quad n_r = 1.45,\ n_a = 3.45,\ a = 0.22\,\mu m,\ \rho = 2\,\mu m;\quad$ variable g.

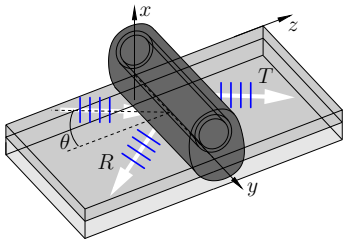
TE- / TM-excitation at $\lambda = 1.55\,\mu m$, varying θ.

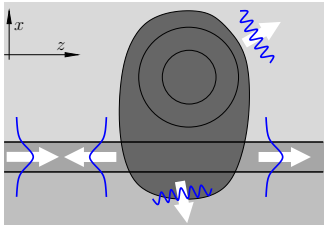
Semi guided waves at oblique angles of incidence



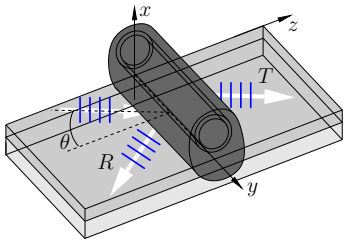


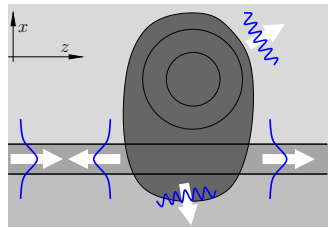
Semi guided waves at oblique angles of incidence

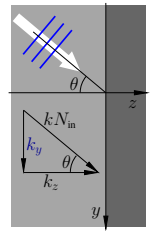




Semi guided waves at oblique angles of incidence





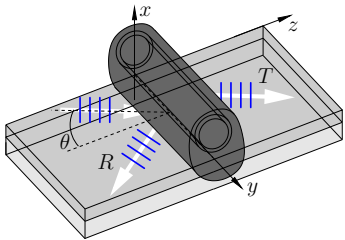


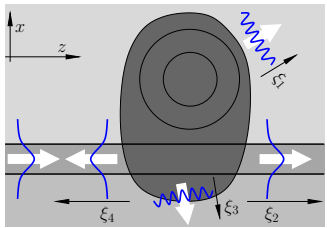
$$\sim \mathrm{e}^{\mathrm{i}\omega t},\ \omega = k\mathrm{c} = 2\pi\mathrm{c}/\lambda$$

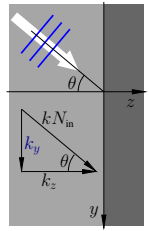
- Incoming slab mode $\{N_{\text{in}}; \boldsymbol{\Psi}_{\text{in}}\}$, $(\boldsymbol{E}, \boldsymbol{H}) \sim \boldsymbol{\Psi}_{\text{in}}(x)\,\mathrm{e}^{-\mathrm{i}(k_y y + k_z z)}$,
  incidence angle θ, $k^2 N_{\text{in}}^2 = k_y^2 + k_z^2$, $k_y = kN_{\text{in}}\sin\theta$.

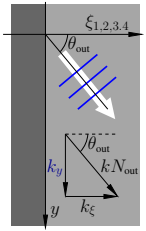
- y-homogeneous problem: $(\boldsymbol{E}, \boldsymbol{H}) \sim \mathrm{e}^{-\mathrm{i}k_y y}$ everywhere.

Semi guided waves at oblique angles of incidence









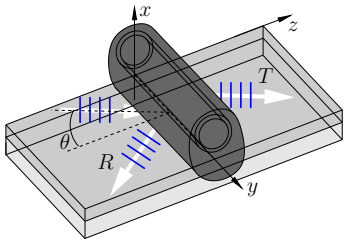
- Outgoing wave $\{N_{\text{out}}; \boldsymbol{\Psi}_{\text{out}}\}$, $(\boldsymbol{E}, \boldsymbol{H}) \sim \boldsymbol{\Psi}_{\text{out}}(\,.\,)\,\mathrm{e}^{-\mathrm{i}(k_y y + k_\xi \xi)}$,

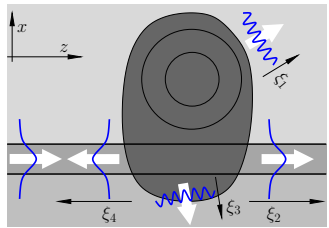
  $$k^2 N_{\text{out}}^2 = k_y^2 + k_\xi^2, \quad k_y = k N_{\text{in}} \sin\theta.$$

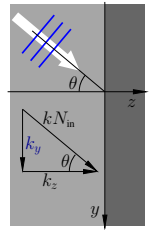
- $k^2 N_{\text{out}}^2 > k_y^2$: $k_\xi = k N_{\text{out}} \cos\theta_{\text{out}}$, wave propagating at angle θ_{out},

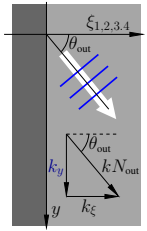
  $N_{\text{out}} \sin\theta_{\text{out}} = N_{\text{in}} \sin\theta$.

Semi guided waves at oblique angles of incidence









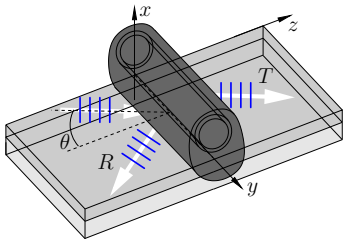
- Outgoing wave $\{N_{\text{out}}; \boldsymbol{\Psi}_{\text{out}}\}$, $(\boldsymbol{E}, \boldsymbol{H}) \sim \boldsymbol{\Psi}_{\text{out}}(\,.\,)\,\mathrm{e}^{-\mathrm{i}(k_y y + k_\xi \xi)}$,

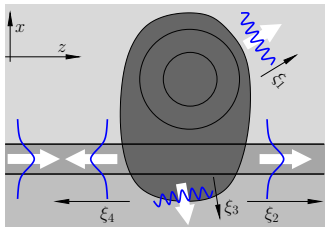
  $$k^2 N_{\text{out}}^2 = k_y^2 + k_\xi^2, \quad k_y = k N_{\text{in}} \sin\theta.$$

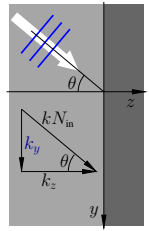
- $k^2 N_{\text{out}}^2 < k_y^2$: $\quad k_\xi = -\mathrm{i}\sqrt{k_y^2 - k^2 N_{\text{out}}^2}$, ξ-evanescent wave,

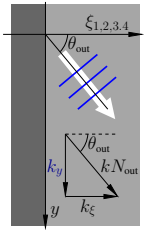
  the outgoing wave does not carry optical power.

Semi guided waves at oblique angles of incidence







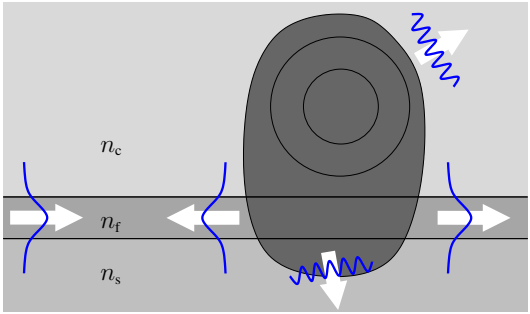


- Outgoing wave $\{N_{\text{out}}; \boldsymbol{\Psi}_{\text{out}}\}$, $(\boldsymbol{E}, \boldsymbol{H}) \sim \boldsymbol{\Psi}_{\text{out}}(\,.\,)\,\mathrm{e}^{-\mathrm{i}(k_y y + k_\xi \xi)}$,

  $$k^2 N_{\text{out}}^2 = k_y^2 + k_\xi^2, \quad k_y = k N_{\text{in}} \sin\theta.$$

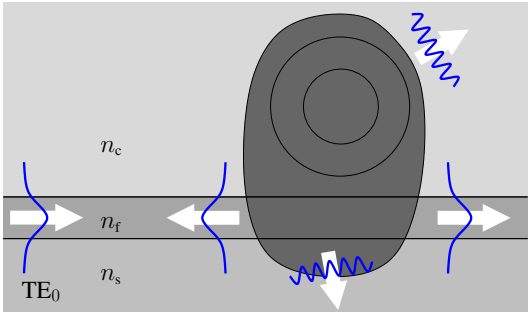
- Scan over θ:
  change from ξ-propagating to ξ-evanescent if $k^2 N_{\text{out}}^2 = k^2 N_{\text{in}}^2 \sin^2\theta$
  ⇝ mode $\{N_{\text{out}}; \boldsymbol{\Psi}_{\text{out}}\}$ does not carry power for $\theta > \theta_{\text{cr}}$,
  critical angle θ_{cr}, $\sin\theta_{\text{cr}} = N_{\text{out}}/N_{\text{in}}$.

Critical angles



$n_f > n_s > n_c$,
single mode slabs, $N_{TE} > N_{TM} > n_s$.

Critical angles

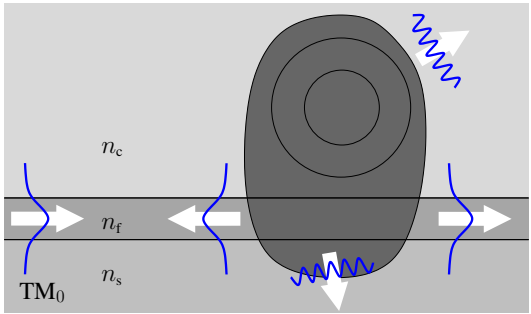


$n_f > n_s > n_c$,
single mode slabs, $N_{TE} > N_{TM} > n_s$,
in: TE_0.

- Propagation in the substrate and cladding relates to effective indices $N_{out} \leq n_s$
  $\rightsquigarrow$ $R_{TE} + R_{TM} + T_{TE} + T_{TM} = 1$ for $\theta > \theta_s$, $\sin\theta_s = n_s/N_{TE}$.

- TM polarized waves relate to effective mode indices $N_{out} \leq N_{TM}$
  $\rightsquigarrow$ $R_{TM} = T_{TM} = 0$, $R_{TE} + T_{TE} = 1$ for $\theta > \theta_{TM}$, $\sin\theta_{TM} = N_{TM}/N_{TE}$.

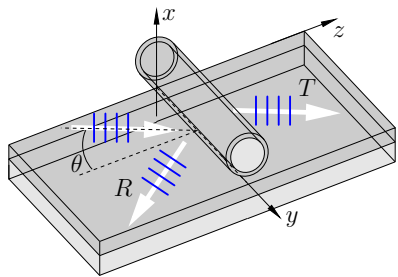
Critical angles

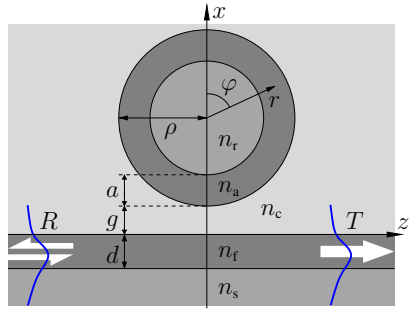


$n_f > n_s > n_c$,
single mode slabs, $N_{TE} > N_{TM} > n_s$,
in: TM_0.

- Propagation in the substrate and cladding relates to effective indices $N_{out} \leq n_s$
  $\rightsquigarrow$ $R_{TE} + R_{TM} + T_{TE} + T_{TM} = 1$ for $\theta > \theta_s$, $\sin\theta_s = n_s/N_{TM}$.

High-contrast slab & fiber

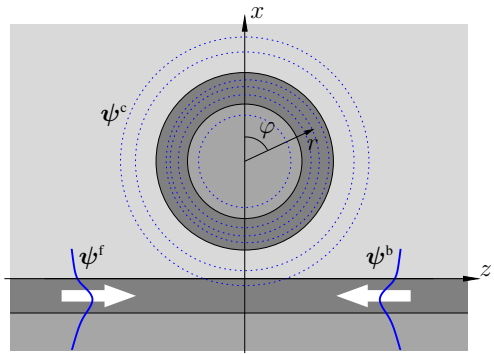




$n_s = 1.45,\ n_f = 3.45,\ n_c = 1.0,\ d = 0.22\,\mu\text{m};\quad n_r = 1.45,\ n_a = 3.45,\ a = 0.22\,\mu\text{m},\ \rho = 2\,\mu\text{m};\quad$ variable g.
TE- / TM-excitation at $\lambda = 1.55\,\mu\text{m}$, varying θ.

TE input: $\theta_c = 20.88°,\ \theta_s = 31.13°,\ \theta_{TM} = 41.94°;\quad$ TM input: $\theta_c = 32.24°,\ \theta_s = 50.66°$.

Simulations: Hybrid coupled mode theory



- θ, k_y given, $\boldsymbol{E}, \boldsymbol{H} \sim \exp(-\mathrm{i} k_y y)$,
- Slab waveguide:

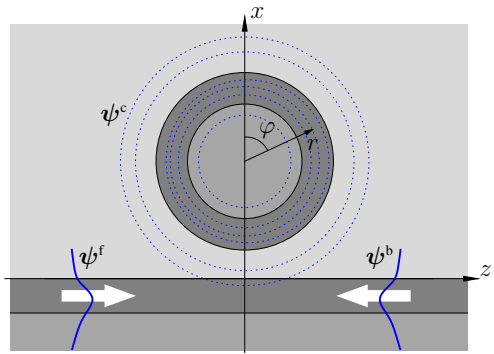
$$\boldsymbol{\psi}_p^{\mathrm{f,b}}(x,z) = \begin{pmatrix} \tilde{\boldsymbol{E}} \\ \tilde{\boldsymbol{H}} \end{pmatrix}_p^{\mathrm{f,b}} (k_y, x)\ \mathrm{e}^{\mp \mathrm{i}\, k_z^p(k_y)\, z}, \qquad p \in \{\mathrm{TE}, \mathrm{TM}\}.$$

- Fiber:

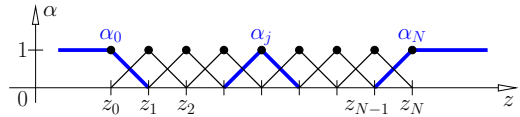
$$\boldsymbol{\psi}_j^{\mathrm{c}}(r,\varphi) = \begin{pmatrix} \tilde{\boldsymbol{E}} \\ \tilde{\boldsymbol{H}} \end{pmatrix}_j^{\mathrm{c}} (r)\, \mathrm{e}^{-\mathrm{i} l_j \varphi}, \qquad l_j \in \mathbb{Z}.$$

$$\begin{pmatrix} \boldsymbol{E} \\ \boldsymbol{H} \end{pmatrix}(x,z) = \sum_p f_p(z)\, \boldsymbol{\psi}_p^{\mathrm{f}}(x,z) + \sum_p b_p(z)\, \boldsymbol{\psi}_p^{\mathrm{b}}(x,z) + \sum_j c_j\, \boldsymbol{\psi}_j^{\mathrm{c}}(r,\varphi),$$

$$r = r(x,z),\ \varphi = \varphi(x,z). \qquad f_p, b_p, c_j : \ ?$$



1-D linear finite elements



$$f_p(z) = \sum_{j=0}^{N} f_{p,j}\,\alpha_j(z)\,,$$

$b_p(z)$ analogous.

$$\begin{pmatrix} \boldsymbol{E} \\ \boldsymbol{H} \end{pmatrix}(x,z) = \sum_{p,j} f_{p,j}\big(\alpha_j \psi_j^{\mathrm{f}}\big)(x,z) + \sum_{p,j} b_{p,j}\big(\alpha_j \psi_j^{\mathrm{b}}\big)(x,z) + \sum_j c_j\, \psi_j'^{\mathrm{c}}(x,z)$$

$$=: \sum_k a_k \begin{pmatrix} \boldsymbol{E}_k \\ \boldsymbol{H}_k \end{pmatrix}(x,z), \qquad a_k \in \{f_{p,j}, b_{p,j}, c_j\}, \qquad a_k\text{: } ?$$

$$\begin{aligned} \boldsymbol{\nabla} \times \boldsymbol{H} - \mathrm{i}\omega\epsilon_0\epsilon\boldsymbol{E} &= 0 \\ -\boldsymbol{\nabla} \times \boldsymbol{E} - \mathrm{i}\omega\mu_0\boldsymbol{H} &= 0 \end{aligned} \quad \Big|_{\partial_y \to -\mathrm{i}k_y} \qquad \cdot \begin{pmatrix} \boldsymbol{F} \\ \boldsymbol{G} \end{pmatrix}^*, \qquad \iint$$

$$\rightsquigarrow \qquad \iint \mathcal{K}(\boldsymbol{F}, \boldsymbol{G}; \boldsymbol{E}, \boldsymbol{H}) \, \mathrm{d}x \, \mathrm{d}z = 0 \quad \text{for all } \boldsymbol{F}, \ \boldsymbol{G},$$

where

$$\mathcal{K}(\boldsymbol{F}, \boldsymbol{G}; \boldsymbol{E}, \boldsymbol{H}) = \boldsymbol{F}^* \cdot \left(\boldsymbol{\nabla}_{k_y} \times \boldsymbol{H}\right) - \boldsymbol{G}^* \cdot \left(\boldsymbol{\nabla}_{k_y} \times \boldsymbol{E}\right) - \mathrm{i}\omega\epsilon_0\epsilon\boldsymbol{F}^* \cdot \boldsymbol{E} - \mathrm{i}\omega\mu_0\boldsymbol{G}^* \cdot \boldsymbol{H} \, .$$

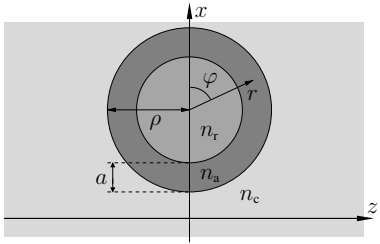
HCMT model, solution

- Insert $\begin{pmatrix} \boldsymbol{E} \\ \boldsymbol{H} \end{pmatrix} = \sum_k a_k \begin{pmatrix} \boldsymbol{E}_k \\ \boldsymbol{H}_k \end{pmatrix}$,
- select $\{\mathrm{u}\}$: indices of unknown coefficients,
  $\{\mathrm{g}\}$: given values related to prescribed influx,
- require $\iint \mathcal{K}(\boldsymbol{E}_l, \boldsymbol{H}_l; \boldsymbol{E}, \boldsymbol{H})\, \mathrm{d}x\, \mathrm{d}z = 0 \quad \text{for } l \in \{\mathrm{u}\}$,
- compute $K_{lk} = \iint \mathcal{K}(\boldsymbol{E}_l, \boldsymbol{H}_l; \boldsymbol{E}_k, \boldsymbol{H}_k)\, \mathrm{d}x\, \mathrm{d}z$.

$$\sum_{k\in\{\mathrm{u,g}\}} K_{lk} a_k = 0\,,\ l \in \{\mathrm{u}\}\,, \qquad \begin{pmatrix} \mathsf{K}_{\mathrm{u\,u}} & \mathsf{K}_{\mathrm{u\,g}} \end{pmatrix} \begin{pmatrix} \boldsymbol{a}_{\mathrm{u}} \\ \boldsymbol{a}_{\mathrm{g}} \end{pmatrix} = 0\,, \qquad \text{or} \qquad \mathsf{K}_{\mathrm{u\,u}} \boldsymbol{a}_{\mathrm{u}} = -\mathsf{K}_{\mathrm{u\,g}} \boldsymbol{a}_{\mathrm{g}}\,.$$

. . . plenty.

OAM modes of the coated step-index fiber

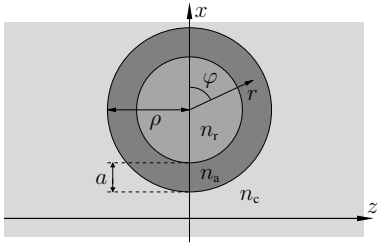


$$\begin{pmatrix} \boldsymbol{E} \\ \boldsymbol{H} \end{pmatrix}(r,\varphi,y) = \left(\boldsymbol{\Psi}(r)\,\mathrm{e}^{-\mathrm{i}l\varphi}\right)\,\mathrm{e}^{-\mathrm{i}kN_\mathrm{m}y}$$

angular order $l \in \mathbb{Z}$, effective index N_m;

degenerate modes OAM$(l,\ .\ )$ and OAM$(-l,\ .\ )$.

OAM modes of the coated step-index fiber



$$\begin{pmatrix} \boldsymbol{E} \\ \boldsymbol{H} \end{pmatrix}(r,\varphi,y) = \left(\boldsymbol{\Psi}(r)\,\mathrm{e}^{-\mathrm{i}l\varphi}\right)\,\mathrm{e}^{-\mathrm{i}kN_{\mathrm{m}}y}$$

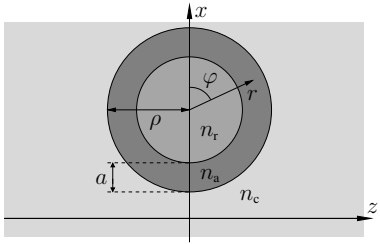
angular order $l \in \mathbb{Z}$, effective index N_{m};
degenerate modes OAM$(l,\ .\ )$ and OAM$(-l,\ .\ )$.

$n_{\mathrm{r}} : n_{\mathrm{a}} : n_{\mathrm{c}} = 1.45 : 3.45 : 1.0$,
$a = 0.22\,\mu\mathrm{m}$, $\rho = 2\,\mu\mathrm{m}$, $\lambda = 1.55\,\mu\mathrm{m}$:

TE$(0,1)$, TE$(0,2)$, TE$(0,3)$,
TM$(0,1)$, TM$(0,2)$, TM$(0,3)$,
OAM$(\pm l,1)$, $l = 1,2,\ldots,20$,
OAM$(\pm l,2)$, $l = 1,2,\ldots,11$,
OAM$(\pm l,3)$, $l = 1,2,\ldots,5$,
OAM$(\pm l,4)$, $l = 1,2,3$,
OAM$(\pm l,5)$, $l = 1,2$,
OAM$(\pm 1,6)$;

90 orthogonal modes.

OAM modes of the coated step-index fiber



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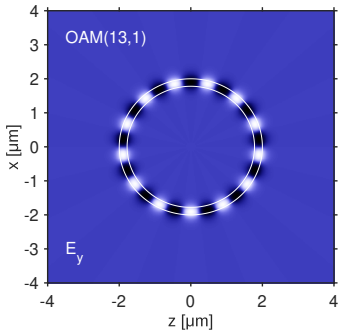
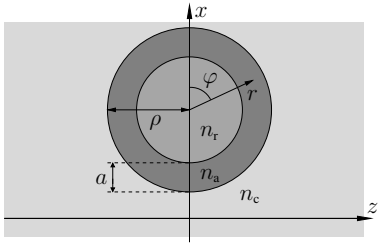


OAM modes of the coated step-index fiber



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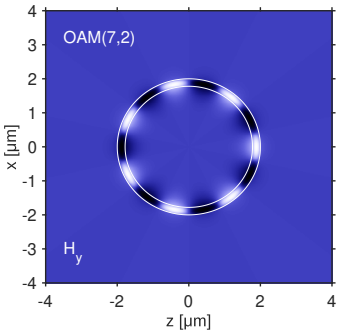
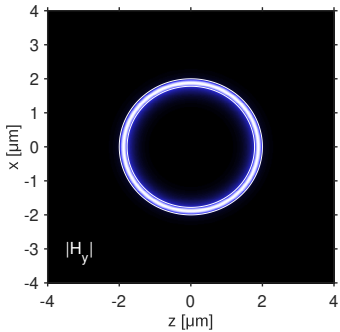
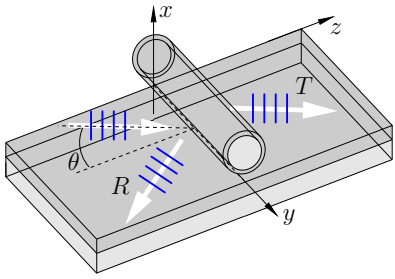
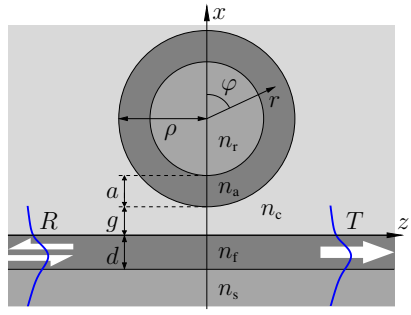


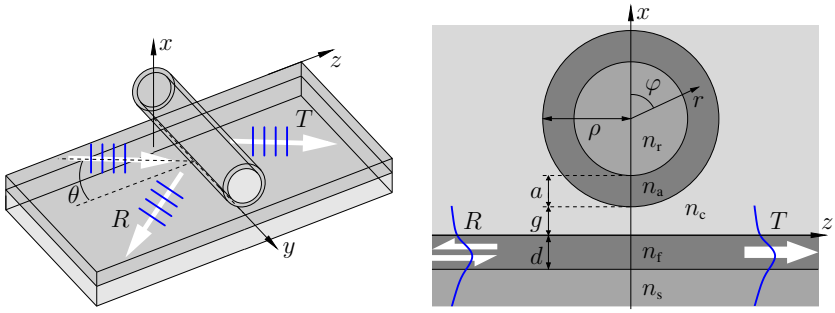


Oblique resonant excitation of the fiber



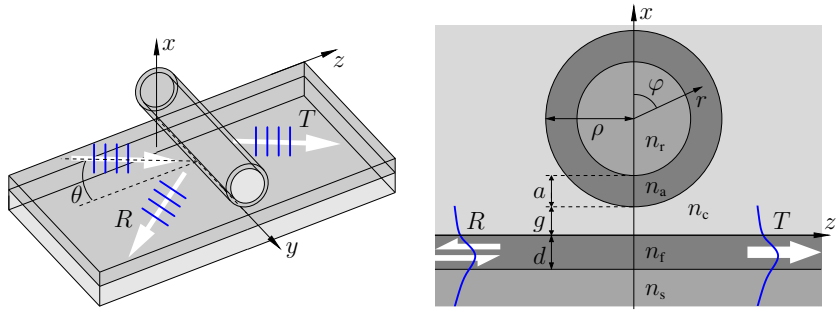


Oblique resonant excitation of the fiber



The fiber supports a guided mode with effective index N_{m}.

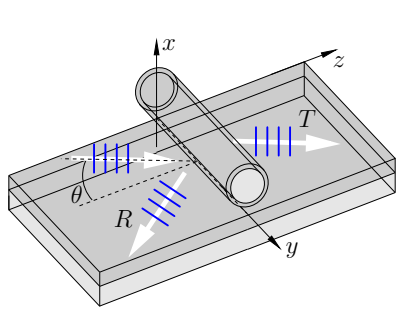
Oblique resonant excitation of the fiber

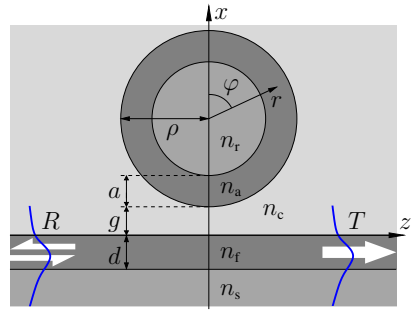


The fiber supports a guided mode with effective index N_{m}

Resonant interaction with the waves in the slab expected at $\theta \approx \theta_{\mathrm{m}}$,
where $k_y = kN_{\mathrm{TE}} \sin\theta \approx kN_{\mathrm{m}}$, $\sin\theta_{\mathrm{m}} = N_{\mathrm{m}}/N_{\mathrm{TE}}$ (TE input).

Oblique resonant excitation of the fiber





The fiber supports a guided mode with effective index N_m

↳ Resonant interaction with the waves in the slab expected at $\theta \approx \theta_m$,
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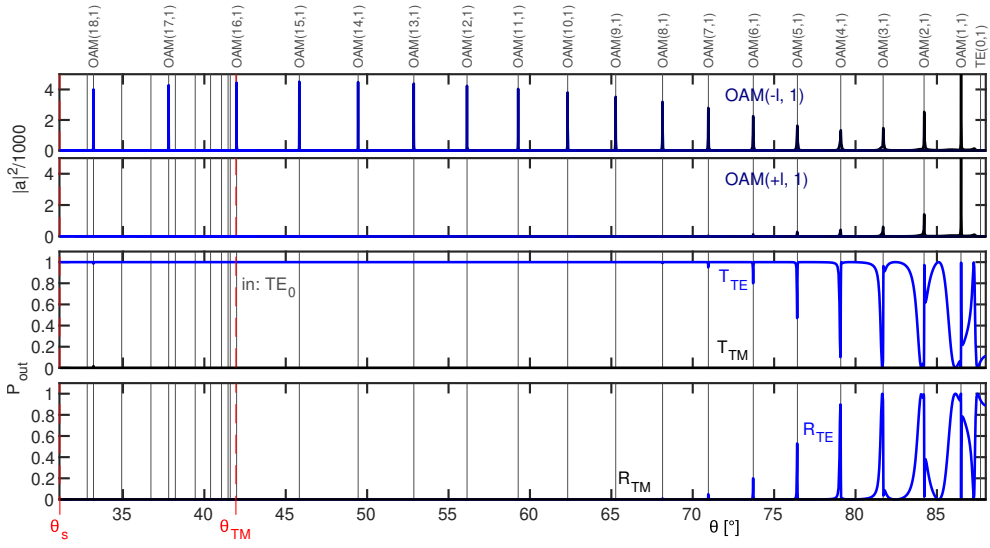
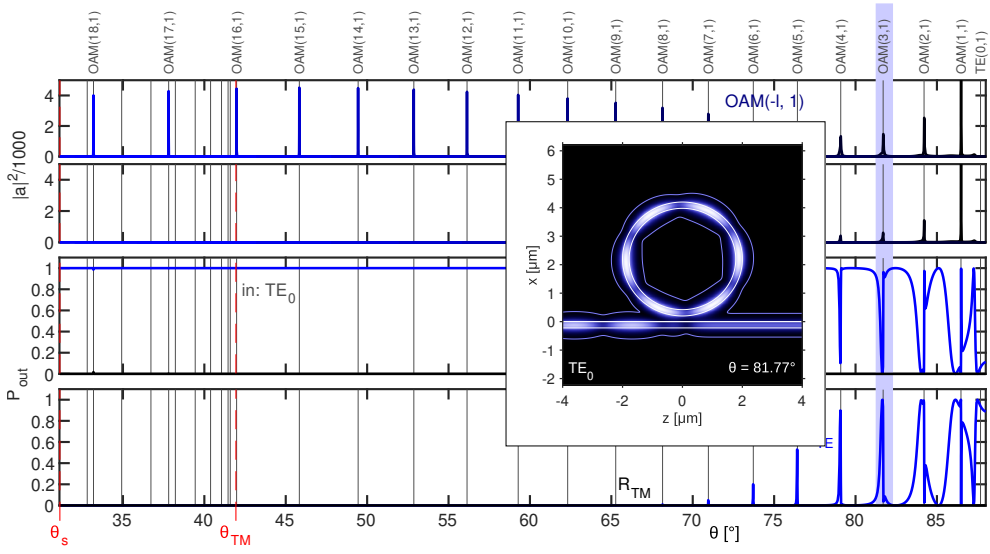
Angular spectrum, TE excitation



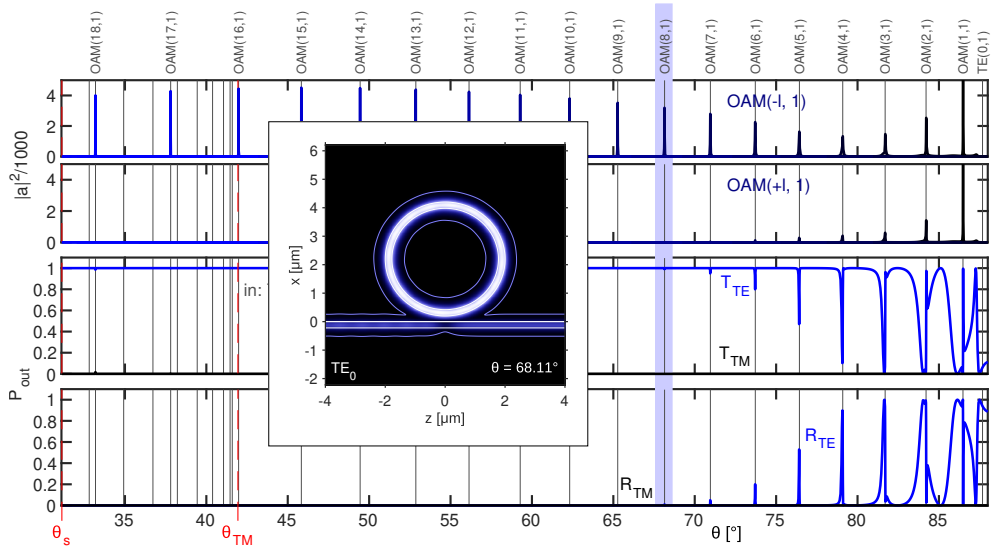
($g = 0.3\,\mu\text{m}$)

Angular spectrum, TE excitation



($g = 0.3$ μm, spectrum, $g = 0.2$ μm, absolute electric field $|\boldsymbol{E}|$)

Angular spectrum, TE excitation



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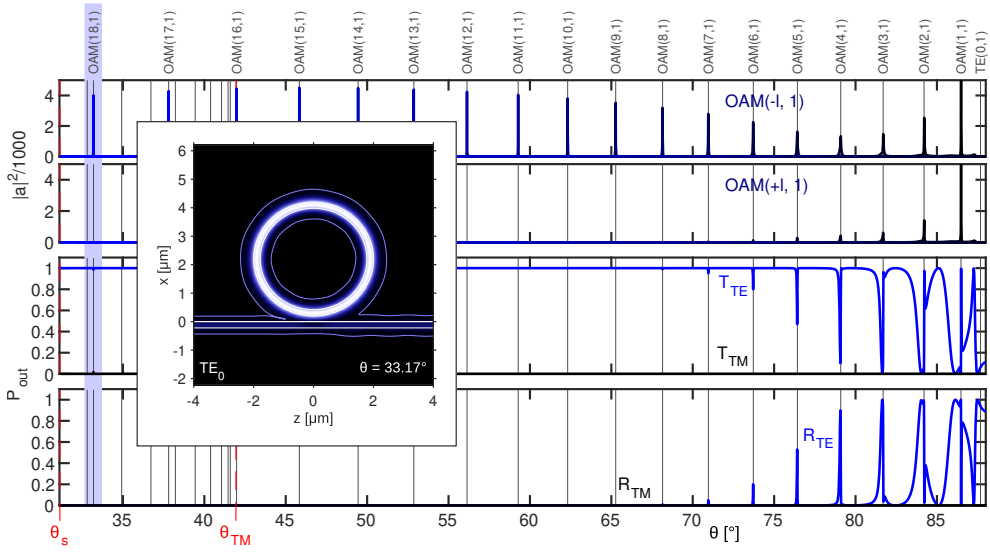
Angular spectrum, TE excitation



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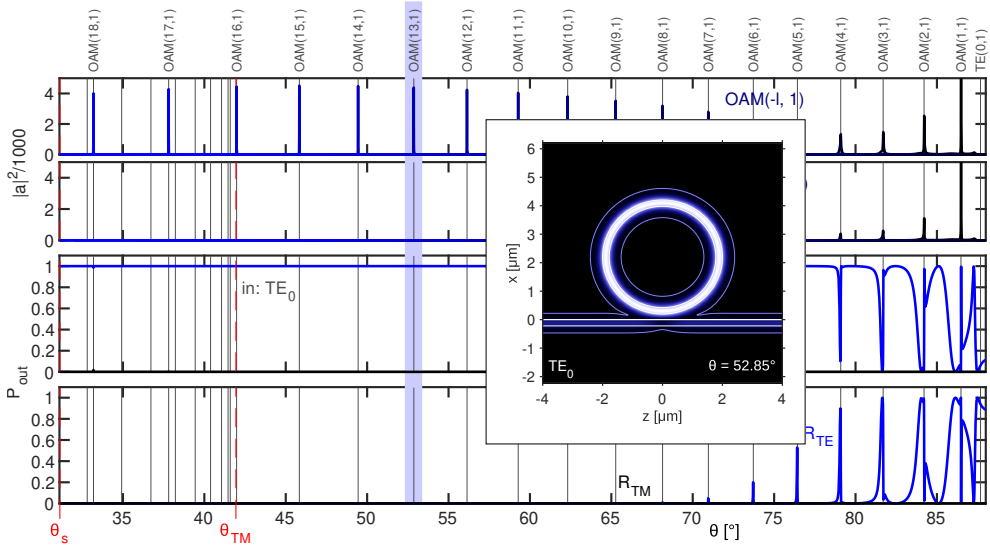
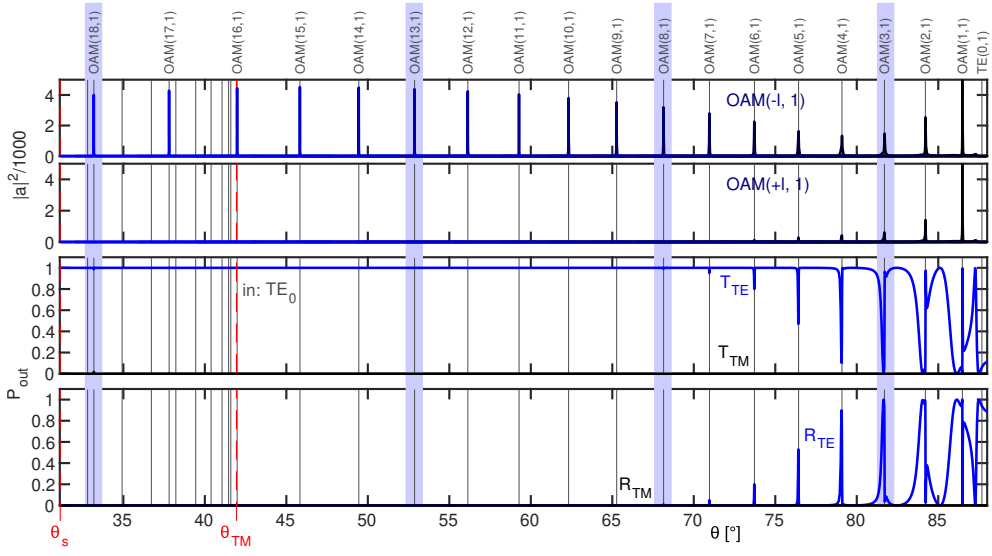
Angular spectrum, TE excitation

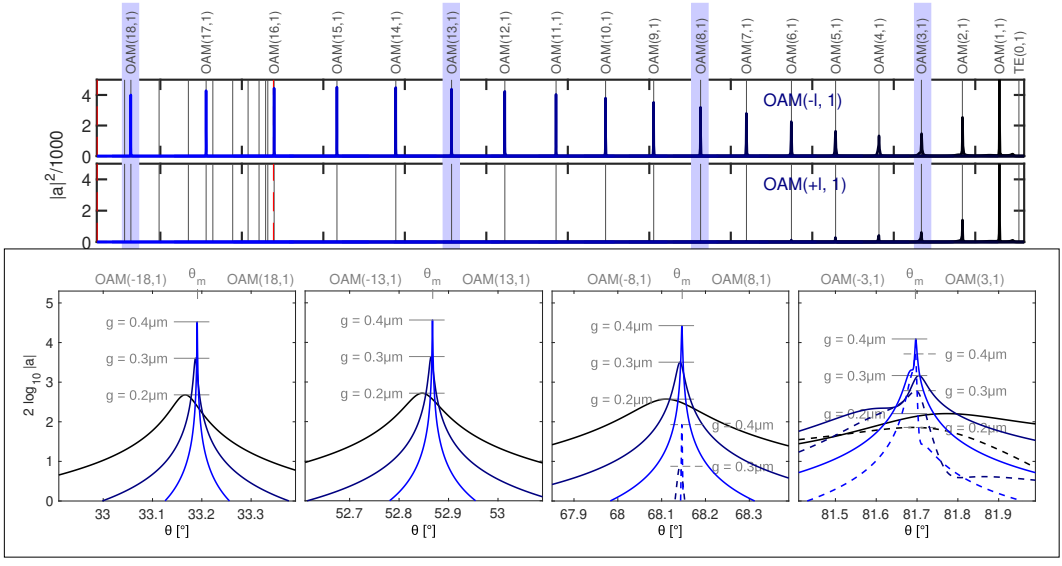


($g = 0.3$ μm, spectrum, $g = 0.2$ μm, absolute electric field $|\boldsymbol{E}|$)

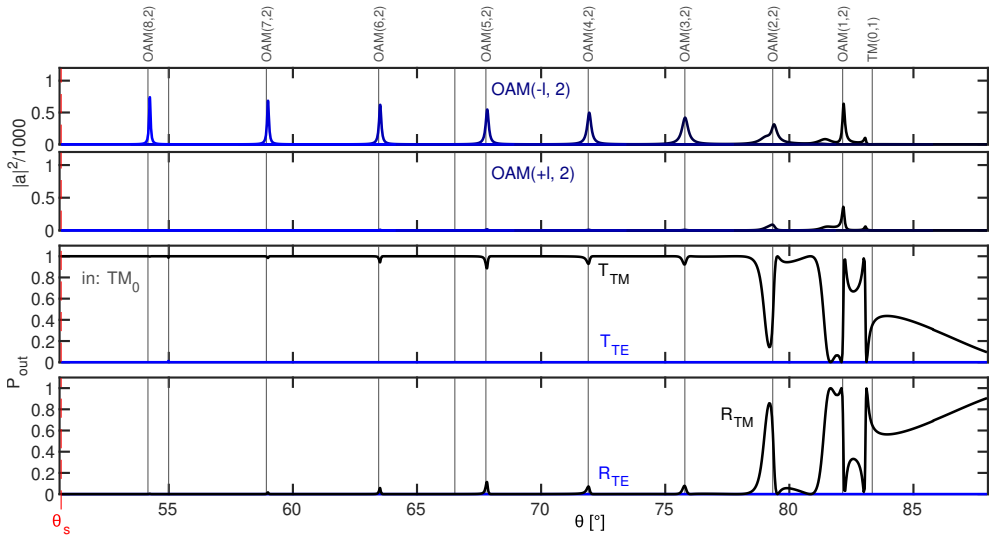
Amplitudes at resonance, TE excitation



Amplitudes at resonance, TE excitation

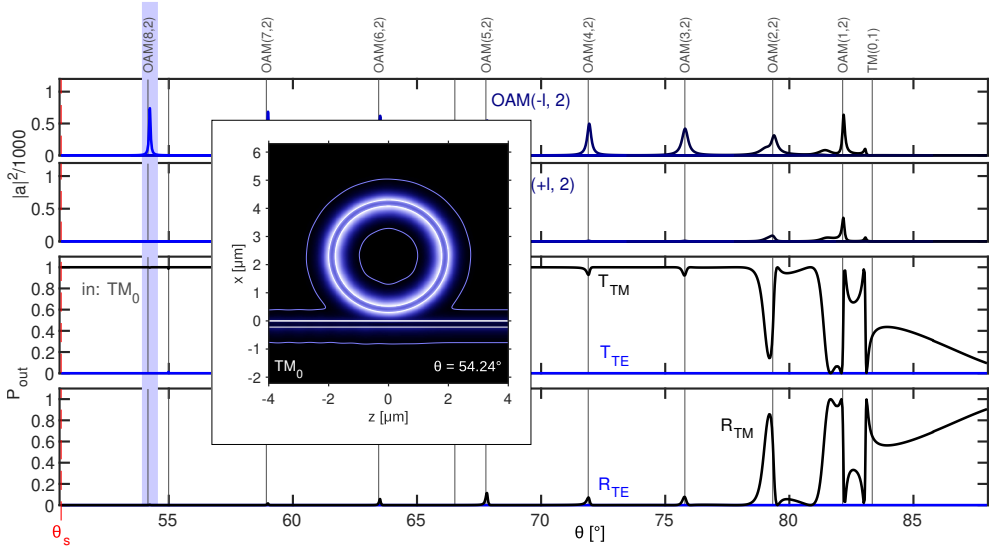


Angular spectrum, TM excitation



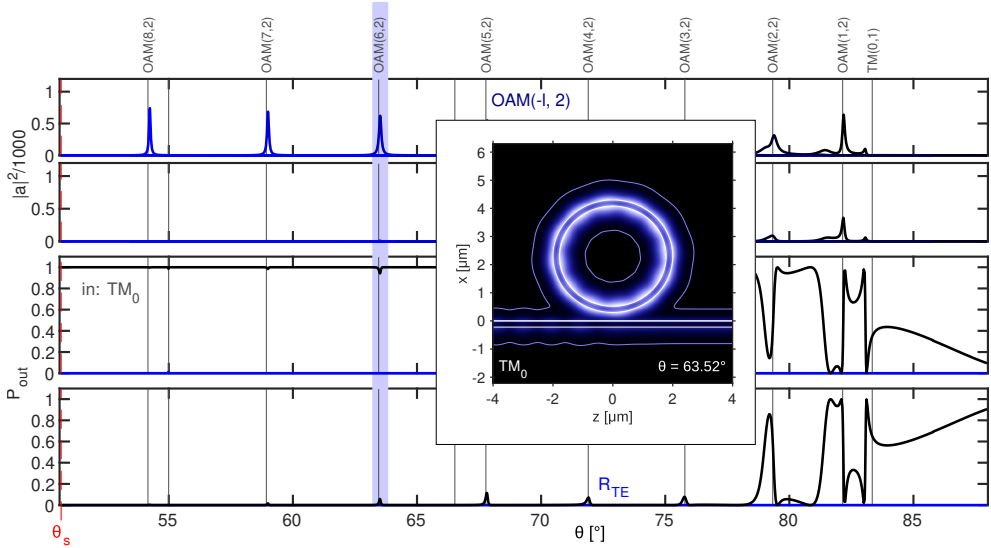
($g = 0.3\,\mu\text{m}$)

Angular spectrum, TM excitation



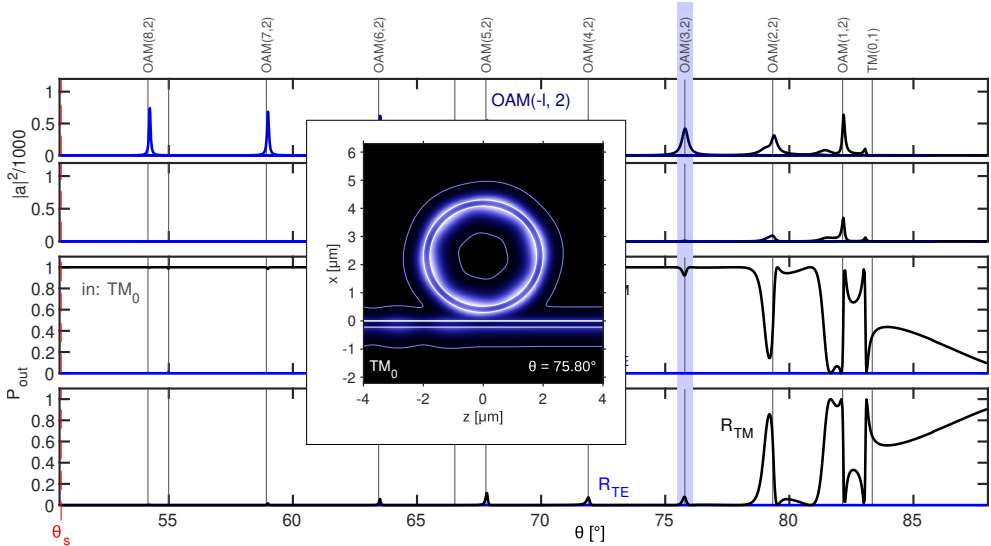
($g = 0.3$ μm, spectrum, absolute electric field $|\boldsymbol{E}|$)

Angular spectrum, TM excitation



($g = 0.3$ μm, spectrum, absolute electric field $|\boldsymbol{E}|$)

Angular spectrum, TM excitation



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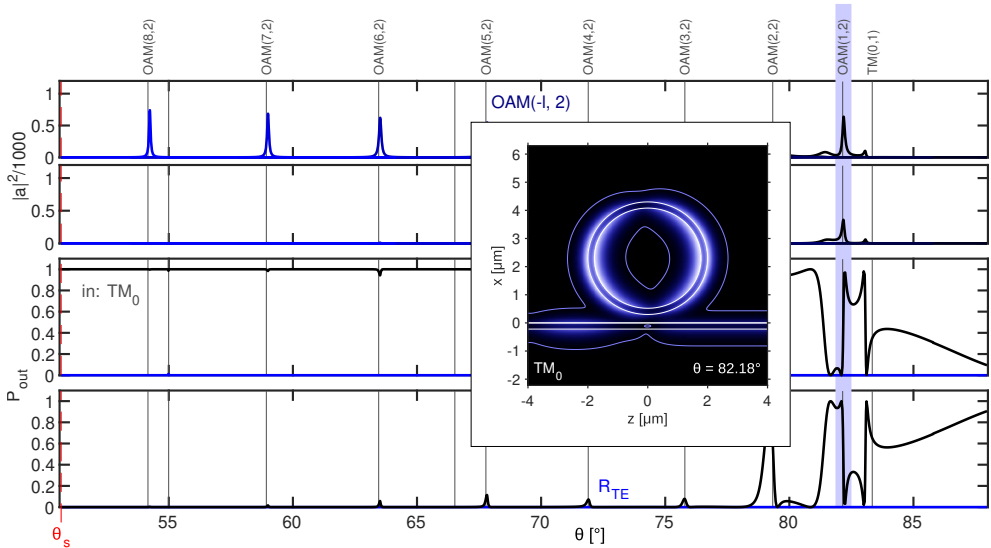
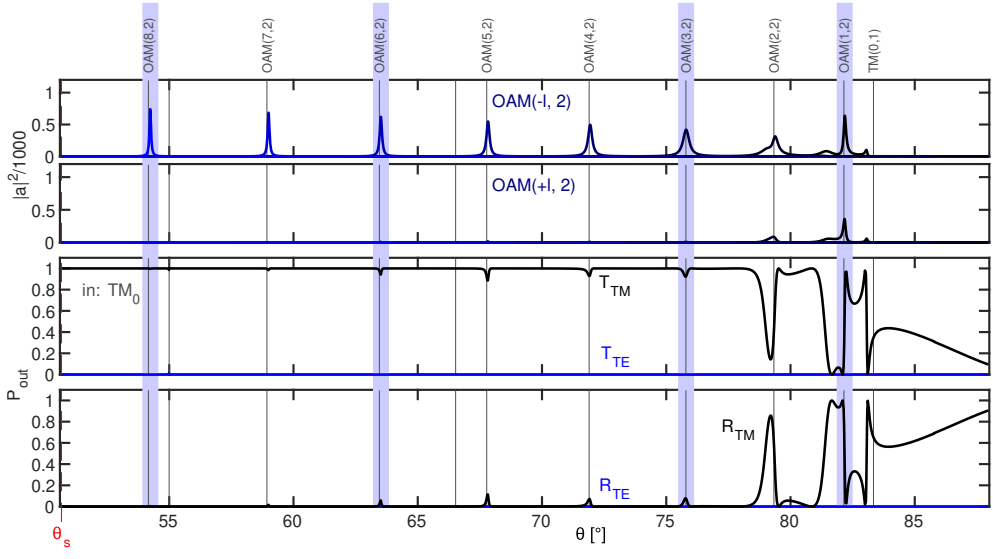
Angular spectrum, TM excitation

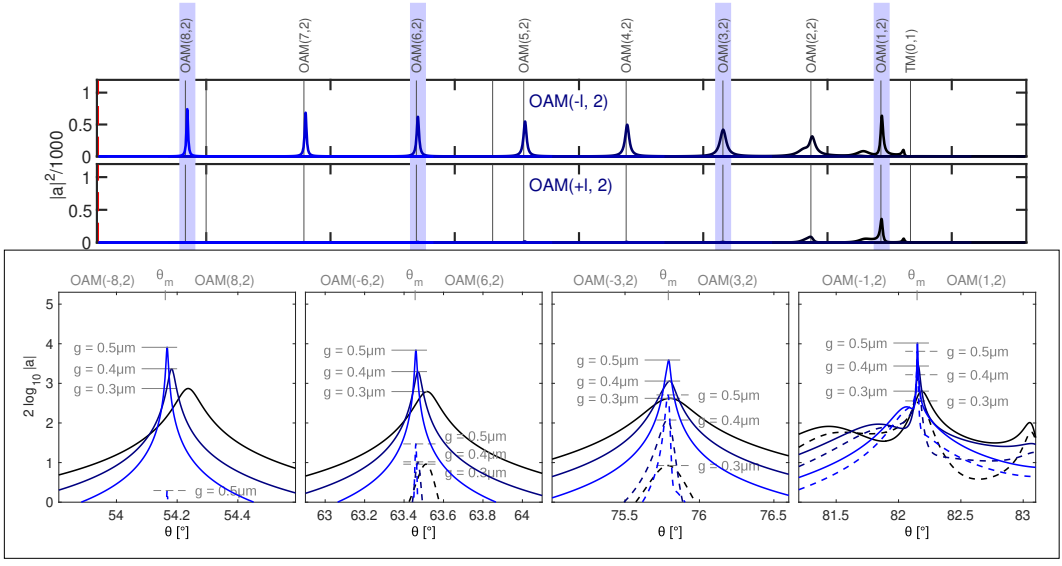


($g = 0.3$ µm, spectrum, absolute electric field $|\boldsymbol{E}|$)

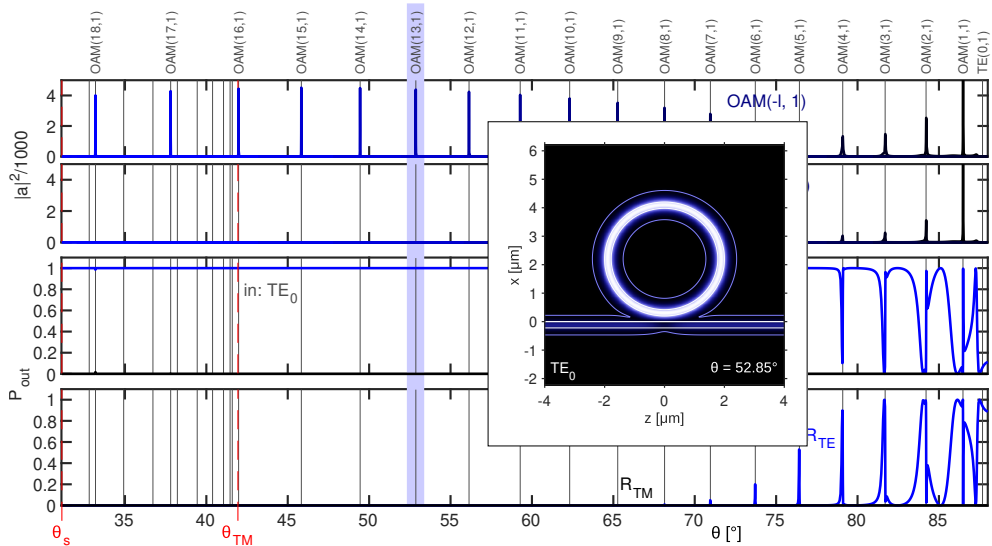
Amplitudes at resonance, TM excitation



Amplitudes at resonance, TM excitation

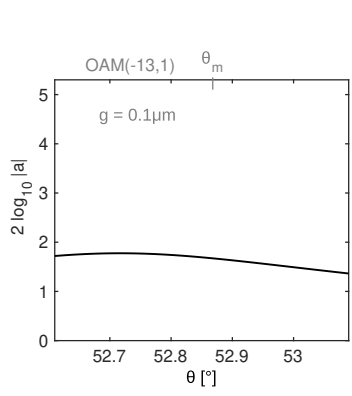


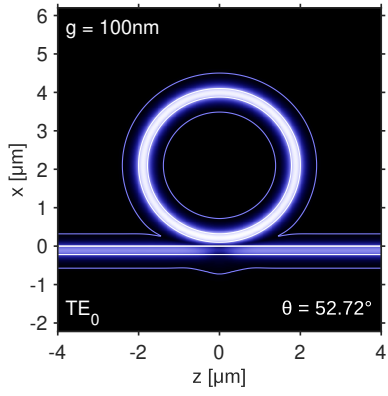
OAM$(\pm 13, 1)$*, TE excitation*



($g = 0.3$ μm, spectrum, $g = 0.2$ μm, absolute electric field $|\boldsymbol{E}|$)

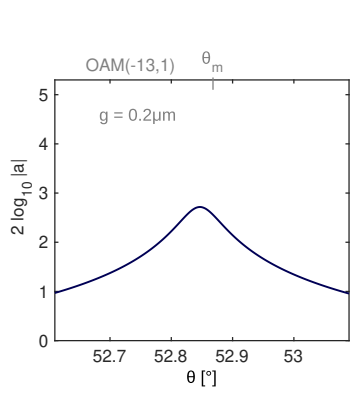
OAM$(\pm 13, 1)$*, TE excitation, varying gap*

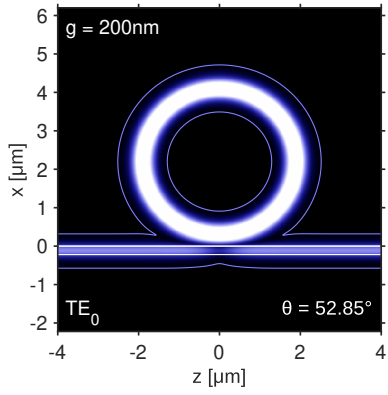




Purity: $\dfrac{|a_{-13}|^2}{\sum_j |a_j|^2} = 1 - 6 \cdot 10^{-3}.$

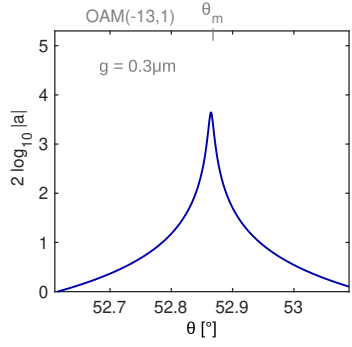
OAM$(\pm 13, 1)$*, TE excitation, varying gap*

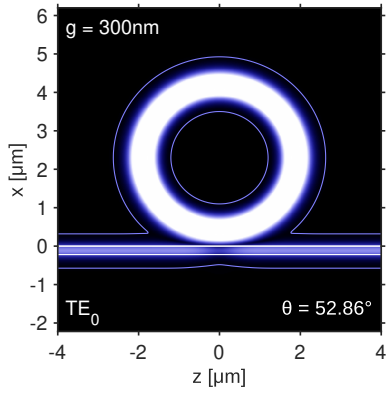




Purity: $\dfrac{|a_{-13}|^2}{\sum_j |a_j|^2} = 1 - 1 \cdot 10^{-4}$.

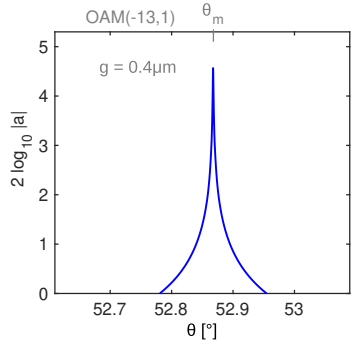
OAM$(\pm 13, 1)$*, TE excitation, varying gap*

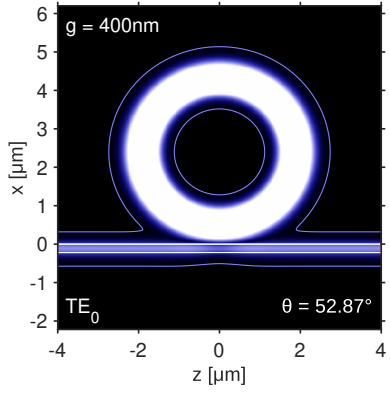




Purity: $\dfrac{|a_{-13}|^2}{\sum_j |a_j|^2} = 1 - 3 \cdot 10^{-6}$.

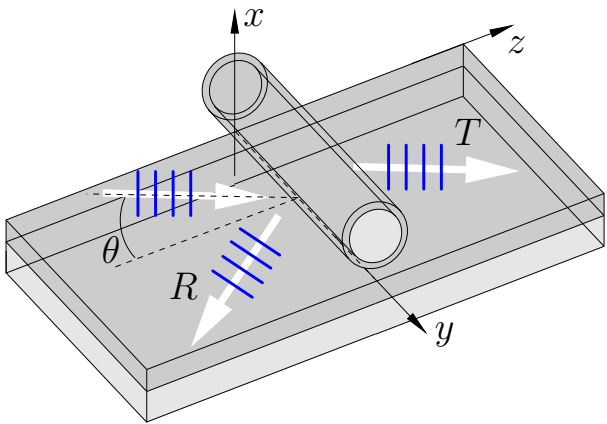
OAM$(\pm 13, 1)$*, TE excitation, varying gap*



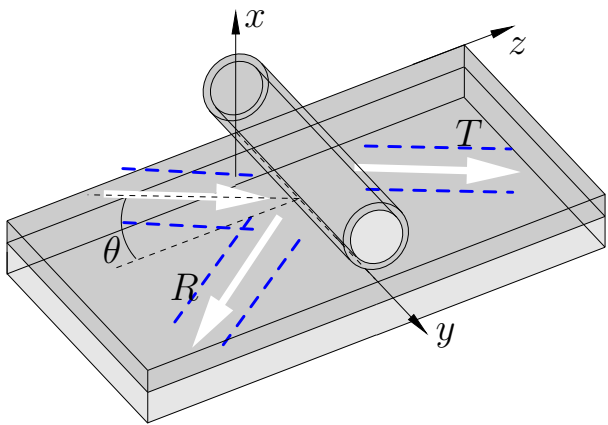


Purity: $\dfrac{|a_{-13}|^2}{\sum_j |a_j|^2} = 1 - 2 \cdot 10^{-7}.$

(2.5-D) $\partial_y \epsilon = 0,\ (\boldsymbol{E}, \boldsymbol{H}) \sim \exp(-\mathrm{i} k_y y),\ k_y \sim \sin\theta$



(3-D) $\partial_y \epsilon = 0,\ (\boldsymbol{E}, \boldsymbol{H}) = \int (\ .\ ) \exp(-\mathrm{i} k_y y)\, \mathrm{d}k_y$



Gaussian bundles of semi-guided waves

- Superimpose 2-D solutions for a range of k_y / a range of θ, such that the input field resembles an in-plane confined beam.

$$(\boldsymbol{E}, \boldsymbol{H})\,(x, \quad z) = \boldsymbol{\Psi}_{\text{in}}(k_y; x)\, \mathrm{e}^{-\mathrm{i}k_z(k_y)(z - z_0)} + \boldsymbol{\rho}(k_y; x, z)$$

Gaussian bundles of semi-guided waves

- Superimpose 2-D solutions for a range of k_y / a range of θ, such that the input field resembles an in-plane confined beam.

$$(\boldsymbol{E}, \boldsymbol{H})\,(x, y, z) =$$

$$\left(\boldsymbol{\Psi}_{\text{in}}(k_y; x)\, \mathrm{e}^{-\mathrm{i} k_z(k_y)(z - z_0)} + \boldsymbol{\rho}(k_y; x, z) \right) \mathrm{e}^{-\mathrm{i} k_y (y - y_0)}$$

Gaussian bundles of semi-guided waves

- Superimpose 2-D solutions for a range of k_y / a range of θ, such that the input field resembles an in-plane confined beam.

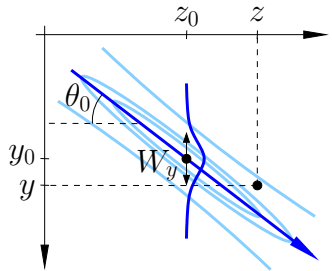
$$(\boldsymbol{E}, \boldsymbol{H})\,(x, y, z) = A \int \mathrm{e}^{-\frac{(k_y - k_{y0})^2}{w_k^2}} \left(\boldsymbol{\Psi}_{\mathrm{in}}(k_y; x)\, \mathrm{e}^{-\mathrm{i} k_z(k_y)(z - z_0)} + \boldsymbol{\rho}(k_y; x, z) \right) \mathrm{e}^{-\mathrm{i} k_y (y - y_0)}\, \mathrm{d}k_y$$

Focus at (y_0, z_0),
primary angle of incidence θ_0,
$k_{y0} = k N_{\mathrm{in}} \sin\theta_0$.

Gaussian bundles of semi-guided waves

- Superimpose 2-D solutions for a range of k_y / a range of θ, such that the input field resembles an in-plane confined beam.
- Incoming wave, "small" w_k:

$$(\boldsymbol{E},\boldsymbol{H})_{\text{in}}(x,y,z) \sim \mathrm{e}^{-\frac{\left((y-y_0)-\frac{k_{y0}}{k_{z0}}(z-z_0)\right)^2}{(W_y/2)^2}} \boldsymbol{\Psi}_{\text{in}}(k_{y0};x)\,\mathrm{e}^{-\mathrm{i}(k_{y0}(y-y_0)+k_{z0}(z-z_0))}$$



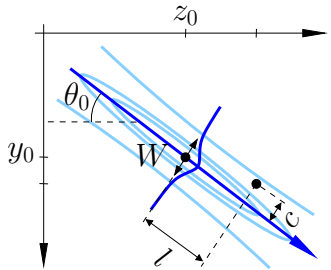
Focus at (y_0, z_0),
primary angle of incidence θ_0,
$k_{y0} = kN_{\text{in}} \sin\theta_0$,
$k_{z0} = kN_{\text{in}} \cos\theta_0$,
width W_y (full, along y, 1/e, field, at focus),

$W_y = 4/w_k$.

Gaussian bundles of semi-guided waves

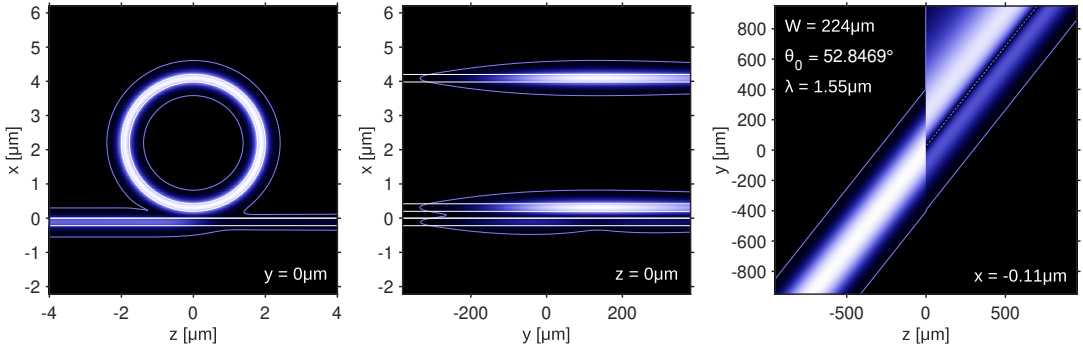
- Superimpose 2-D solutions for a range of k_y / a range of θ, such that the input field resembles an in-plane confined beam.
- Incoming wave, "small" w_k:

$$(\boldsymbol{E},\boldsymbol{H})_{\text{in}}\,(x,c,l) \sim \mathrm{e}^{-\dfrac{c^2}{(W/2)^2}}\ \boldsymbol{\Psi}_{\text{in}}(k_{y0};x)\ \ \mathrm{e}^{-\mathrm{i}kN_{\text{in}}l}$$



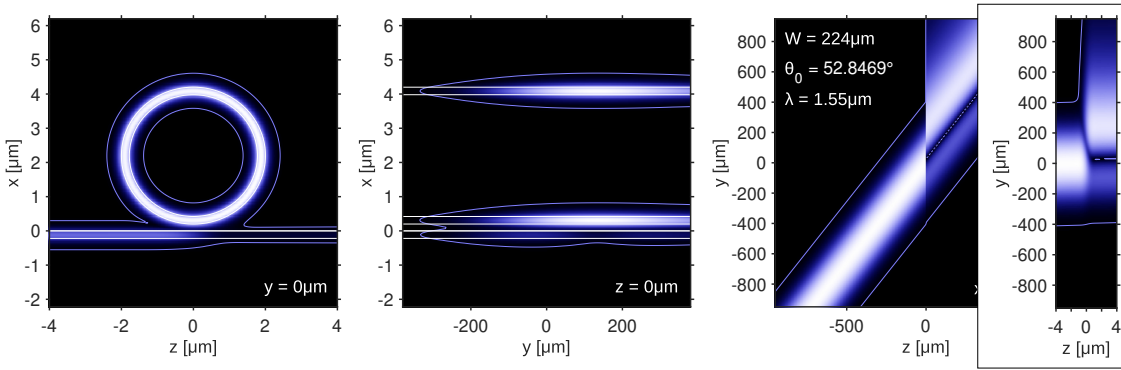
Focus at (y_0, z_0),
primary angle of incidence θ_0,
$k_{y0} = kN_{\text{in}} \sin\theta_0$,
$k_{z0} = kN_{\text{in}} \cos\theta_0$,
width W_y (full, along y, 1/e, field, at focus),
width W (full, cross section, 1/e, field, at focus),
$W_y = 4/w_k$, $W = W_y \cos\theta_0$.

Excitation by semi-guided beams



($g = 200\,\text{nm}$, TE input, target mode OAM$(-13, 1)$; absolute electric field $|\boldsymbol{E}|$)

Excitation by semi-guided beams



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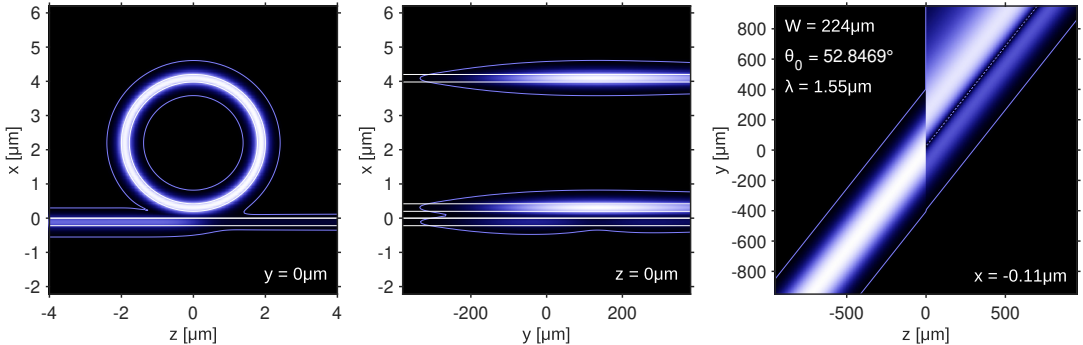

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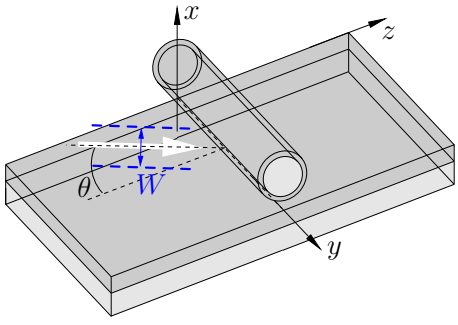
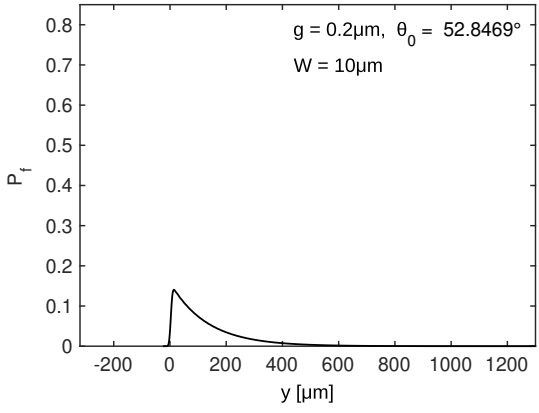
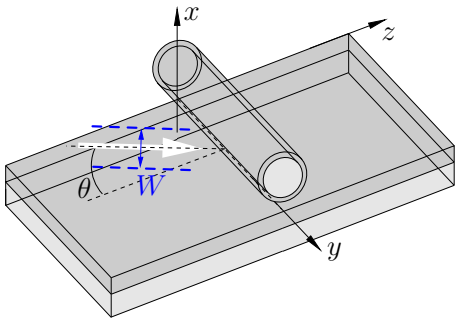
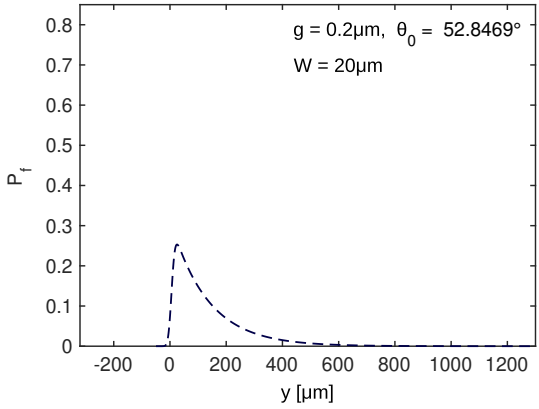




$P_f(y)$: Power fraction diverted from the incoming beam to the fiber, at axial position y.

Excitation by semi-guided beams





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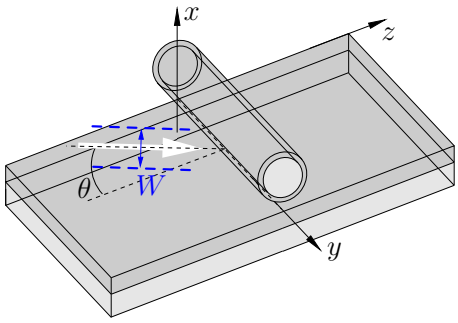

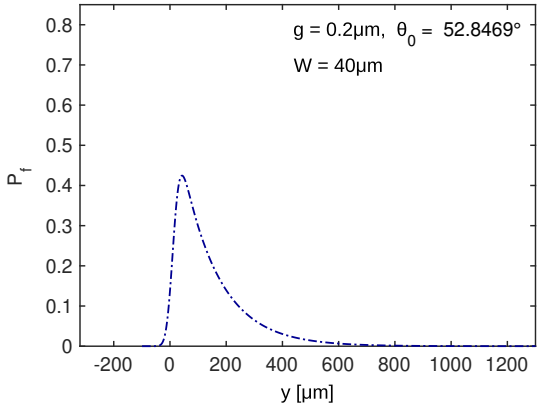

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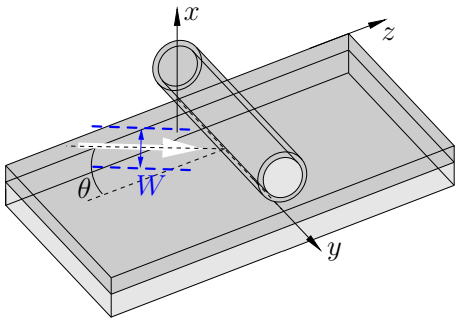

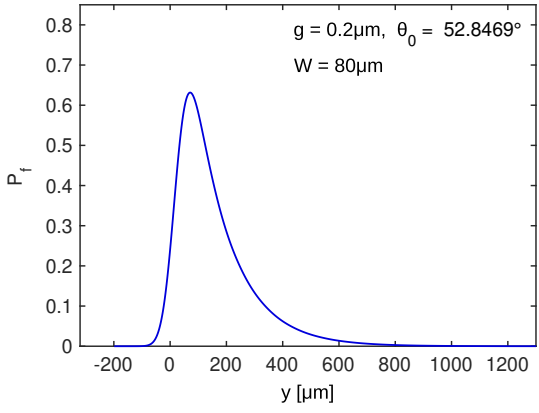

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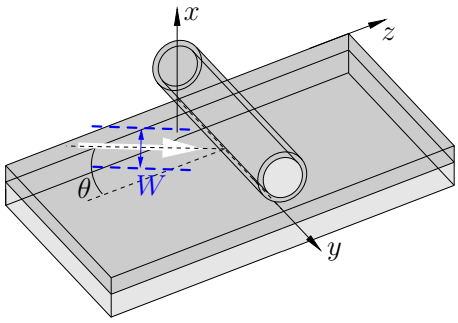

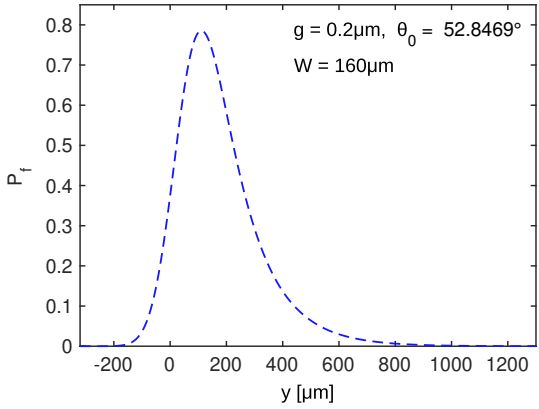

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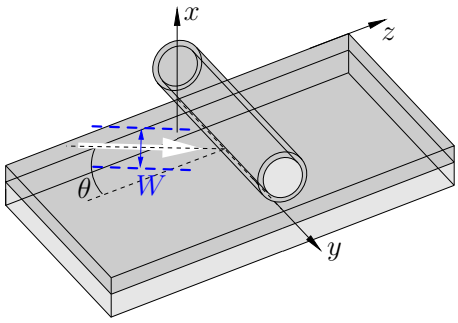

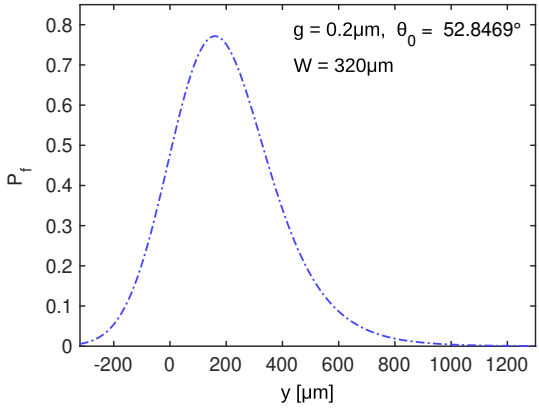

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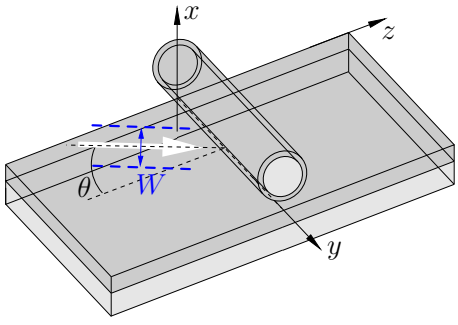

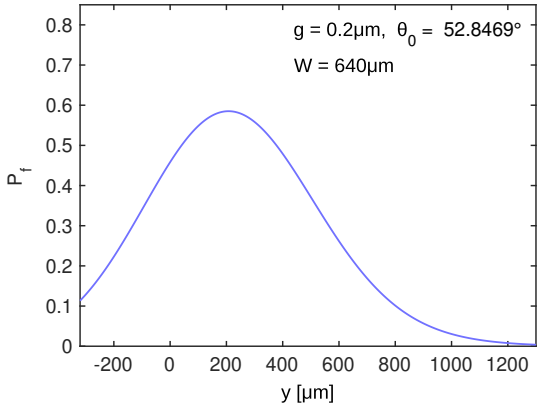

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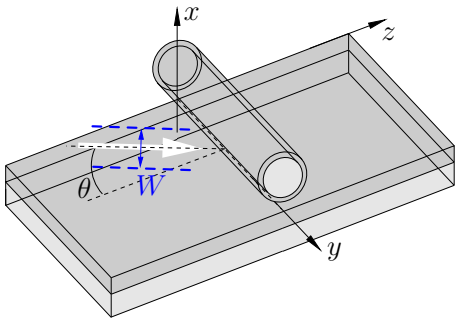

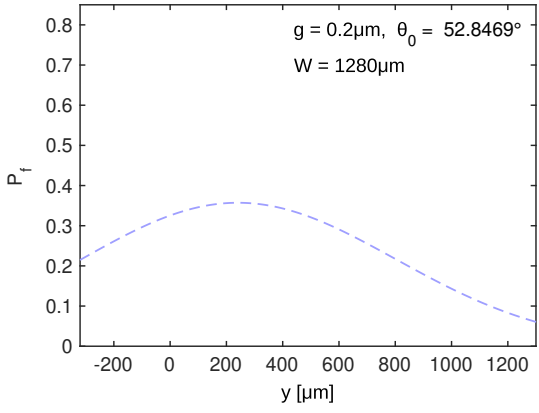

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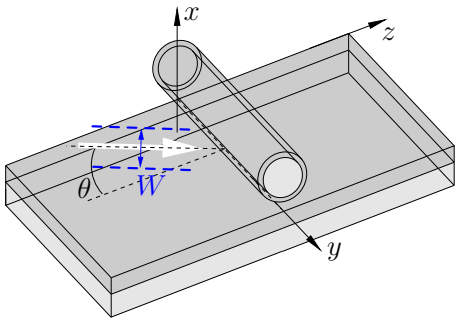

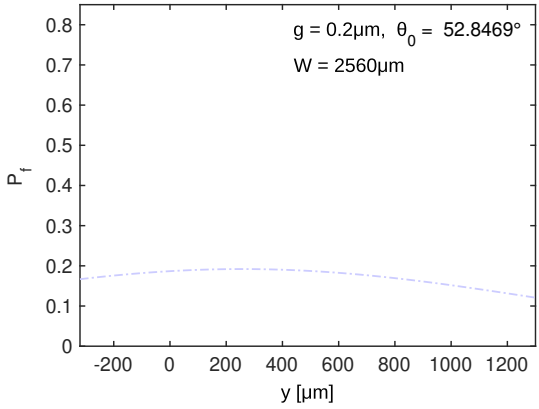

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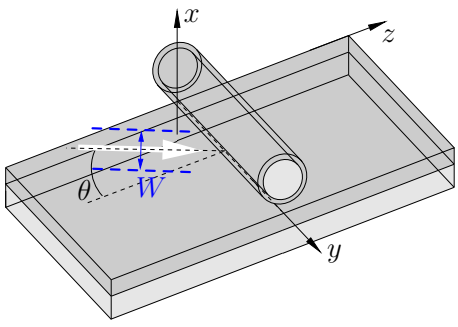
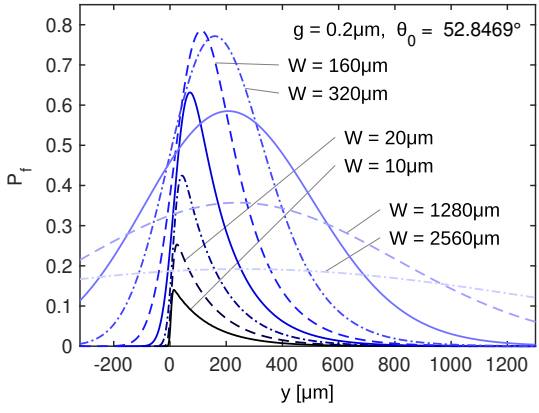
Excitation by semi-guided beams





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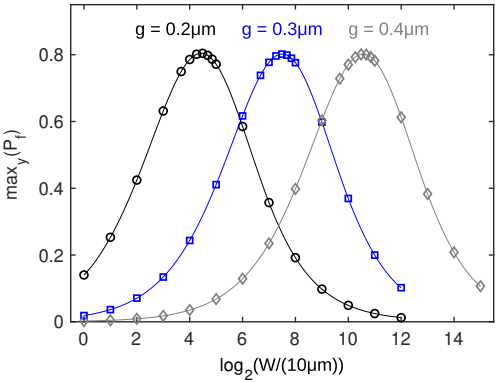
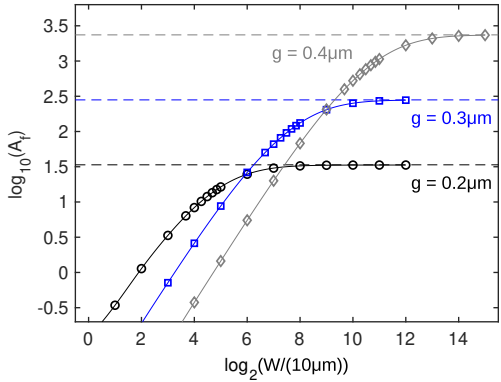
Excitation by semi-guided beams

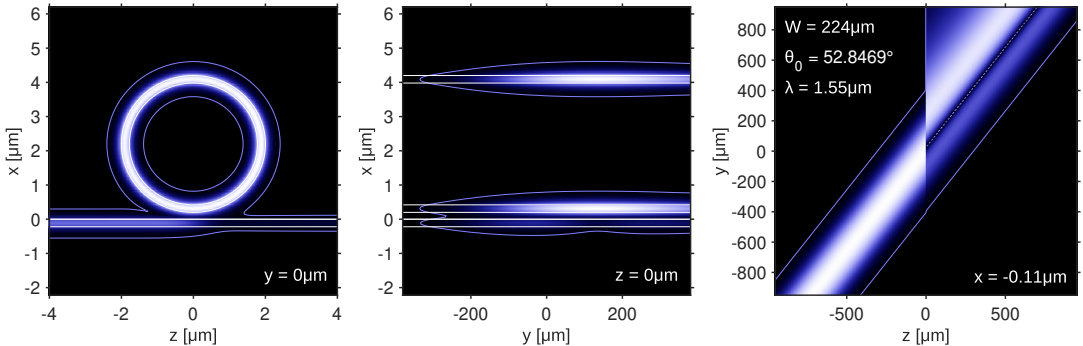




A_{f}: Amplification ratio $\max_y |\boldsymbol{E}_{\mathrm{fiber}}|^2 / \max_z |\boldsymbol{E}_{\mathrm{in}}|^2$

$P_{\mathrm{f}}(y)$: Power fraction diverted from the incoming beam to the fiber, at axial position y.

Excitation by semi-guided beams

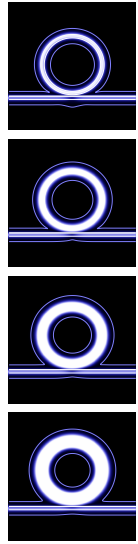


($g = 200\,\text{nm}$, TE input, target mode OAM$(-13, 1)$; absolute electric field $|\boldsymbol{E}|$)

$\max_y P_\text{f} \approx 0.8, \quad A_\text{f} \approx 10^{1.5}, \quad (\text{purity} \approx 0.9999).$

Resonant evanescent excitation of OAM modes in a high-contrast circular step-index fiber:

- an exceptionally simple, efficient scheme for the generation of waves that carry high order orbital angular momentum,
- similar resonance features for variations of vacuum wavelength λ instead of angle θ,
- an optical resonator of travelling-wave type with an open, lossless dielectric cavity,
- concept transfers to other fiber/slab configurations, e.g. to systems with slightly lower contrast, or to a non-coated, high-index dielectric rod.



— supplementary material —

Formal problem, effective permittivity

$$\boldsymbol{\nabla} \times \tilde{\boldsymbol{E}} = -\mathrm{i}\omega\mu_0 \tilde{\boldsymbol{H}}, \quad \boldsymbol{\nabla} \times \tilde{\boldsymbol{H}} = \mathrm{i}\omega\epsilon\epsilon_0 \tilde{\boldsymbol{E}},$$

& $\partial_y \epsilon = 0,$

& $\begin{pmatrix} \tilde{\boldsymbol{E}} \\ \tilde{\boldsymbol{H}} \end{pmatrix}(x,y,z) = \begin{pmatrix} \boldsymbol{E} \\ \boldsymbol{H} \end{pmatrix}(x,z)\, \mathrm{e}^{-\mathrm{i}k_y y}, \quad k_y = kN_{\mathrm{in}} \sin\theta$

$$\begin{pmatrix} \partial_x \frac{1}{\epsilon}\partial_x \epsilon + \partial_z^2 & \partial_x \frac{1}{\epsilon}\partial_z \epsilon - \partial_z \partial_x \\ \partial_z \frac{1}{\epsilon}\partial_x \epsilon - \partial_x \partial_z & \partial_x^2 + \partial_z \frac{1}{\epsilon}\partial_z \epsilon \end{pmatrix} \begin{pmatrix} E_x \\ E_z \end{pmatrix} + k^2 \epsilon_{\mathrm{eff}} \begin{pmatrix} E_x \\ E_z \end{pmatrix} = 0,$$

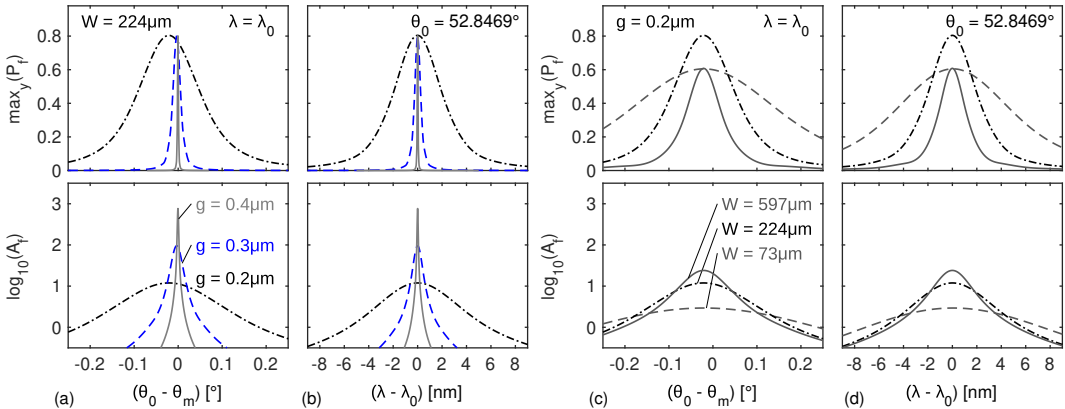
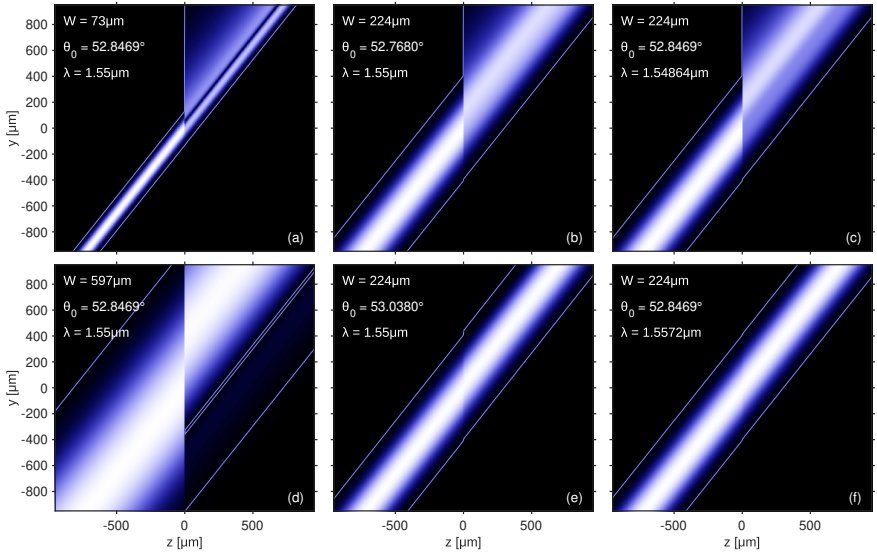
$\epsilon_{\mathrm{eff}}(x,z) = \epsilon(x,z) - N_{\mathrm{in}}^2 \sin^2\theta,$

2-D domain, transparent-influx boundary conditions.

- Where $\partial_x \epsilon = \partial_z \epsilon = 0$:

  $\left(\partial_x^2 + \partial_z^2\right)\phi + k^2 \epsilon_{\mathrm{eff}} \phi = 0, \quad \phi = E_j, H_j.$

Excitation by semi-guided beams, tolerances



Excitation by semi-guided beams, less optimal configurations