

Analytical approaches to the description of optical microresonator devices



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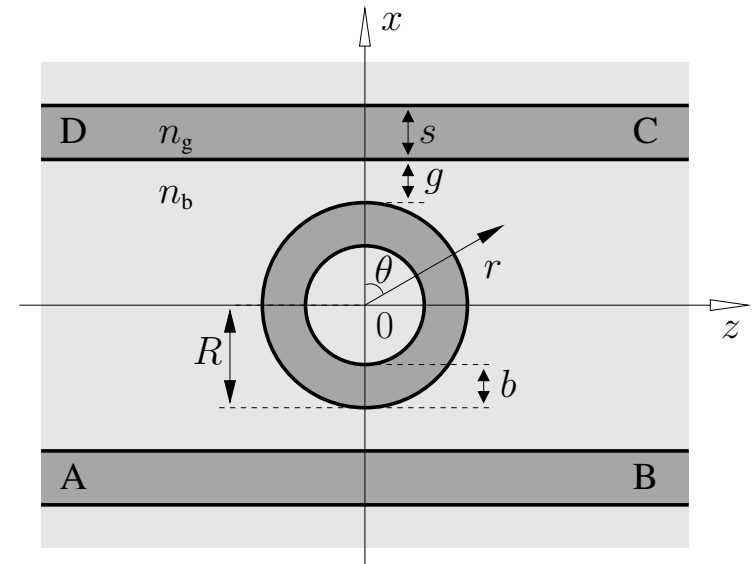
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Outline

Circular traveling wave resonators

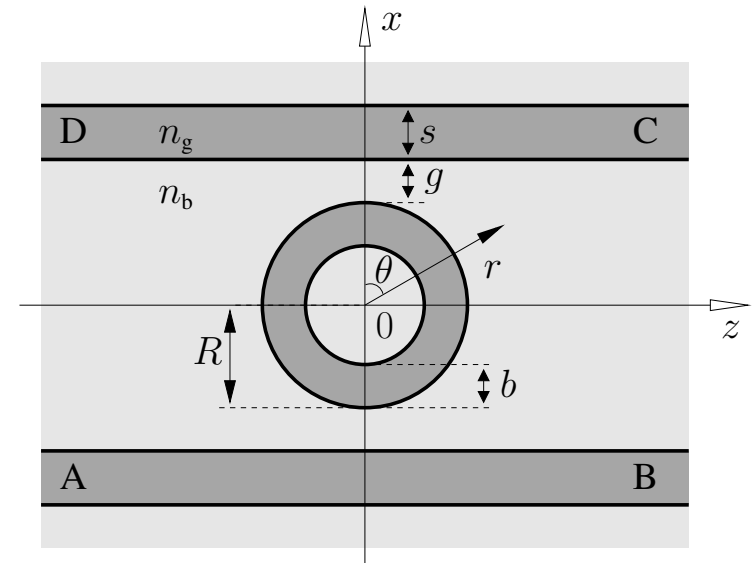
- Abstract model & implications
- Bent slab waveguides & examples
- Coupler modeling & examples



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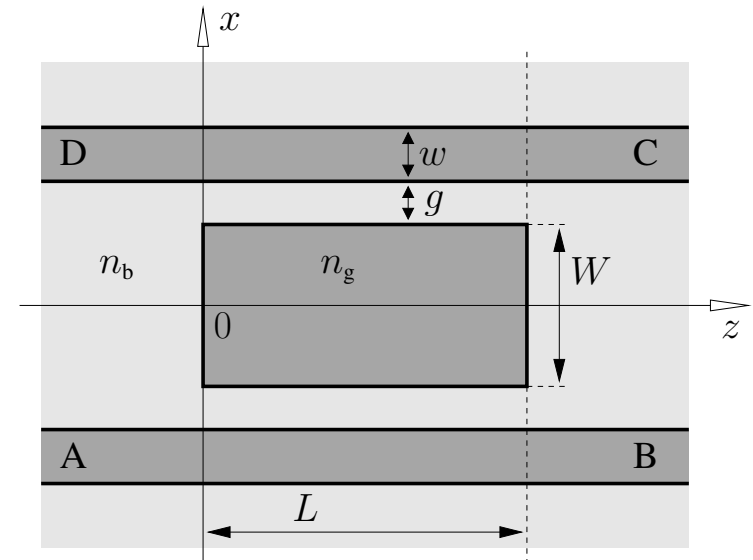
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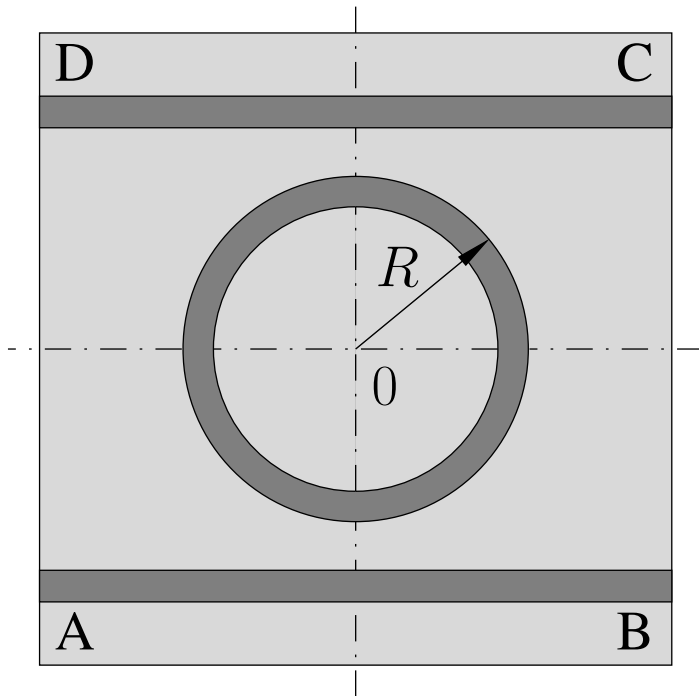


Rectangular standing wave resonators

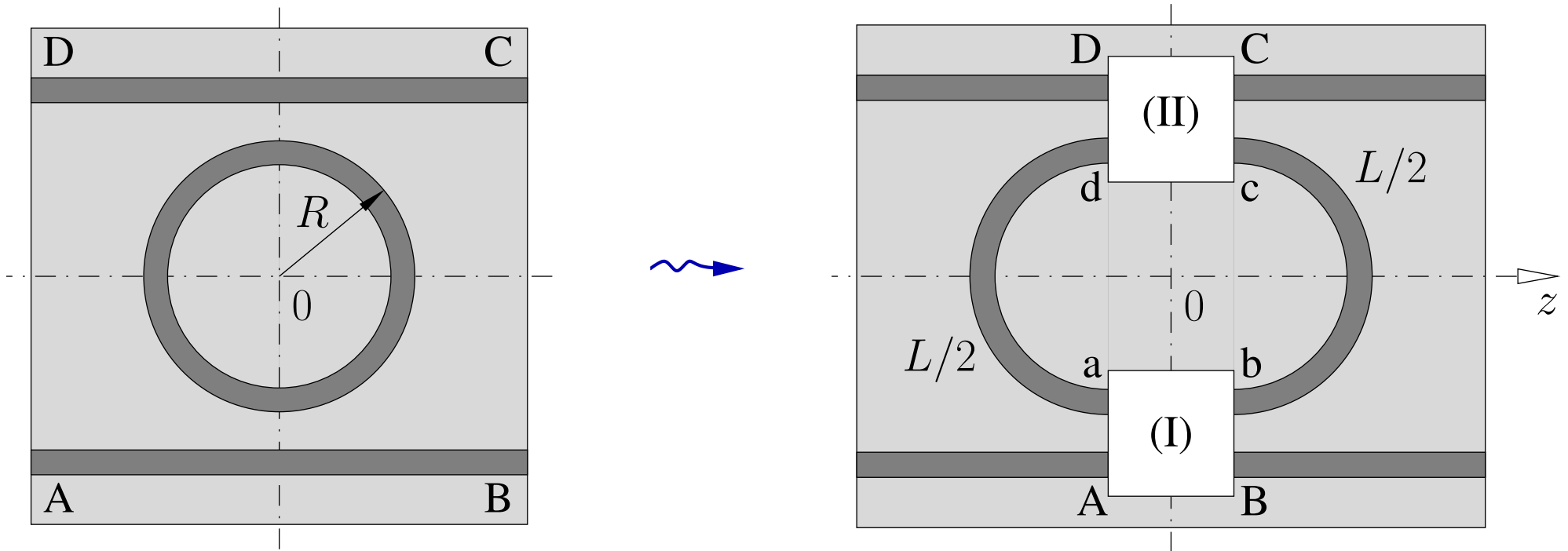
- Abstract model & examples
- Waveguide facets
- Slab mode resonances
- Extensions



Ringresonator: Abstract model

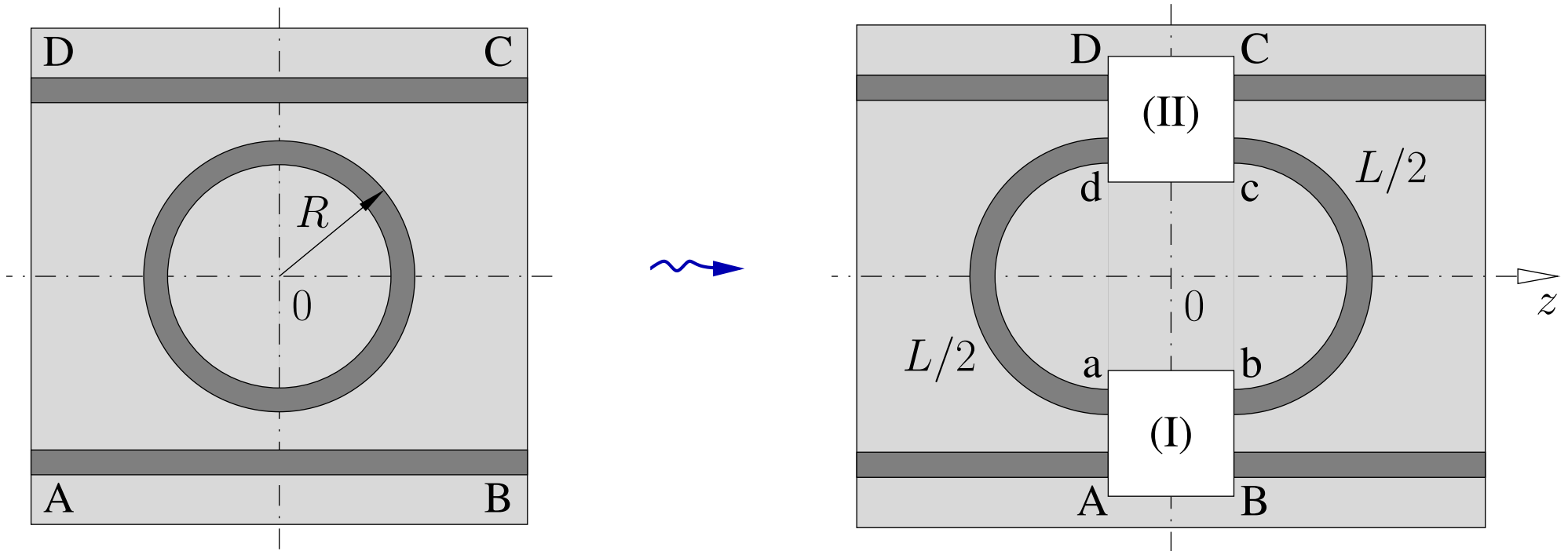


Ringresonator: Abstract model



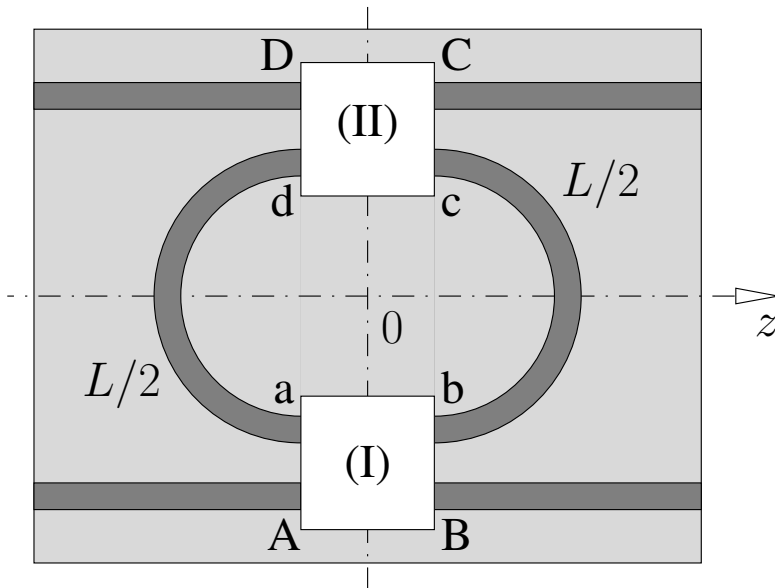
- Ringresonator \approx 2 couplers + 2 cavity segments

Ringresonator: Abstract model



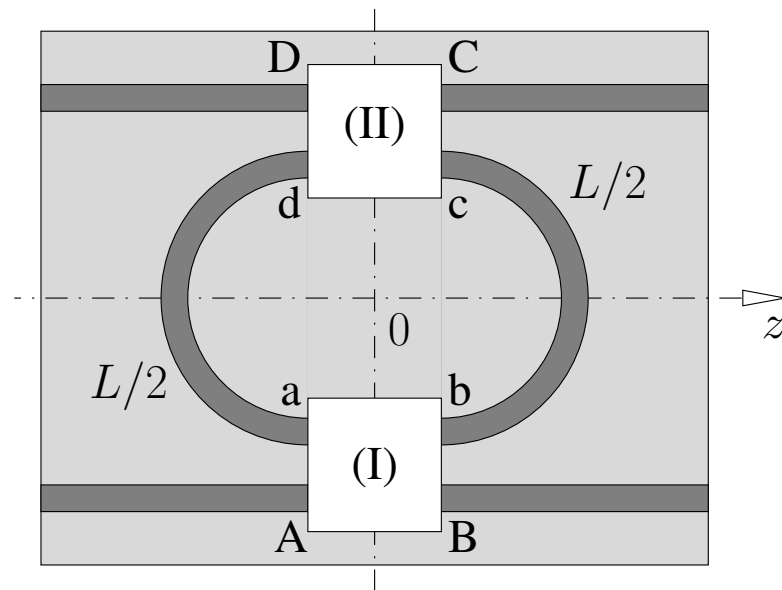
- Ringresonator \approx 2 couplers + 2 cavity segments
- CW description: $\mathbf{E}, \mathbf{H} \sim e^{i\omega t}$, $\omega = kc$, $k = 2\pi/\lambda$.

Couplers: Scattering matrices



- Uniform polarization, single mode waveguides.
- Linear, nonmagnetic (attenuating) elements.
- Backreflections are negligible.
- Interaction restricted to the couplers \leftrightarrow “port” definition.

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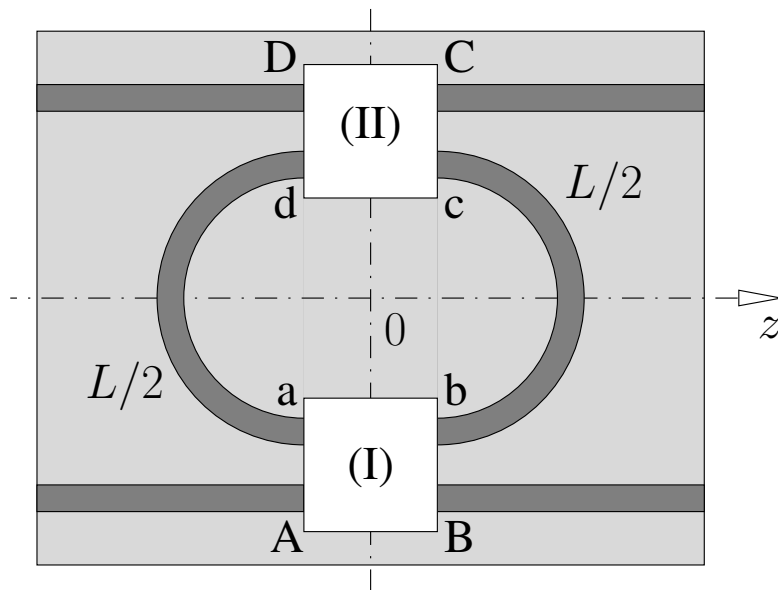
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↪ *Symmetric coupler scattering matrices :*

$$\begin{pmatrix} A_- \\ a_- \\ B_+ \\ b_+ \end{pmatrix} = \begin{pmatrix} 0 & 0 & \rho & \kappa \\ 0 & 0 & \chi & \tau \\ \rho & \chi & 0 & 0 \\ \kappa & \tau & 0 & 0 \end{pmatrix} \begin{pmatrix} A_+ \\ a_+ \\ B_- \\ b_- \end{pmatrix}$$

$A_{\pm}, B_{\pm}, a_{\pm}, b_{\pm}$: Amplitudes of waves traveling in $\pm z$ -direction.

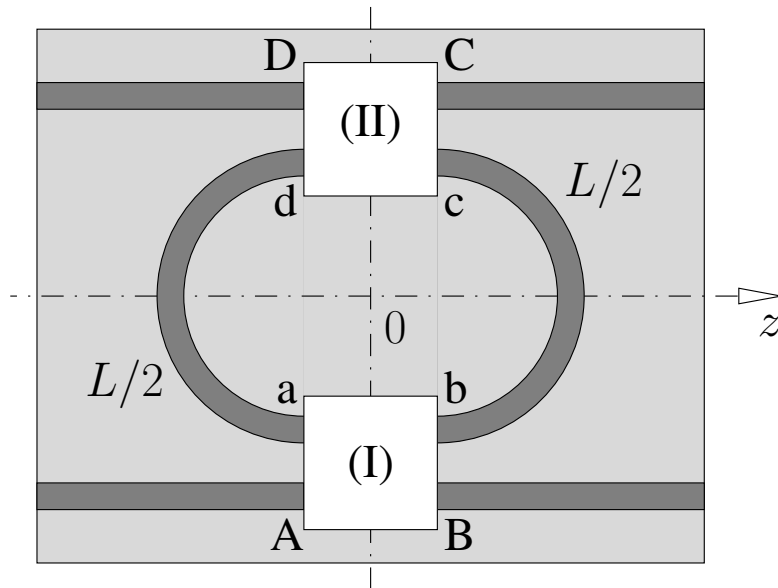
Coupler symmetries



Symmetry $z \rightarrow -z$:

$$A_+ \rightarrow b_+ \stackrel{!}{=} B_- \rightarrow a_-$$

Coupler symmetries

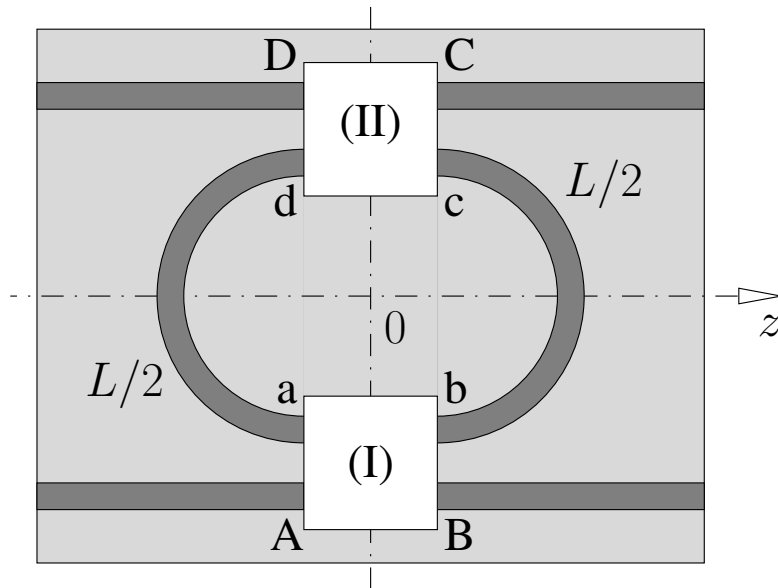


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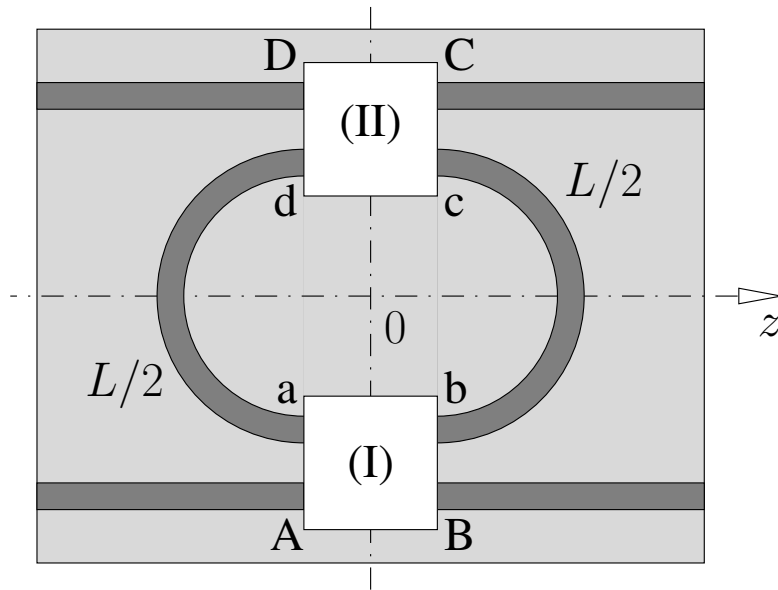


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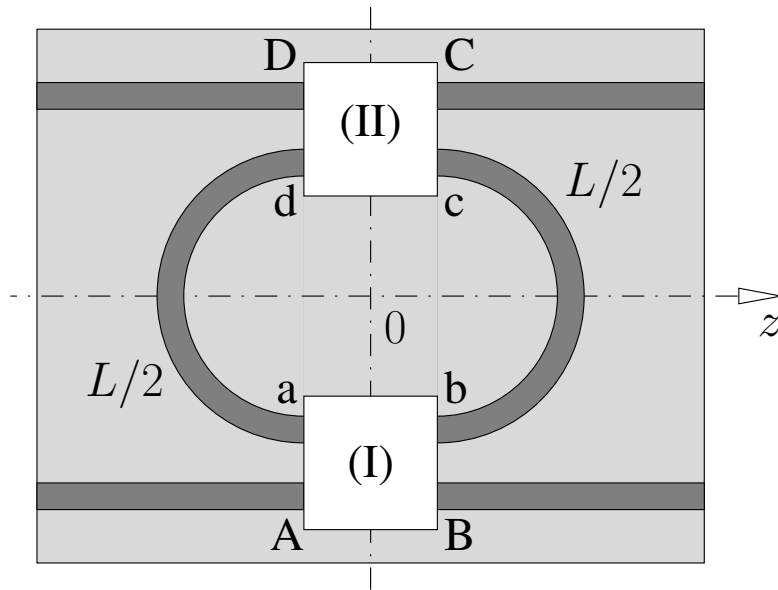
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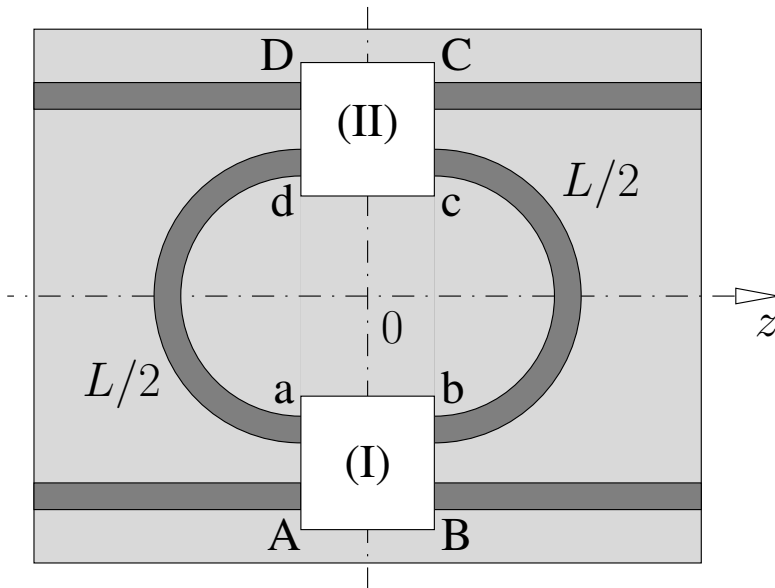
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Symmetry $x \rightarrow -x$, (I) = (II):

$$\hookrightarrow \begin{pmatrix} D_- \\ d_- \end{pmatrix} = \begin{pmatrix} \rho & \kappa \\ \kappa & \tau \end{pmatrix} \begin{pmatrix} C_- \\ c_- \end{pmatrix}, \quad \begin{pmatrix} C_+ \\ c_+ \end{pmatrix} = \begin{pmatrix} \rho & \kappa \\ \kappa & \tau \end{pmatrix} \begin{pmatrix} D_+ \\ d_+ \end{pmatrix}.$$

Cavity segments

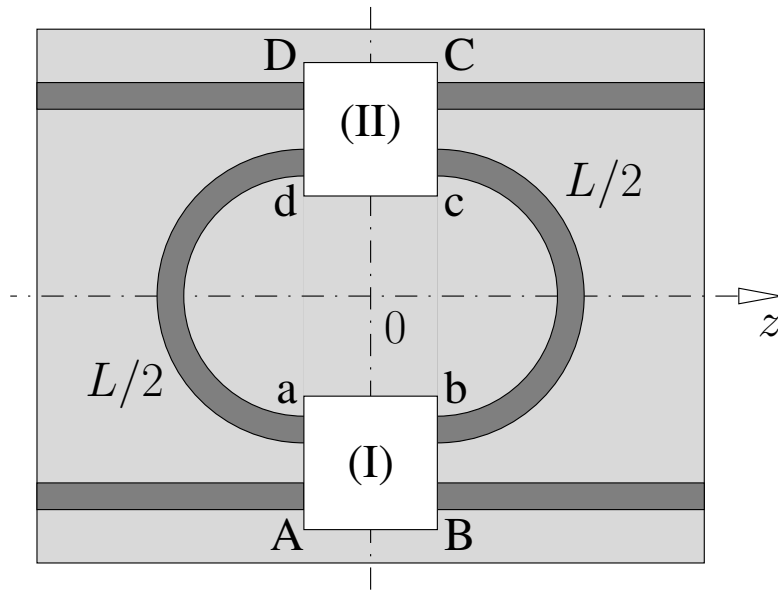


Field evolution $\sim e^{-i\gamma s}$
along the cavity core,
propagation distance s .

$$\gamma = \beta - i\alpha,$$

β : phase propagation constant,
 α : attenuation constant.

Cavity segments



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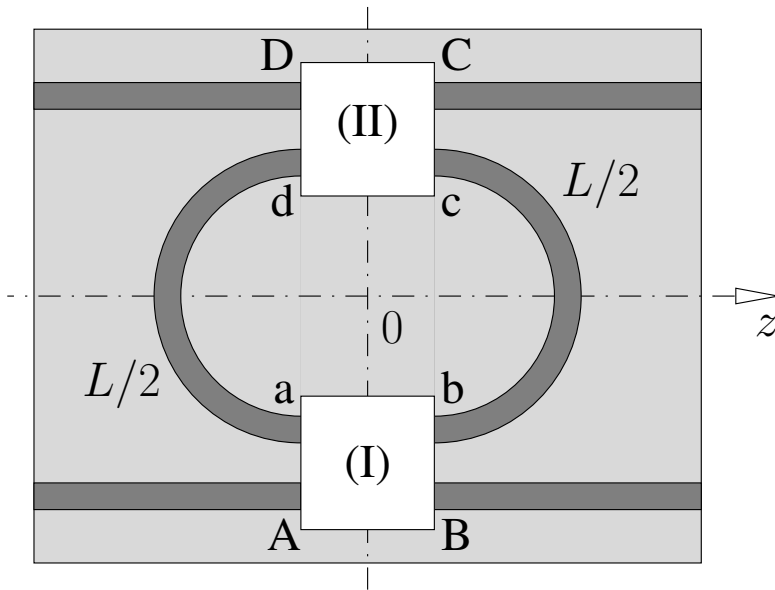
$$\gamma = \beta - i\alpha,$$

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↪ Relations of amplitudes at the ends of the cavity segments :

$$\begin{aligned} c_- &= b_+ e^{-i\beta L/2} e^{-\alpha L/2}, & a_+ &= d_- e^{-i\beta L/2} e^{-\alpha L/2}, \\ b_- &= c_+ e^{-i\beta L/2} e^{-\alpha L/2}, & d_+ &= a_- e^{-i\beta L/2} e^{-\alpha L/2}. \end{aligned}$$

Output amplitudes

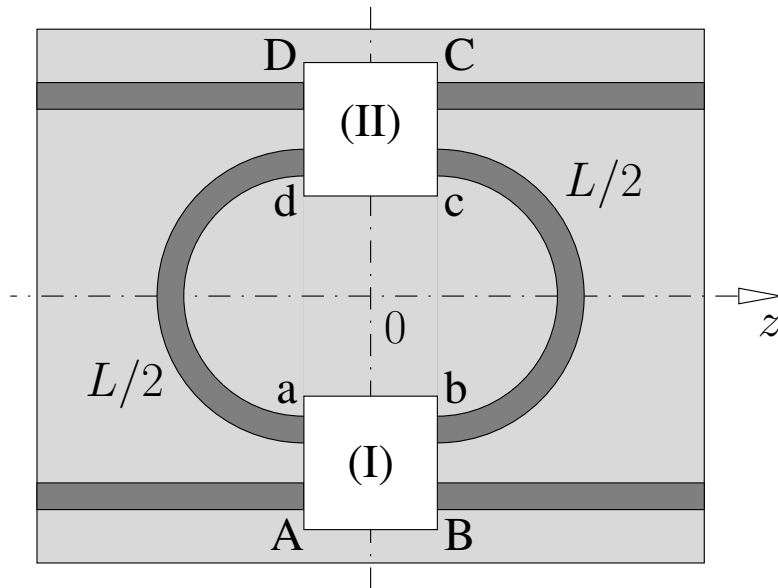


Coupler scattering matrices
+ Cavity field evolution
+ External input amplitudes

$$A_+ = \sqrt{P_{\text{in}}},$$

$$B_- = C_- = D_+ = 0$$

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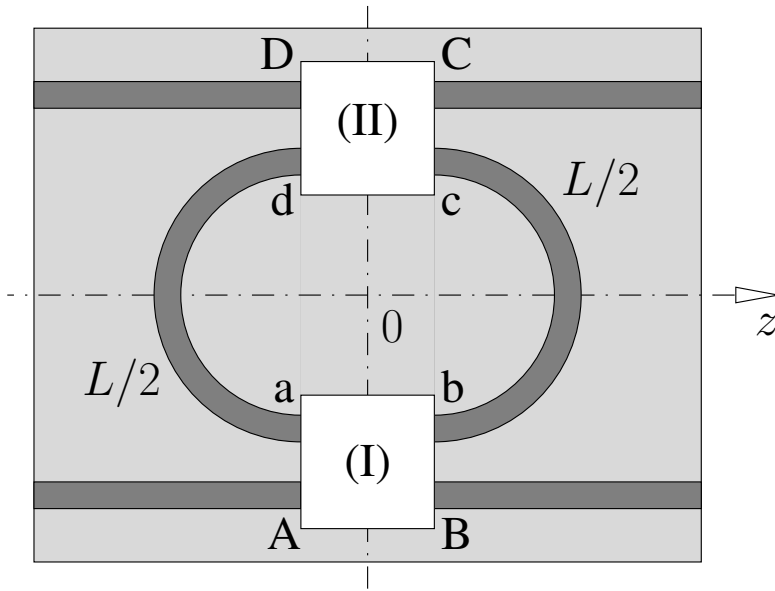
$$B_- = C_- = D_+ = 0$$

External output amplitudes :

$$A_- = 0, \quad C_+ = 0, \quad D_- = \frac{\kappa^2 p}{1 - \tau^2 p^2} A_+, \quad B_+ = \left(\rho + \frac{\kappa^2 \tau p^2}{1 - \tau^2 p^2} \right) A_+,$$

$$p = e^{-i\beta L/2} e^{-\alpha L/2}.$$

Power transfer



Power drop : $P_D = |D_-|^2,$

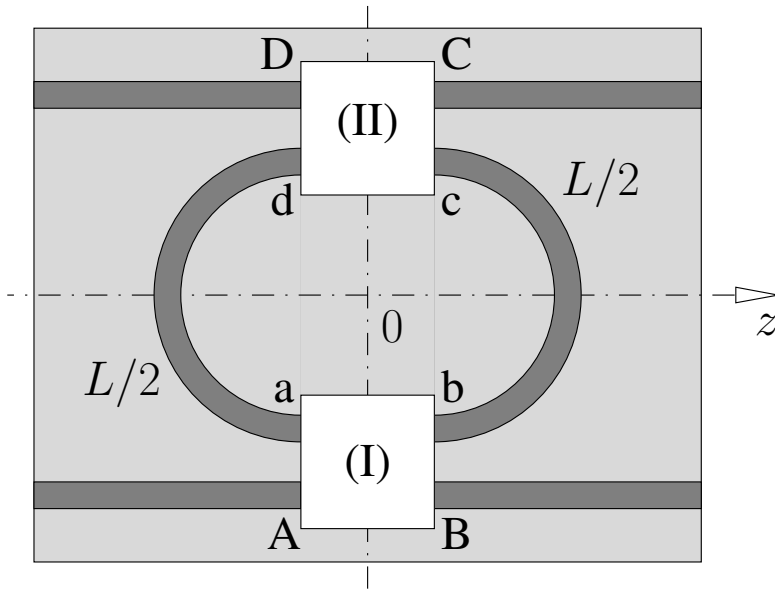
Transmission : $P_T = |B_-|^2.$

$$P_D = P_{\text{in}} \frac{|\kappa|^4 e^{-\alpha L}}{1 + |\tau|^4 e^{-2\alpha L} - 2|\tau|^2 e^{-\alpha L} \cos(\beta L - 2\varphi)}$$

$$P_T = P_{\text{in}} \frac{|\rho|^2 (1 + |\tau|^2 d^2 e^{-2\alpha L} - 2|\tau| d e^{-\alpha L} \cos(\beta L - \varphi - \psi))}{1 + |\tau|^4 e^{-2\alpha L} - 2|\tau|^2 e^{-\alpha L} \cos(\beta L - 2\varphi)}$$

$$d e^{i\psi} := \tau - \kappa^2 / \rho,$$

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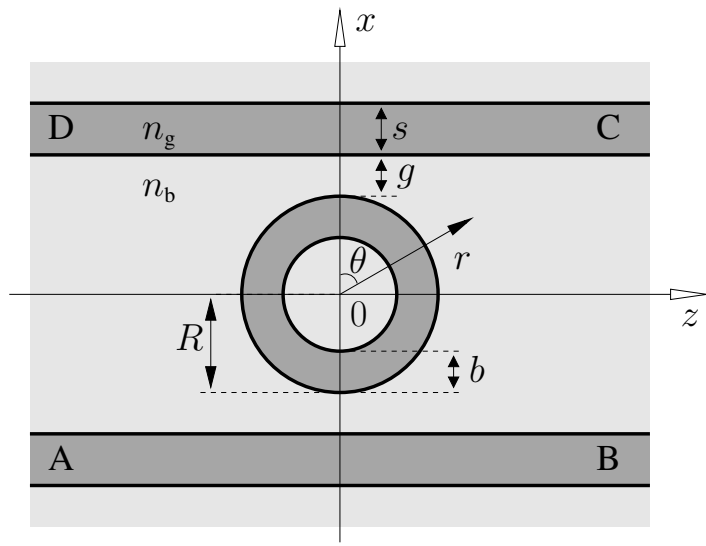
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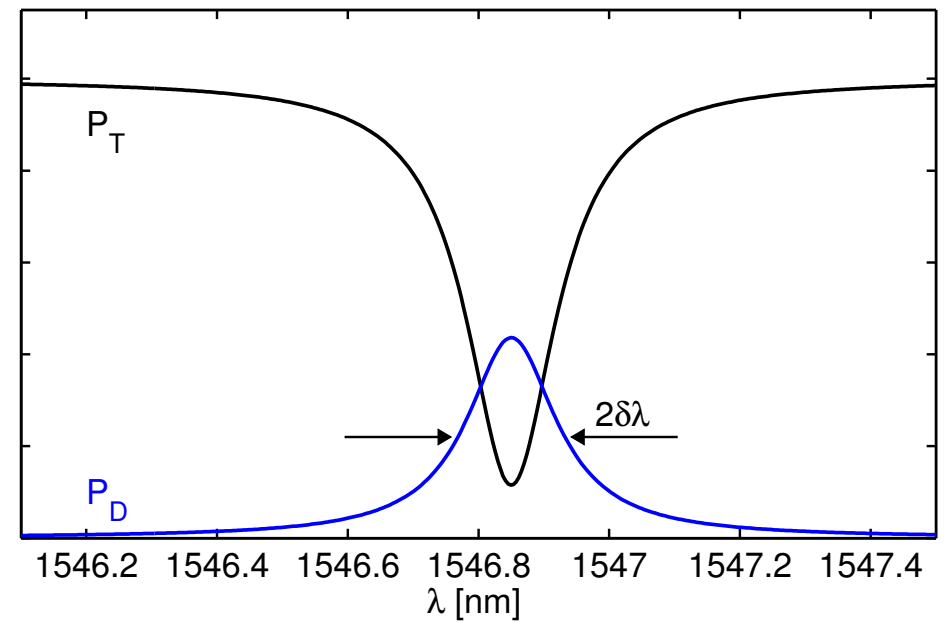
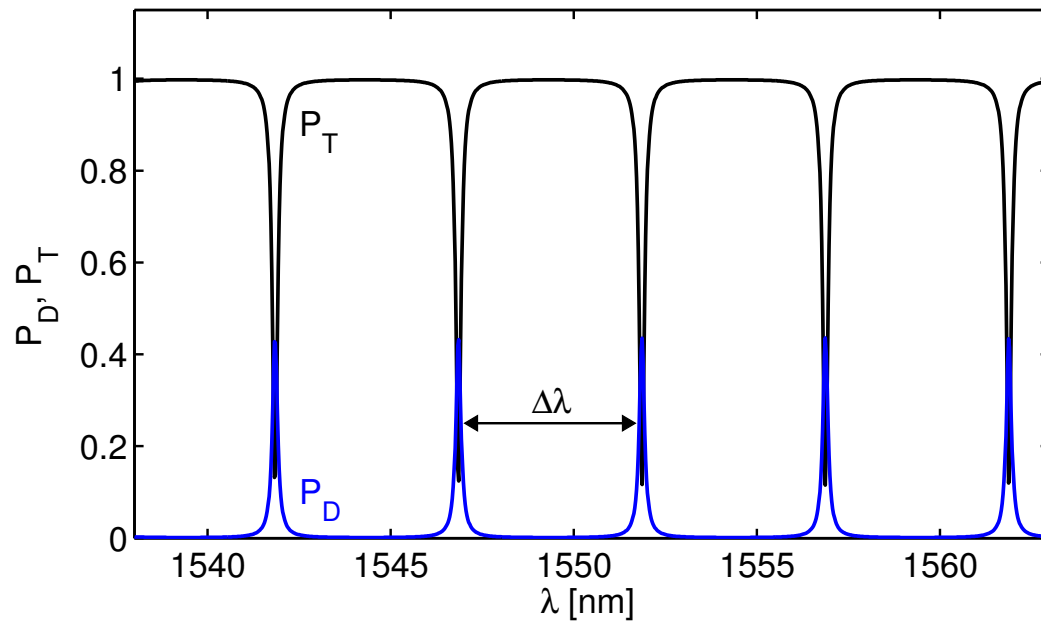
$$d e^{i\psi} := \tau - \kappa^2 / \rho, \quad L \neq 2\pi R.$$

Spectral response



$R = 50 \mu\text{m}$, $b = s = 1.0 \mu\text{m}$, $g = 0.9 \mu\text{m}$,
 $n_b = 1.45$, $n_g = 1.60$; 2D, TE.

$\Delta\lambda = 5.0 \text{ nm}$, $2\delta\lambda = 0.17 \text{ nm}$,
 $F = 30$, $Q = 9400$, $P_{D,\text{res}} = 0.44$.



Resonances

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 $\beta L - 2\varphi = \beta L_{\text{cav}} - \phi$, $\phi = 2\beta l + 2\varphi$, $L_{\text{cav}} = 2\pi R$, $\partial_\lambda \phi \approx 0$.

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$$\beta = \frac{2m\pi + \phi}{L_{\text{cav}}} =: \beta_m \quad \text{integer } m; \quad P_D|_{\beta=\beta_m} = P_{\text{in}} \frac{|\kappa|^4 e^{-\alpha L}}{(1 - |\tau|^2 e^{-\alpha L})^2}.$$

Free spectral range

- Resonance next to β_m :

$$\beta_{m-1} = \frac{2(m-1)\pi + \phi}{L_{\text{cav}}} = \beta_m - \frac{2\pi}{L_{\text{cav}}}$$

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q_j : waveguide parameters with dimension length,

$$\beta(a\lambda, aq_j) = \beta(\lambda, q_j)/a, \quad \partial_a |_{a=1}$$

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$$\text{FSR :} \quad \Delta \lambda = -\frac{2\pi}{L_{\text{cav}}} \left(\left. \frac{\partial \beta}{\partial \lambda} \right|_m \right)^{-1} \approx \frac{\lambda^2}{n_{\text{eff}} L_{\text{cav}}} \Big|_m, \quad n_{\text{eff}} = \beta/k.$$

Spectral width of the resonances

- $$P_D = P_{\text{in}} \frac{|\kappa|^4 e^{-\alpha L}}{1 + |\tau|^4 e^{-2\alpha L} - 2|\tau|^2 e^{-\alpha L} \cos(\beta L_{\text{cav}} - \phi)},$$
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FWHM:
$$2\delta\lambda = \frac{\lambda^2}{\pi L_{\text{cav}} n_{\text{eff}}} \bigg|_m \left(\frac{1}{|\tau|} e^{\alpha L/2} - |\tau| e^{-\alpha L/2} \right).$$

Finesse & Q-factor

Finesse :

$$F = \frac{\Delta\lambda}{2\delta\lambda} = \pi \frac{|\tau| e^{-\alpha L/2}}{1 - |\tau|^2 e^{-\alpha L}} .$$

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$$Q = \frac{\lambda}{2\delta\lambda} = \pi \frac{n_{\text{eff}} L_{\text{cav}}}{\lambda} \frac{|\tau| e^{-\alpha L/2}}{1 - |\tau|^2 e^{-\alpha L}} = \frac{n_{\text{eff}} L_{\text{cav}}}{\lambda} F .$$

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or

$$Q = k R n_{\text{eff}} F \quad \text{for} \quad L_{\text{cav}} = 2\pi R .$$

Performance versus coupling length & losses

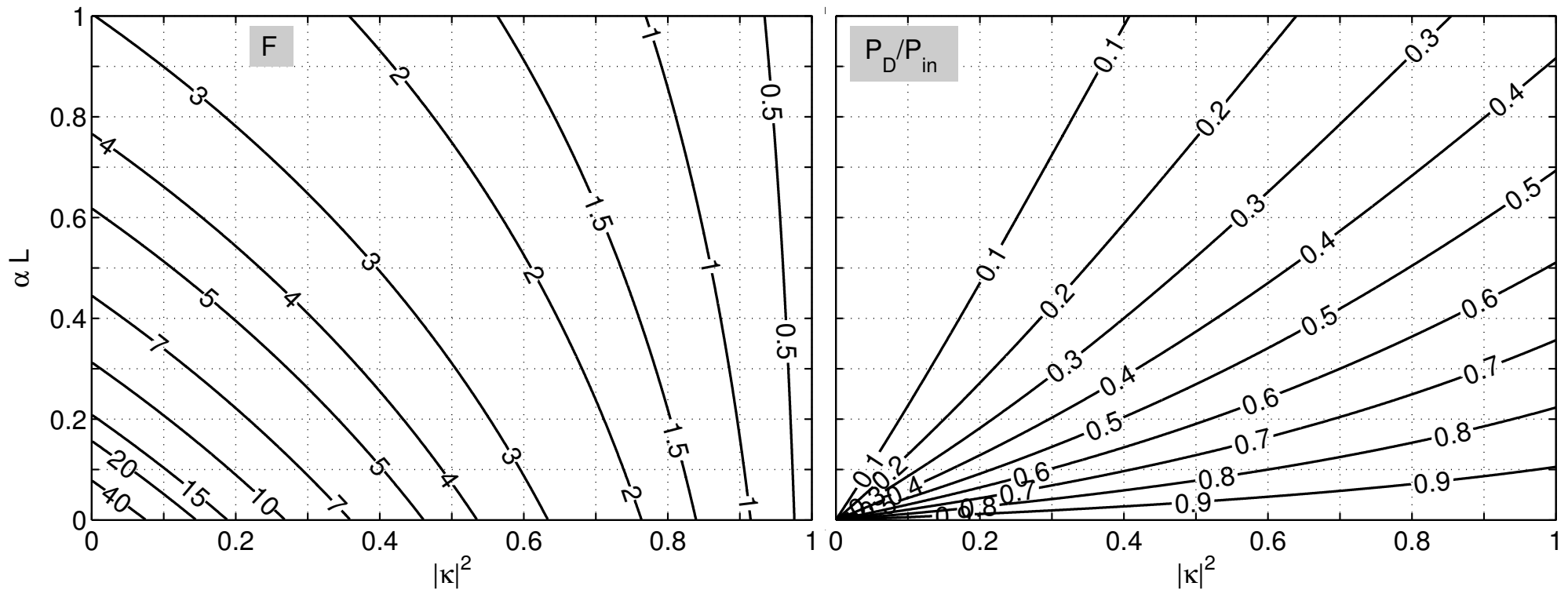
Assumption : Lossless coupler elements, $|\rho|^2 = |\tau|^2 = 1 - |\kappa|^2$.


$$F = \pi \frac{(\sqrt{1 - |\kappa|^2}) e^{-\alpha L/2}}{1 - (1 - |\kappa|^2) e^{-\alpha L}} , \quad P_{\text{D}}|_{\text{res}} = P_{\text{in}} \frac{|\kappa|^4 e^{-\alpha L}}{(1 - (1 - |\kappa|^2) e^{-\alpha L})^2} .$$

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Assumption: Lossless coupler elements, $|\rho|^2 = |\tau|^2 = 1 - |\kappa|^2$.

↪
$$F = \pi \frac{(\sqrt{1 - |\kappa|^2}) e^{-\alpha L/2}}{1 - (1 - |\kappa|^2) e^{-\alpha L}}, \quad P_D|_{\text{res}} = P_{\text{in}} \frac{|\kappa|^4 e^{-\alpha L}}{(1 - (1 - |\kappa|^2) e^{-\alpha L})^2}.$$



Tuning

- Resonance condition: $\beta = (2\pi m + \phi)/L_{\text{cav}} = \beta_m$,
a peak at λ_m : $\beta(\lambda_m) = \beta_m$.

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$$\hookrightarrow \beta(p, \tilde{\lambda}_m) \approx \beta(0, \lambda_m) + p \left. \frac{\partial \beta}{\partial p} \right|_{0, \lambda_m} + (\tilde{\lambda}_m - \lambda_m) \left. \frac{\partial \beta}{\partial \lambda} \right|_{0, \lambda_m} = \beta_m .$$

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Wavelength shift effected by the perturbation :

$$\Delta_p \lambda_m = p \frac{\partial \beta}{\partial p} \frac{\lambda_m}{\beta_m} \quad \text{or} \quad \Delta_p \lambda_m = p \frac{\partial \beta}{\partial p} \frac{\lambda_m^2}{2\pi n_{\text{eff},m}} .$$

Tuning, specific

- Electrooptic tuning,
an external field strength E_t changes the cavity permittivity :

$$\hat{\epsilon}(E_t) = \hat{\epsilon}(0) + E_t \hat{e}.$$

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mode profile $\mathbf{E} = (E_x, E_y, iE_z)$, $\mathbf{H} = (H_x, H_y, iH_z)$

$$\hookrightarrow \frac{\partial \beta}{\partial E_t} = \frac{\omega \epsilon_0}{2} \frac{\iint \mathbf{E}^* \hat{e} \mathbf{E} \, dx dy}{\iint (E_x H_y - E_y H_x) \, dx dy}.$$

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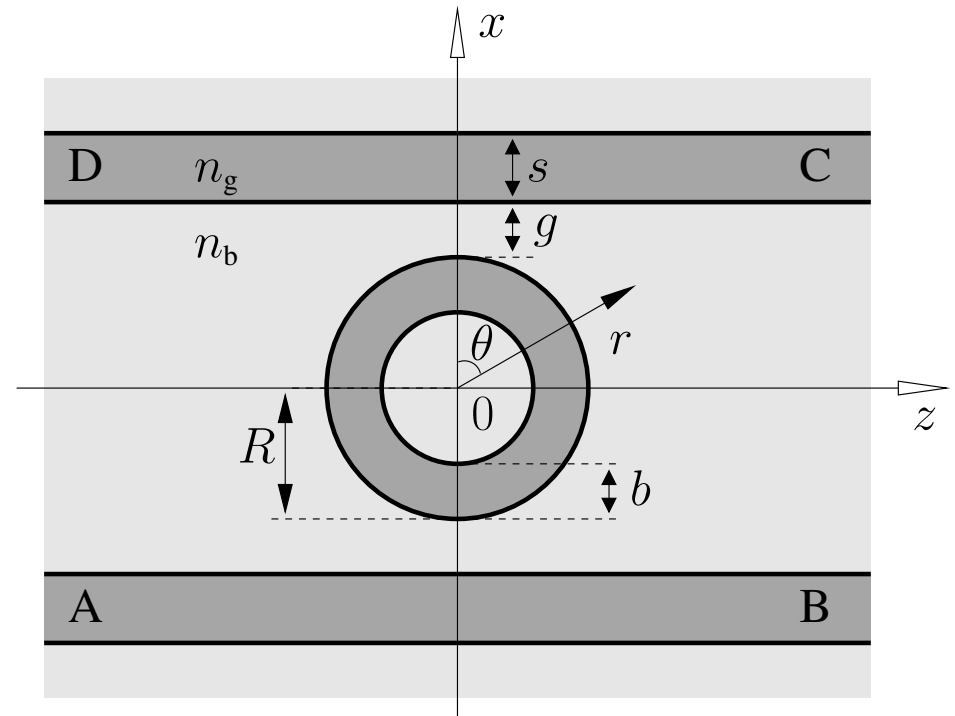
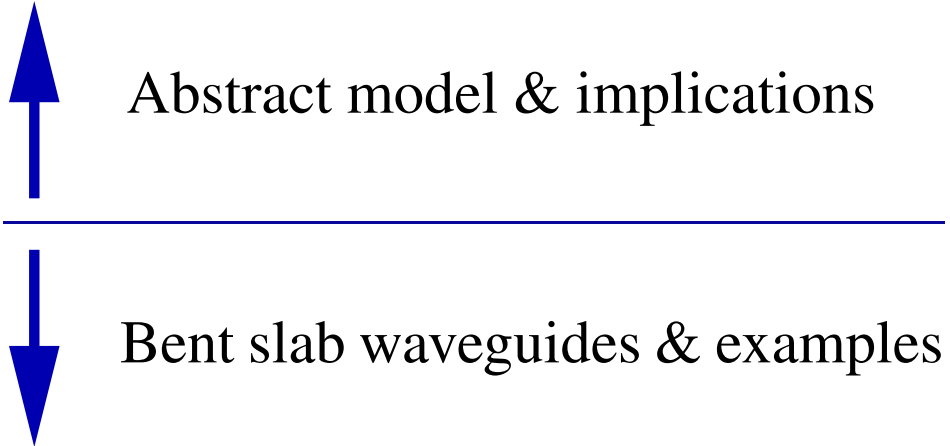
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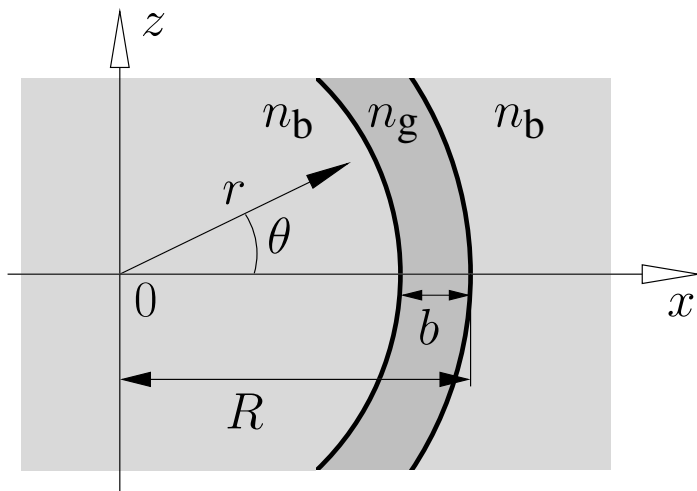
Wavelength shift effected by the electrooptic tuning :

$$\Delta_{E_t} \lambda = E_t \frac{\lambda}{2 n_{\text{eff}}} \sqrt{\frac{\epsilon_0}{\mu_0}} \frac{\iint \mathbf{E}^* \hat{e} \mathbf{E} \, dx dy}{\iint (E_x H_y - E_y H_x) \, dx dy}.$$

...

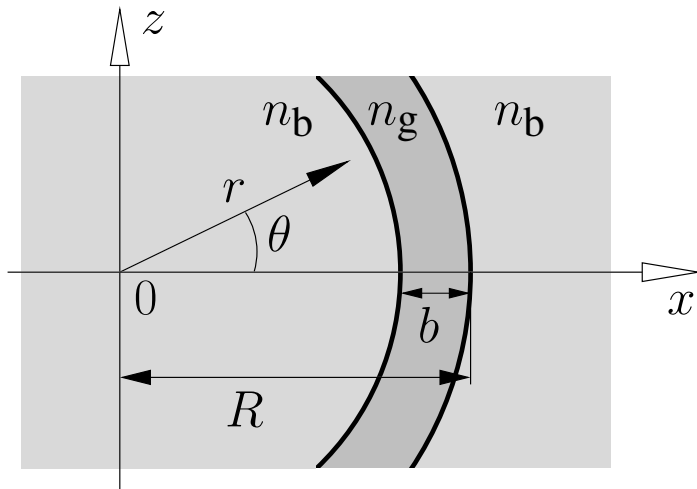


Bend mode properties



Homogeneity along θ

Bend mode properties

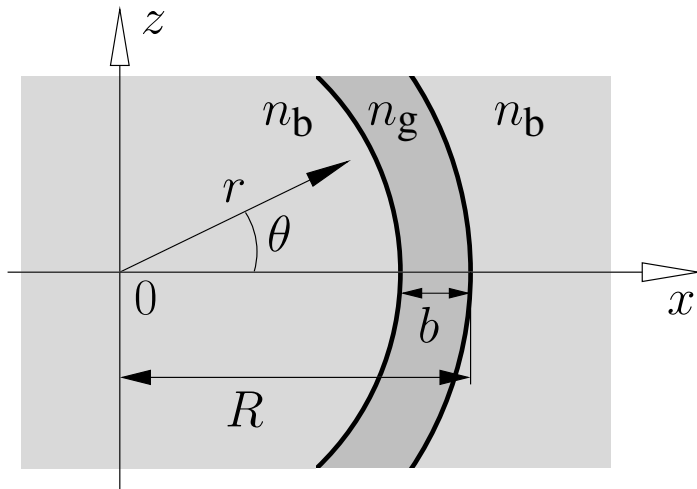


Homogeneity along θ \rightsquigarrow bend mode ansatz

$$\begin{pmatrix} \mathcal{E} \\ \mathcal{H} \end{pmatrix}(r, \theta, t) = \frac{1}{2} \text{Re} \left(\begin{pmatrix} \mathbf{E}_0^b \\ \mathbf{H}_0^b \end{pmatrix}(r) e^{i\omega t - i\gamma R\theta} \right),$$

profile \mathbf{E}_0^b , \mathbf{H}_0^b ,
propagation constant $\gamma = \beta - i\alpha$.

Bend mode properties



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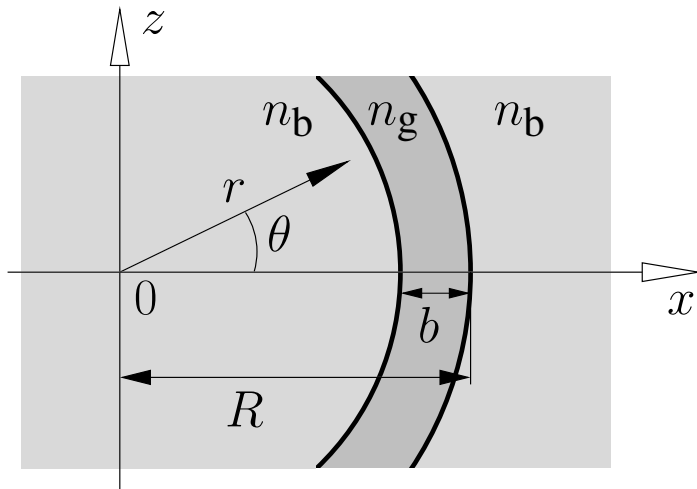
profile $\mathbf{E}_0^b, \mathbf{H}_0^b$,
propagation constant $\gamma = \beta - i\alpha$.



$$\frac{d^2\phi}{dr^2} + \frac{1}{r} \frac{d\phi}{dr} + \left(k^2 n^2 - \frac{\gamma^2 R^2}{r^2} \right) \phi = 0,$$

$n(r)$: piecewise constant, $\phi = E_{0,y}^b$ (TE), $\phi = H_{0,y}^b$ (TM).

Bend mode properties



Homogeneity along $\theta \rightsquigarrow$ bend mode ansatz

$$\begin{pmatrix} \mathcal{E} \\ \mathcal{H} \end{pmatrix}(r, \theta, t) = \frac{1}{2} \text{Re} \begin{pmatrix} \mathbf{E}_0^b \\ \mathbf{H}_0^b \end{pmatrix}(r) e^{i\omega t - i\gamma R\theta},$$

profile $\mathbf{E}_0^b, \mathbf{H}_0^b$,
propagation constant $\gamma = \beta - i\alpha$.

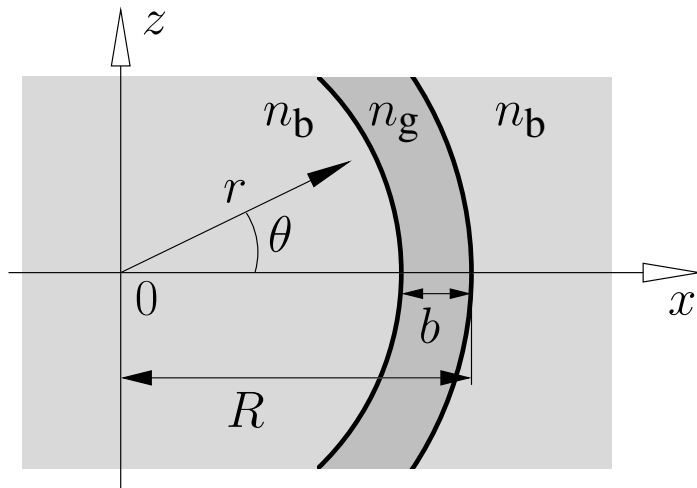


$$\frac{d^2\phi}{dr^2} + \frac{1}{r} \frac{d\phi}{dr} + \left(k^2 n^2 - \frac{\gamma^2 R^2}{r^2} \right) \phi = 0,$$

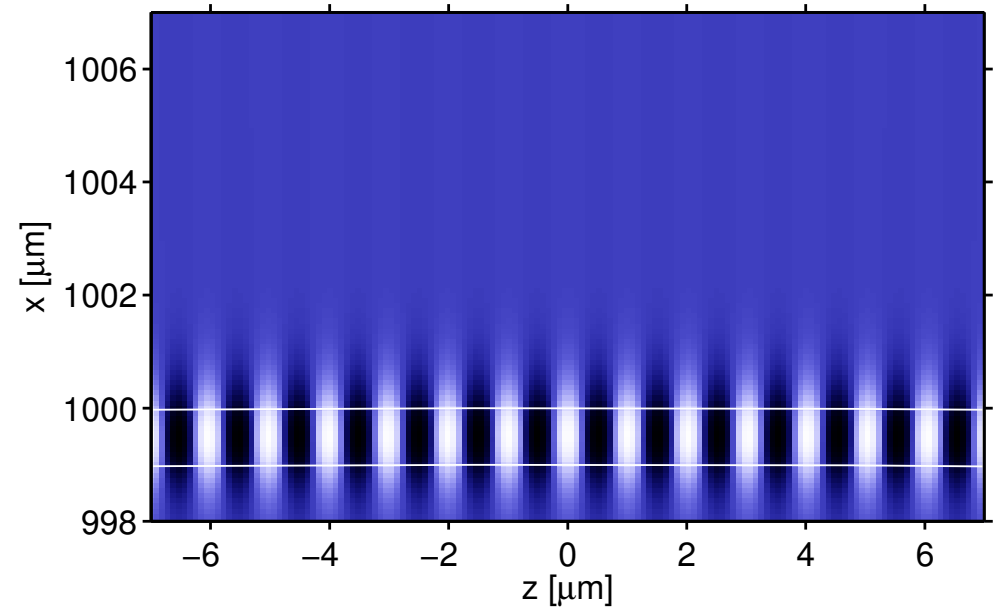
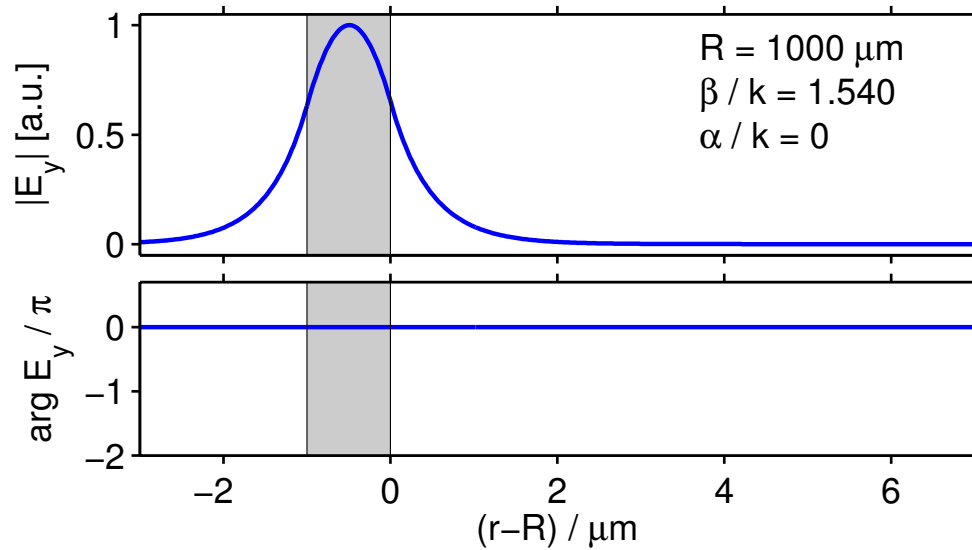
$n(r)$: piecewise constant, $\phi = E_{0,y}^b$ (TE), $\phi = H_{0,y}^b$ (TM).

- Bend modes:
- Nonzero solutions,
 - bounded at the origin, $\sim J_{\gamma R}(n_b k r)$ for $r < R - b$,
 - outgoing exterior fields, $\sim H_{\gamma R}^{(2)}(n_b k r)$ for $r > R$,
 - continuity at interfaces: ϕ & $d_r \phi$ (TE), ϕ & $(d_r \phi)/n^2$ (TM).

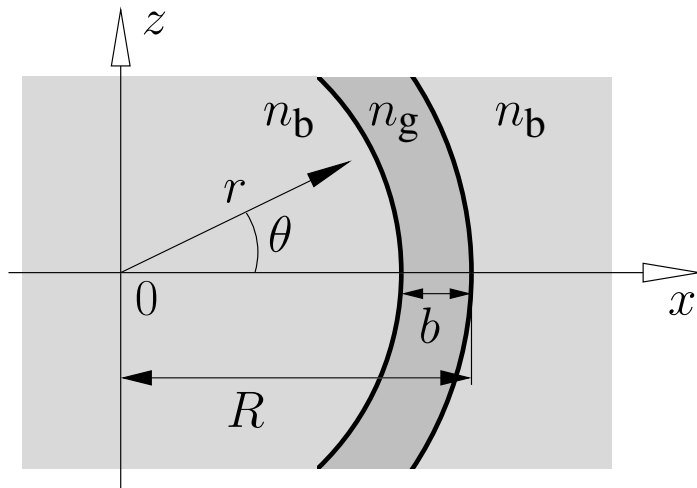
Bend modes, examples



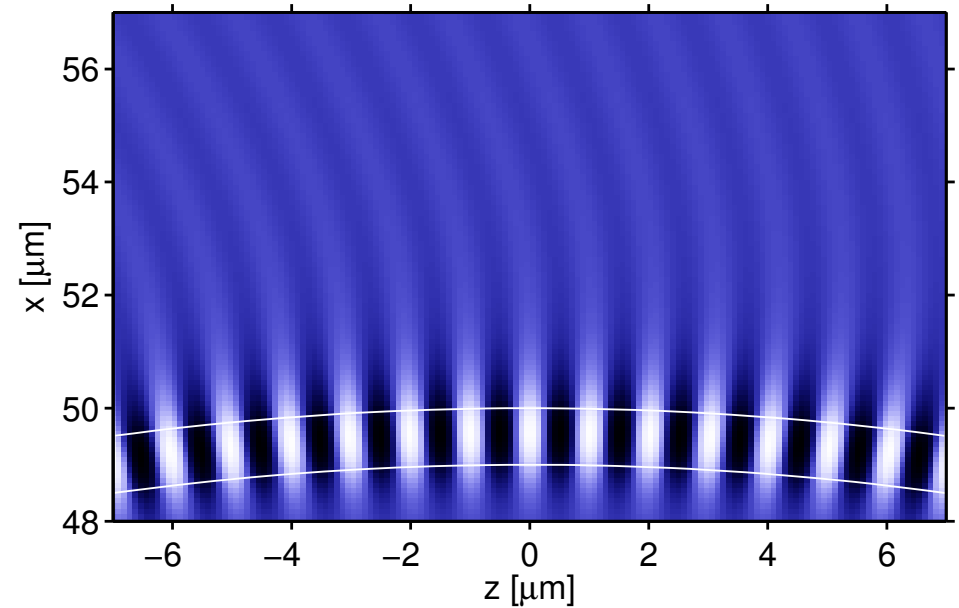
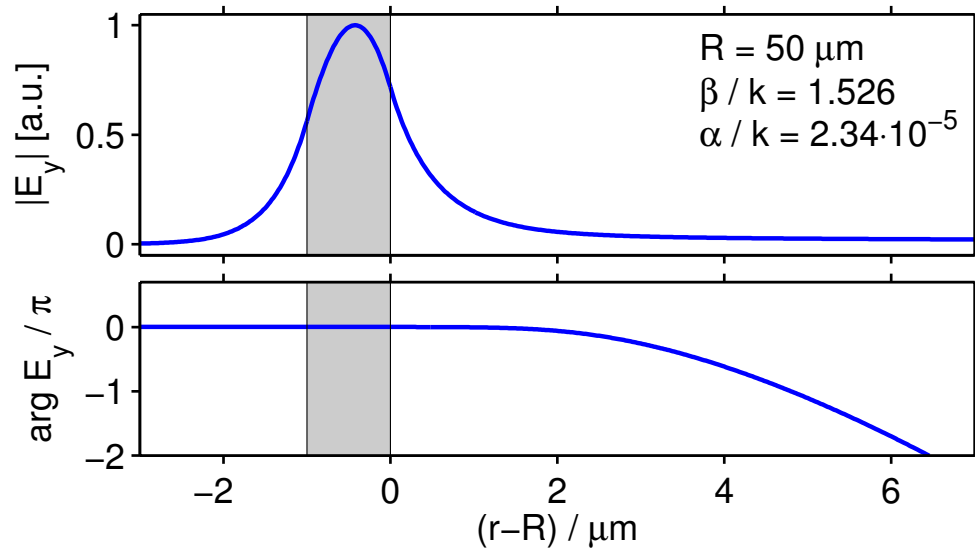
2D, TE,
 $n_b = 1.45$, $n_g = 1.60$, $b = 1.0 \mu\text{m}$, $\lambda = 1.55 \mu\text{m}$,
 $R = 1000 \mu\text{m}$.



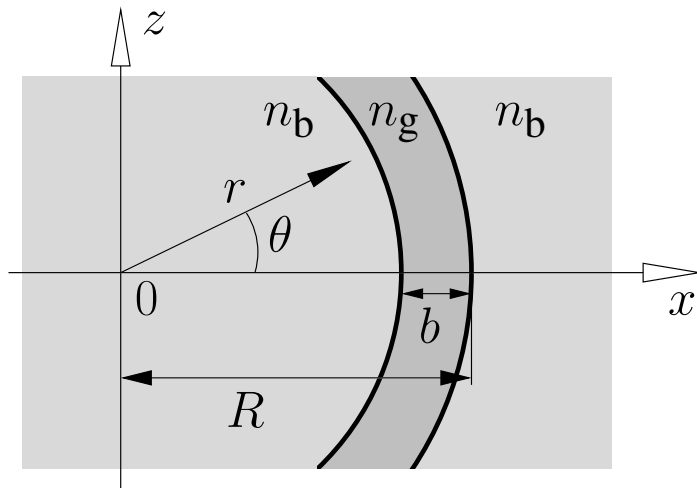
Bend modes, examples



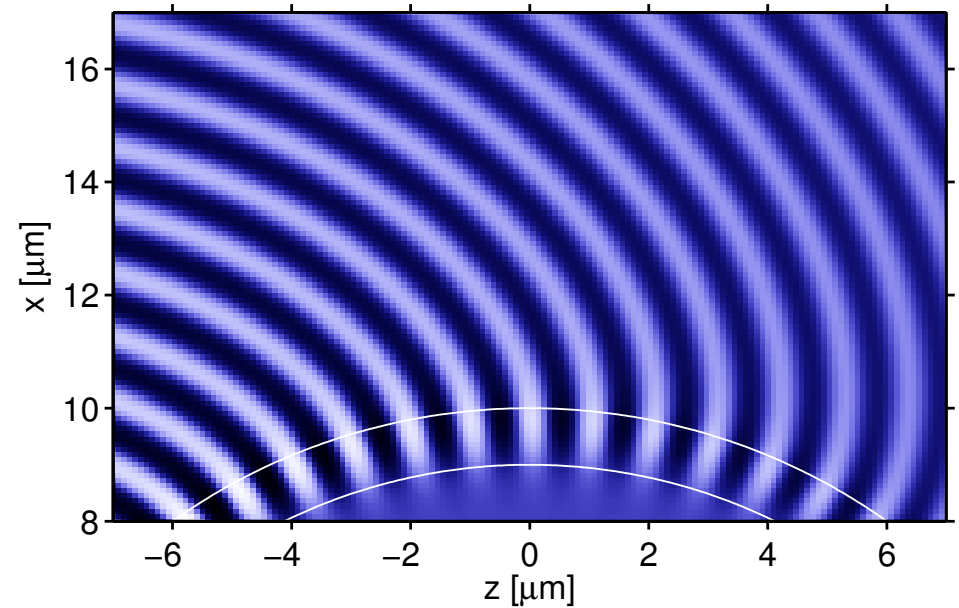
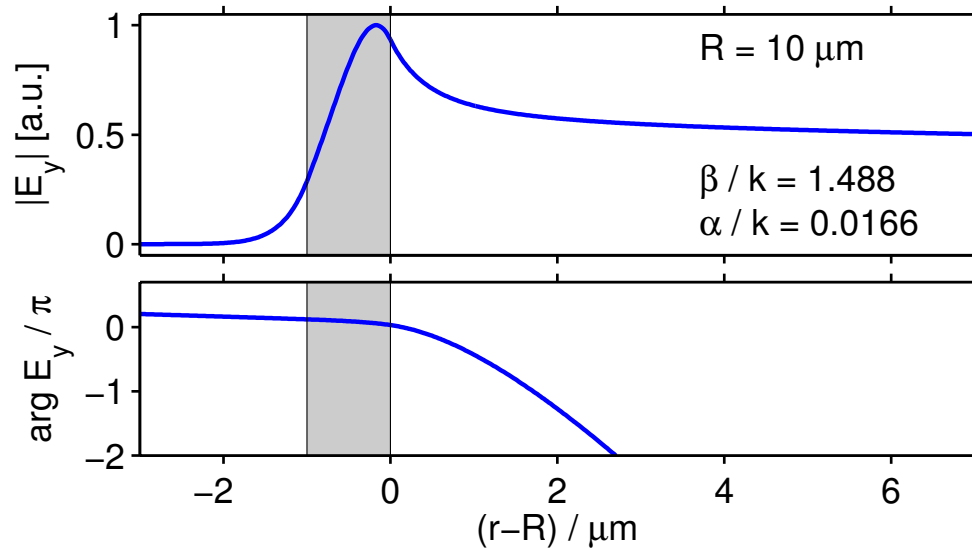
2D, TE,
 $n_b = 1.45$, $n_g = 1.60$, $b = 1.0 \mu\text{m}$, $\lambda = 1.55 \mu\text{m}$,
 $R = 50 \mu\text{m}$.



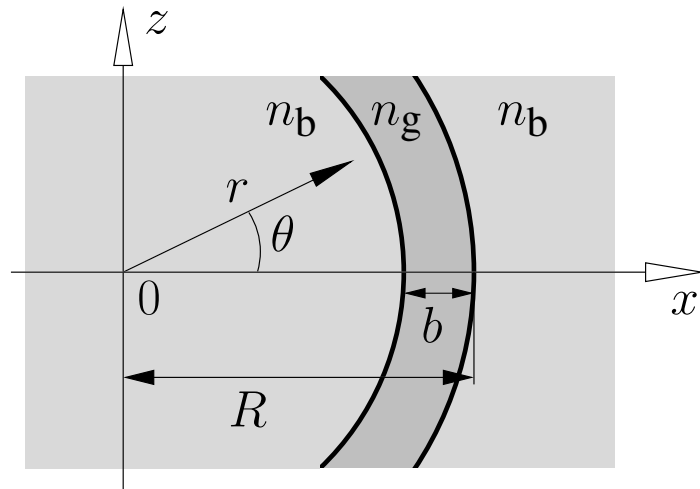
Bend modes, examples



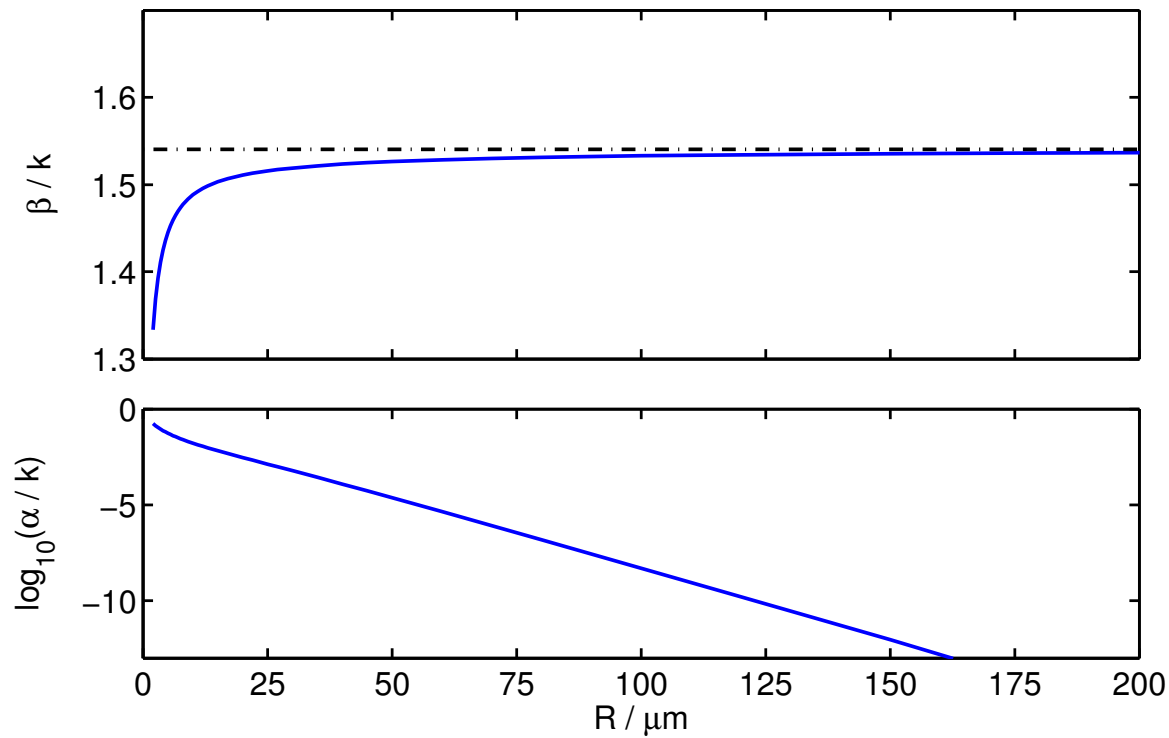
2D, TE,
 $n_b = 1.45$, $n_g = 1.60$, $b = 1.0 \mu\text{m}$, $\lambda = 1.55 \mu\text{m}$,
 $R = 10 \mu\text{m}$.



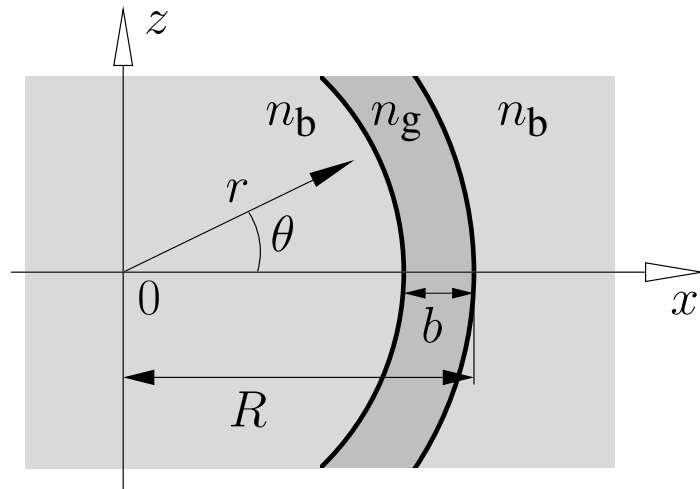
Propagation constant vs. bend radius



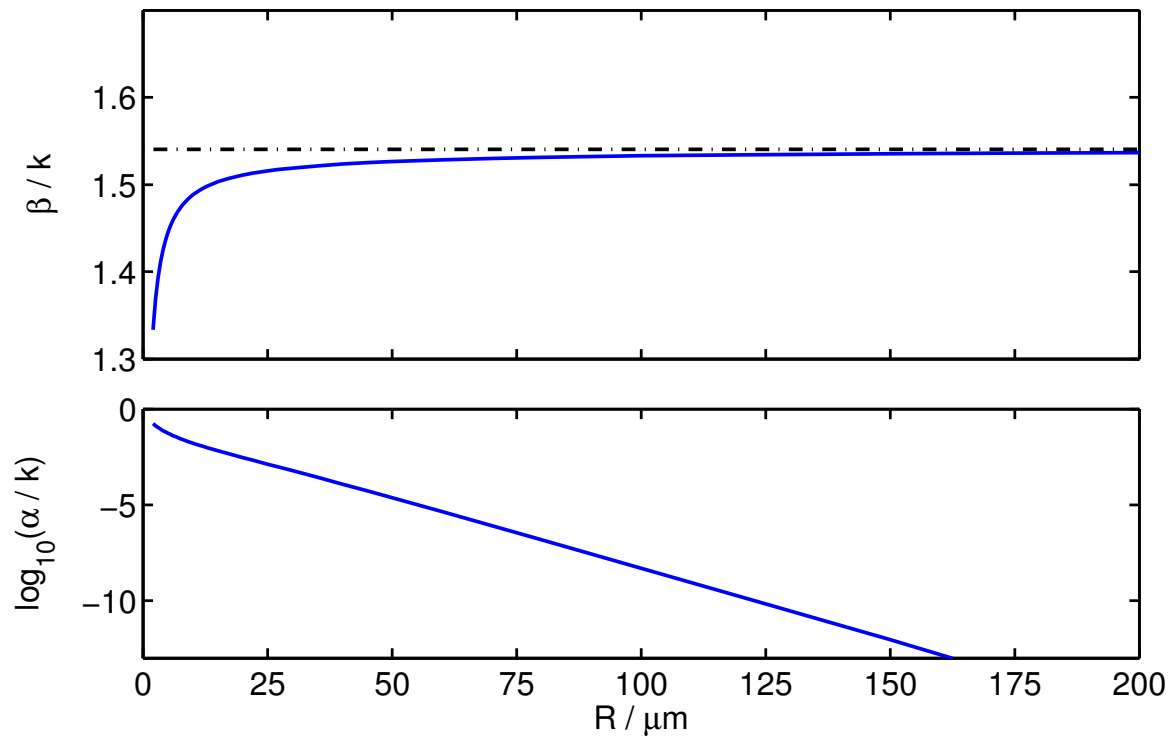
2D, TE,
 $n_b = 1.45$, $n_g = 1.60$, $b = 1.0 \mu\text{m}$, $\lambda = 1.55 \mu\text{m}$,
 $R \in [2, 200] \mu\text{m}$.



Propagation constant vs. bend radius



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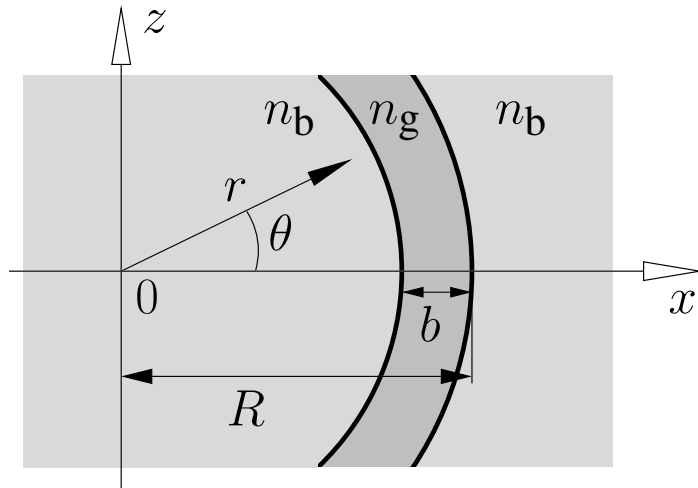
Alternative definition :
 $R' = R - b/2$.

Identical physical fields

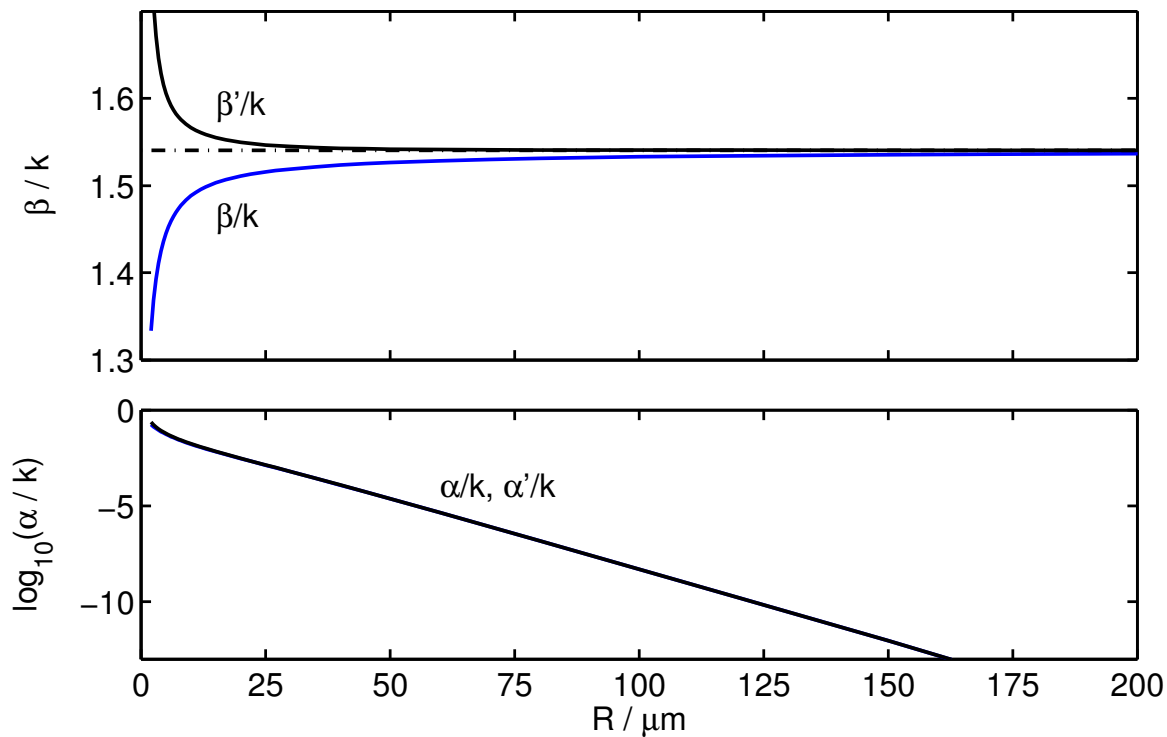
$$\gamma' R' = \gamma R,$$

$$\gamma' = \gamma \frac{R}{R - b/2}.$$

Propagation constant vs. bend radius



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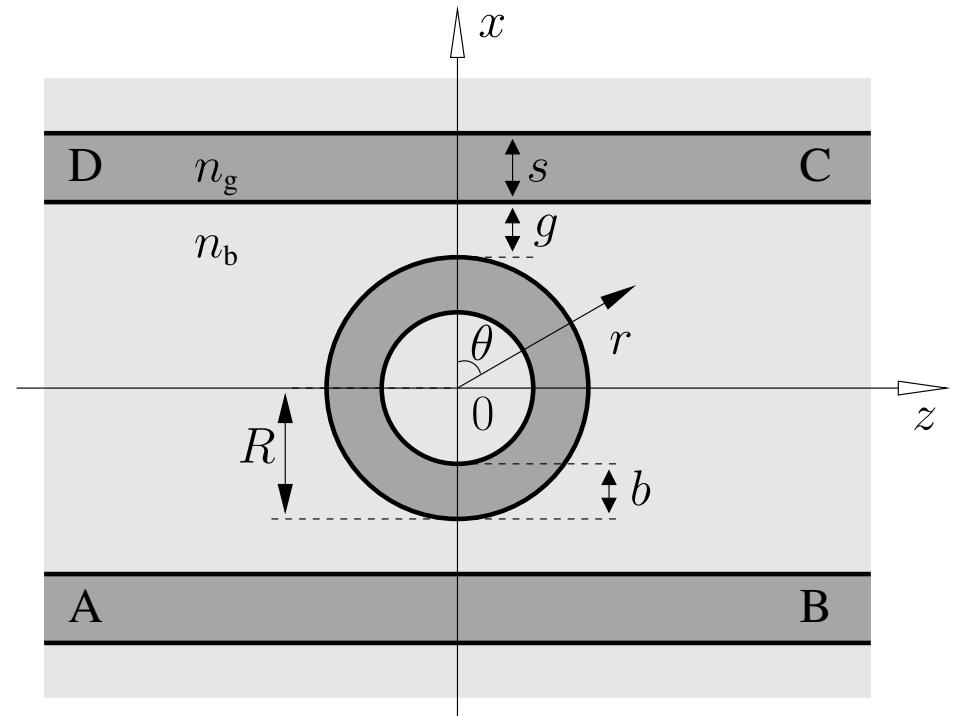
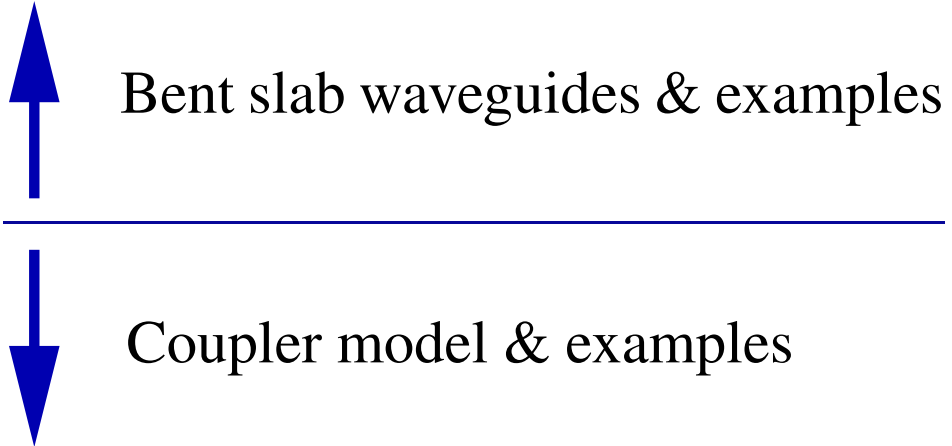
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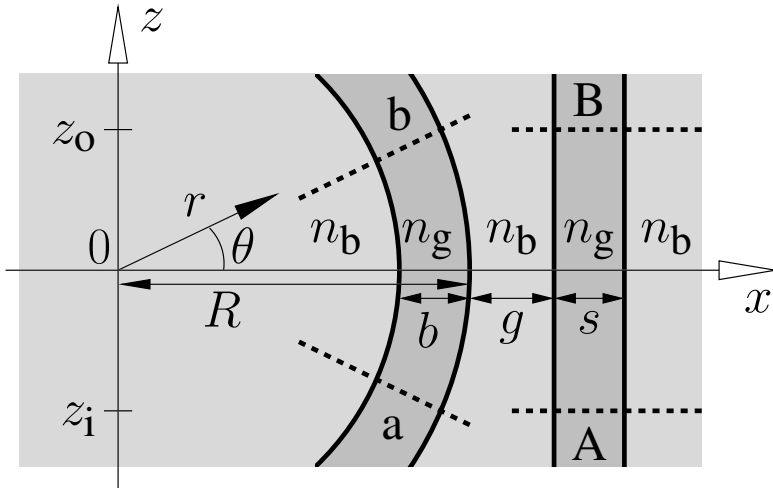
...





$$\begin{pmatrix} \mathbf{E}_s \\ \mathbf{H}_s \end{pmatrix}(x, z) = \begin{pmatrix} \mathbf{E}_0^s \\ \mathbf{H}_0^s \end{pmatrix}(x) \mathrm{e}^{-\mathrm{i}\beta_s z}.$$

Coupler modeling, CMT ansatz

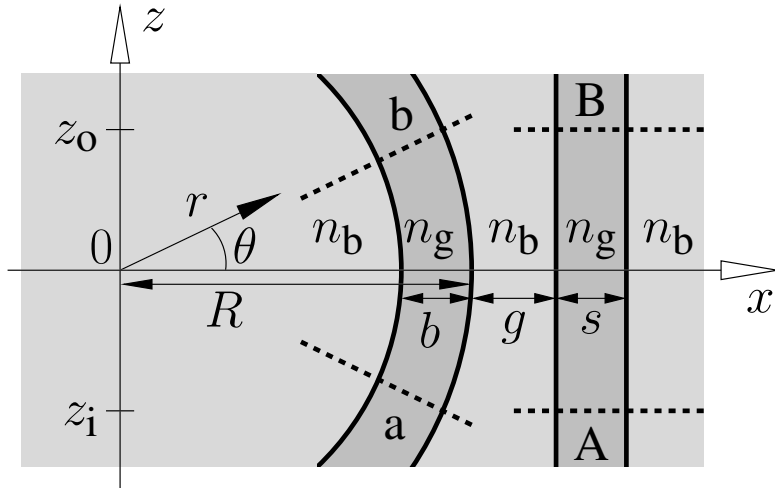


Known: Modes of the bent and straight cores

$$\begin{pmatrix} \mathbf{E}_b \\ \mathbf{H}_b \end{pmatrix}(x, z) = \begin{pmatrix} \mathbf{E}_0^b \\ \mathbf{H}_0^b \end{pmatrix}(r(x, z)) e^{-i\gamma_b R\theta(x, z)},$$

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Coupler modeling, CMT ansatz



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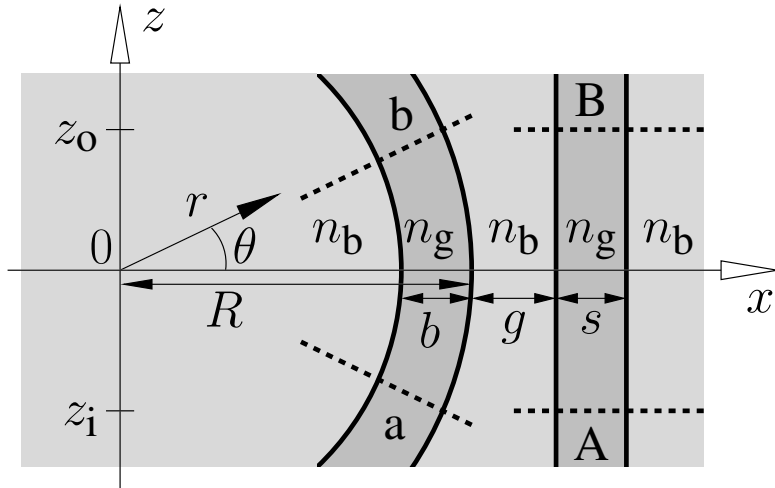
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Coupled mode ansatz:

$$\begin{pmatrix} \mathcal{E} \\ \mathcal{H} \end{pmatrix}(x, z, t) = \frac{1}{2} \text{Re} \left\{ A_b(z) \begin{pmatrix} \mathbf{E}_b \\ \mathbf{H}_b \end{pmatrix}(x, z) + A_s(z) \begin{pmatrix} \mathbf{E}_s \\ \mathbf{H}_s \end{pmatrix}(x, z) \right\} e^{i\omega t}.$$

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$$A_b(z), A_s(z) = ?$$

Coupled mode equations

Diagram illustrating the decomposition of a coupled mode system into two uncoupled systems.

The first system, labeled $(\mathbf{E}, \mathbf{H}, \epsilon)$, shows a curved interface between a core (refractive index n_g) and cladding (refractive index n_b). The core has a radius R and a gap of width g . The cladding has a thickness s . The system is defined by the coordinates (x, z) and the refractive index profile ϵ .

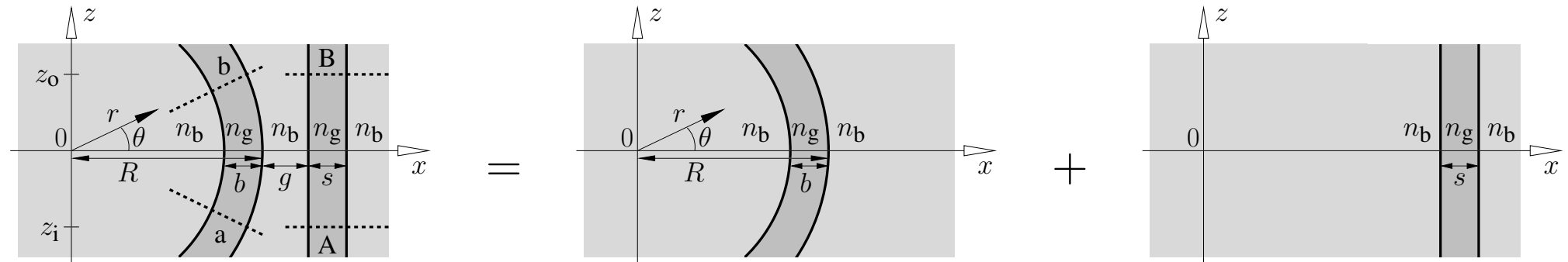
The second system, labeled $(\mathbf{E}_b, \mathbf{H}_b, \epsilon_b)$, shows the core and cladding without the gap. The core has a radius R and a gap of width b . The cladding has a thickness s . The system is defined by the coordinates (x, z) and the refractive index profile ϵ_b .

The third system, labeled $(\mathbf{E}_s, \mathbf{H}_s, \epsilon_s)$, shows the gap and slab without the core. The gap has a width b and the slab has a thickness s . The system is defined by the coordinates (x, z) and the refractive index profile ϵ_s .

The total field is the sum of the two uncoupled fields:

$$(\mathbf{E}, \mathbf{H}, \epsilon) = (\mathbf{E}_b, \mathbf{H}_b, \epsilon_b) + (\mathbf{E}_s, \mathbf{H}_s, \epsilon_s)$$

Coupled mode equations



$(\mathbf{E}, \mathbf{H}, \epsilon)$
 $=$
 $(\mathbf{E}_b, \mathbf{H}_b, \epsilon_b)$
 $+$
 $(\mathbf{E}_s, \mathbf{H}_s, \epsilon_s)$

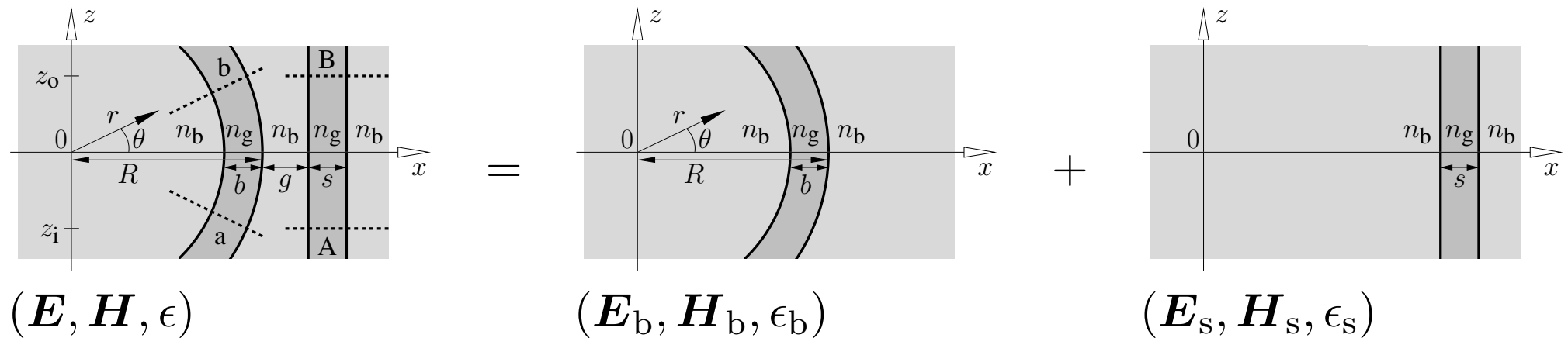
Suitable integral form of Maxwells equations (“reciprocity theorem”)

$\left(\begin{array}{cc} \sigma_{bb} & \sigma_{bs} \\ \sigma_{sb} & \sigma_{ss} \end{array} \right) \frac{d}{dz} \left(\begin{array}{c} A_b \\ A_s \end{array} \right) = \left(\begin{array}{cc} c_{bb} & c_{bs} \\ c_{sb} & c_{ss} \end{array} \right) \left(\begin{array}{c} A_b \\ A_s \end{array} \right),$

$$\sigma_{pq} = \frac{1}{4} \int (E_{px}^* H_{qy} - E_{py}^* H_{qx} + H_{py}^* E_{qx} - H_{px}^* E_{qy}) dx,$$

$$c_{pq} = -i \frac{\omega \epsilon_0}{4} \int \mathbf{E}_p^* (\epsilon - \epsilon_q) \mathbf{E}_q dx, \quad p, q = b, s.$$

Coupled mode equations



Suitable integral form of Maxwells equations (“reciprocity theorem”)

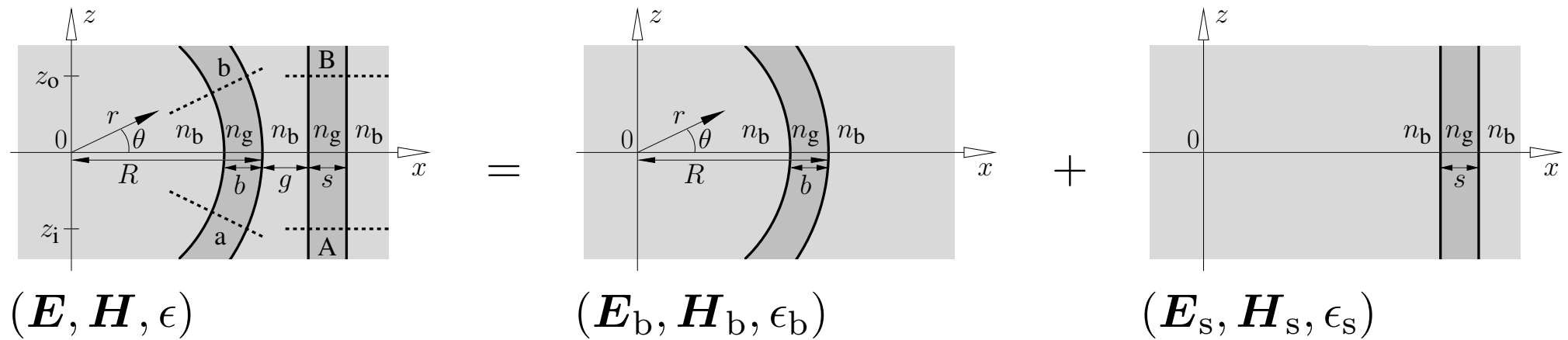
$$\left(\begin{array}{cc} \sigma_{bb} & \sigma_{bs} \\ \sigma_{sb} & \sigma_{ss} \end{array} \right) \frac{d}{dz} \left(\begin{array}{c} A_b \\ A_s \end{array} \right) = \left(\begin{array}{cc} c_{bb} & c_{bs} \\ c_{sb} & c_{ss} \end{array} \right) \left(\begin{array}{c} A_b \\ A_s \end{array} \right),$$

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Numerical evaluation $\rightsquigarrow A_b(z), A_s(z)$

Coupled mode equations



Suitable integral form of Maxwells equations (“reciprocity theorem”)

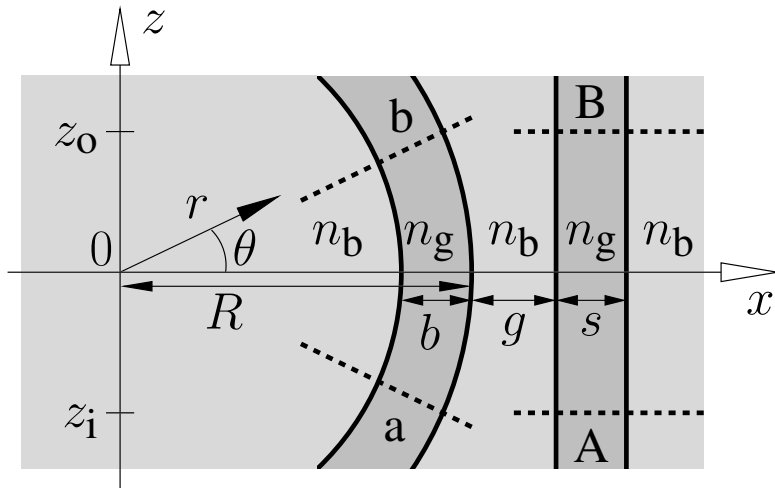
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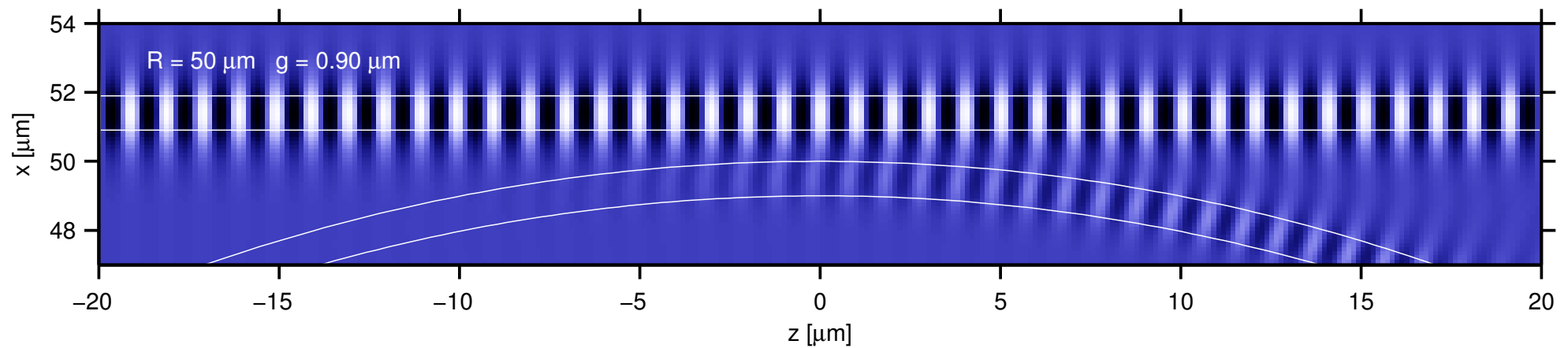
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Numerical evaluation $\rightsquigarrow A_b(z), A_s(z) \rightsquigarrow \dots \rightsquigarrow \rho, \kappa, \tau.$

CMT coupler model, examples

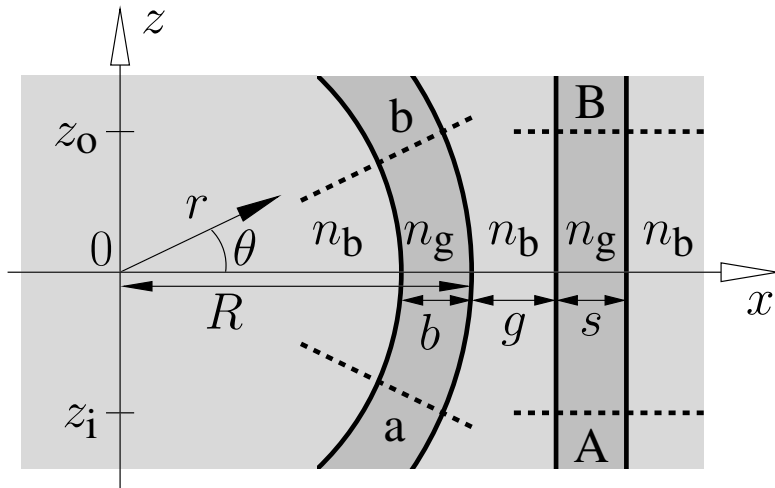


2D, TE,
 $n_b = 1.45$, $n_g = 1.60$, $b = s = 1.0 \mu\text{m}$, $\lambda = 1.55 \mu\text{m}$,
 $R = 50 \mu\text{m}$, $g = 0.90 \mu\text{m}$.

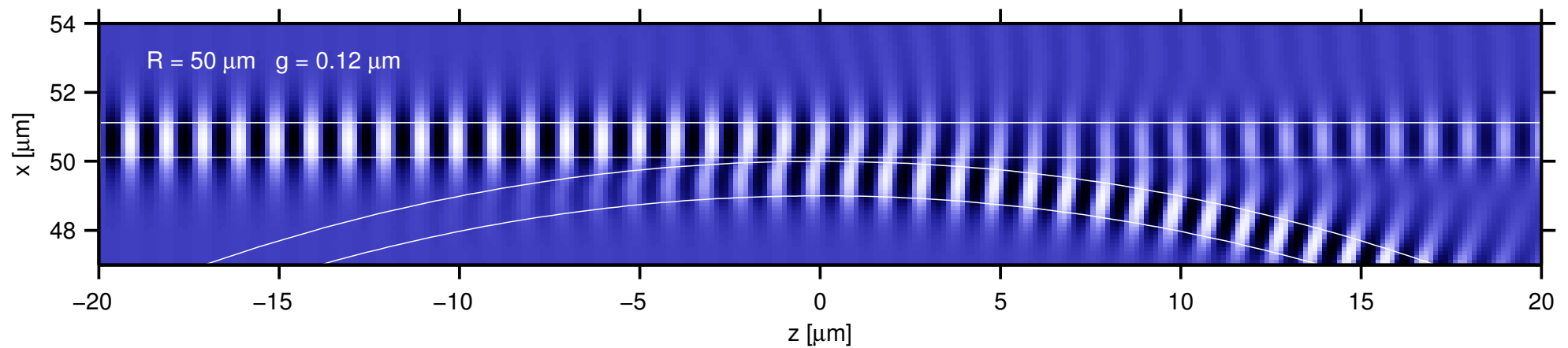


$$|\rho|^2 = 0.93, |\kappa|^2 = 0.07, |\tau|^2 = 0.92.$$

CMT coupler model, examples

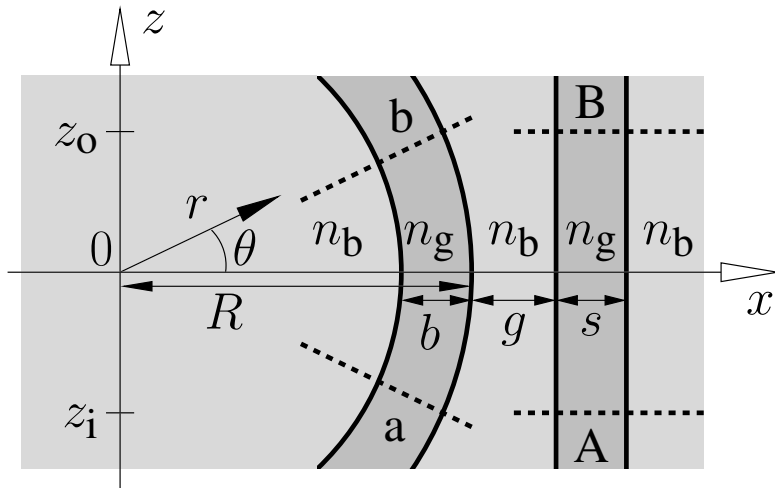


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 $n_b = 1.45$, $n_g = 1.60$, $b = s = 1.0 \mu\text{m}$, $\lambda = 1.55 \mu\text{m}$,
 $R = 50 \mu\text{m}$, $g = 0.12 \mu\text{m}$.

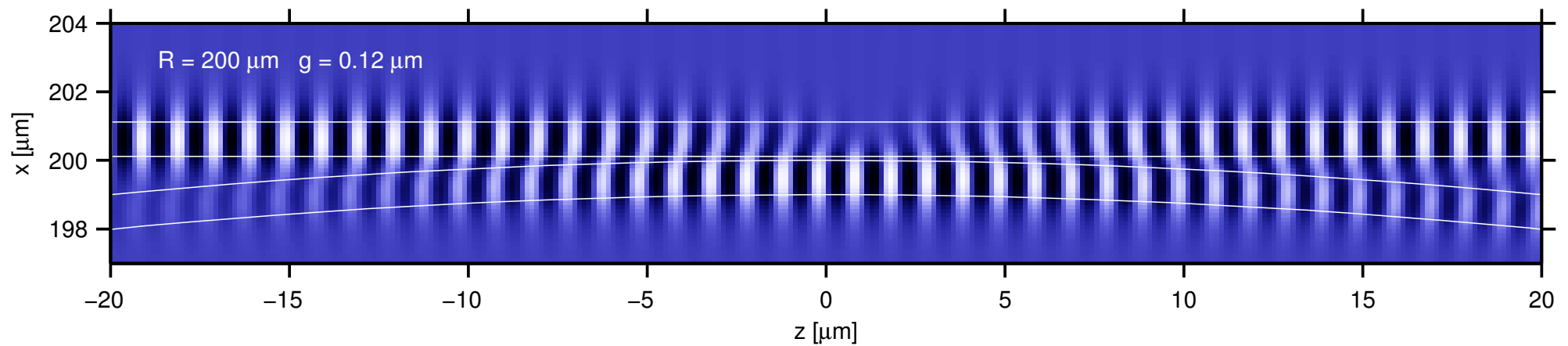


$$|\rho|^2 = 0.16, |\kappa|^2 = 0.83, |\tau|^2 = 0.16.$$

CMT coupler model, examples

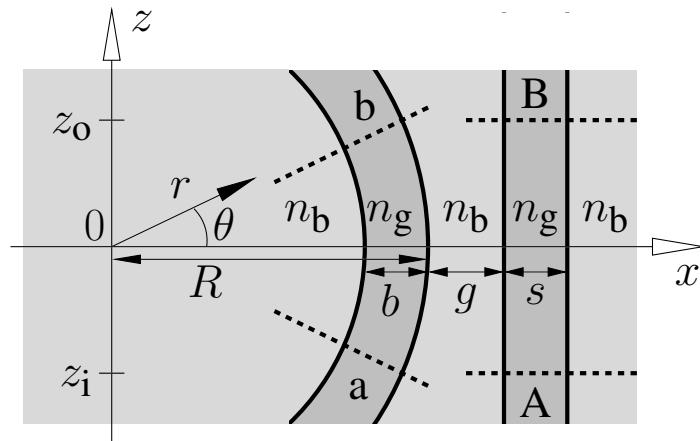


2D, TE,
 $n_b = 1.45$, $n_g = 1.60$, $b = s = 1.0 \mu\text{m}$, $\lambda = 1.55 \mu\text{m}$,
 $R = 200 \mu\text{m}$, $g = 0.12 \mu\text{m}$.

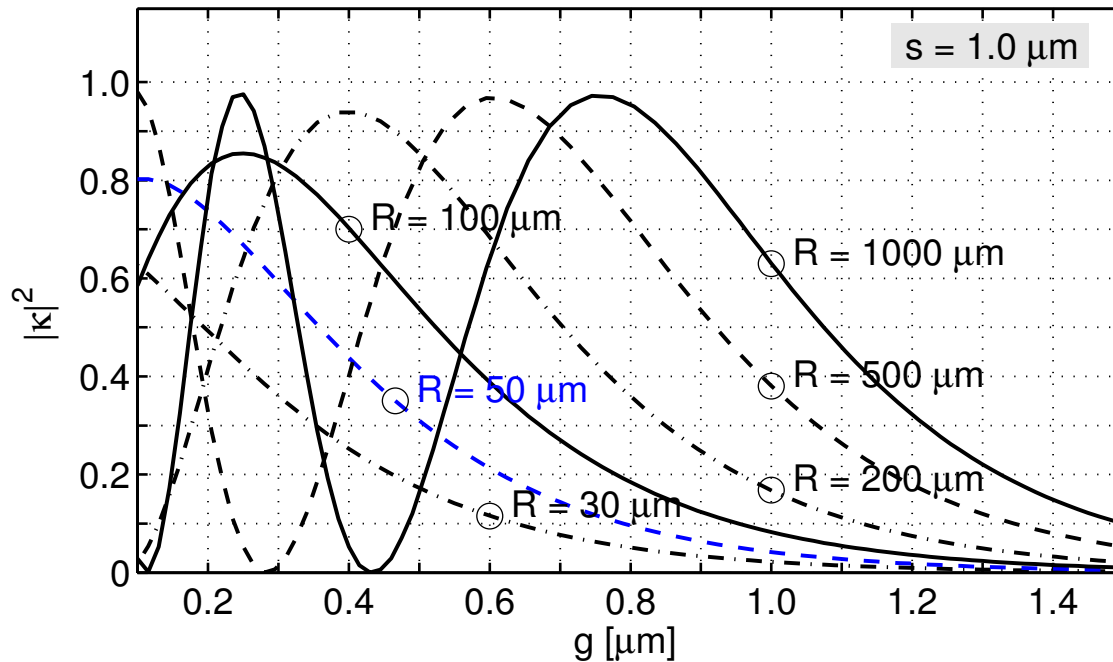


$$|\rho|^2 = 0.93, |\kappa|^2 = 0.07, |\tau|^2 = 0.93.$$

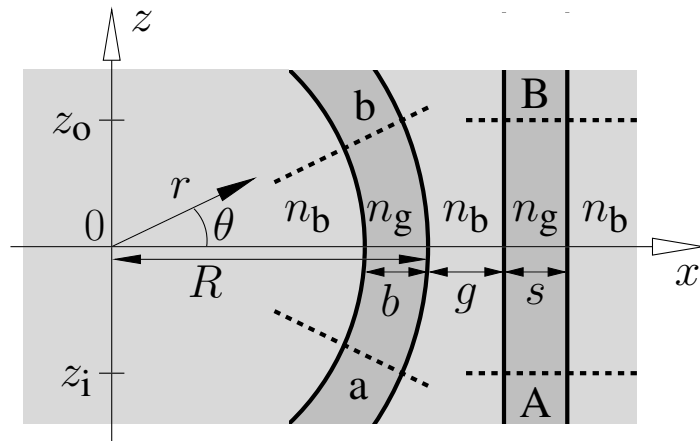
Coupling coefficients vs. coupler geometry



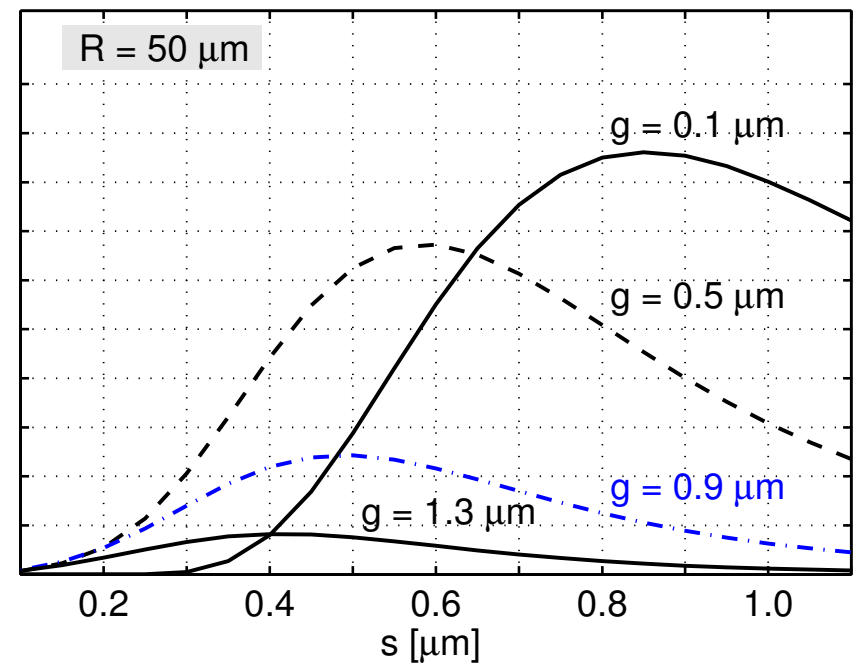
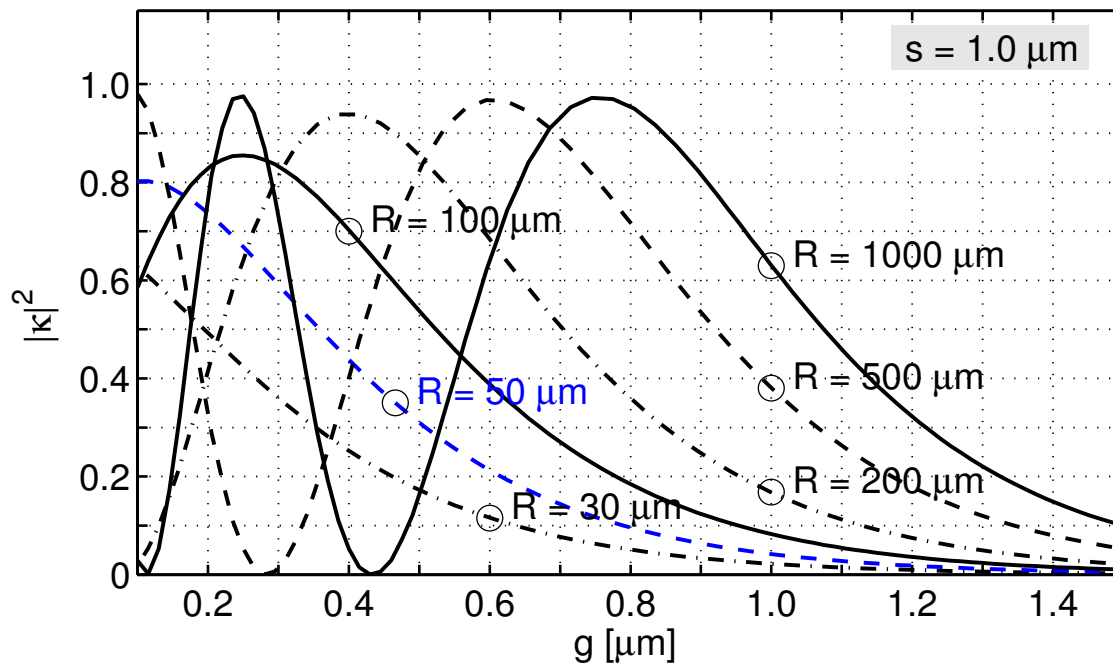
2D, TE,
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Coupling coefficients vs. coupler geometry



2D, TE,
 $n_b = 1.45$, $n_g = 1.60$, $b = 1.0 \mu\text{m}$, $\lambda = 1.55 \mu\text{m}$.



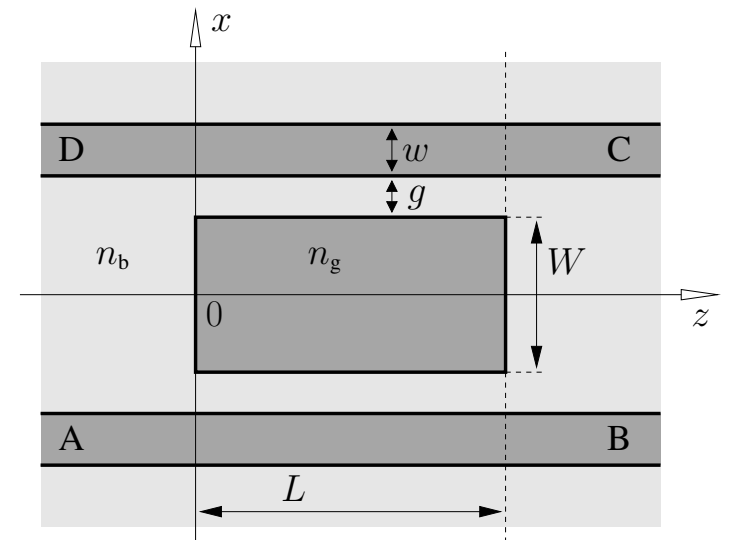
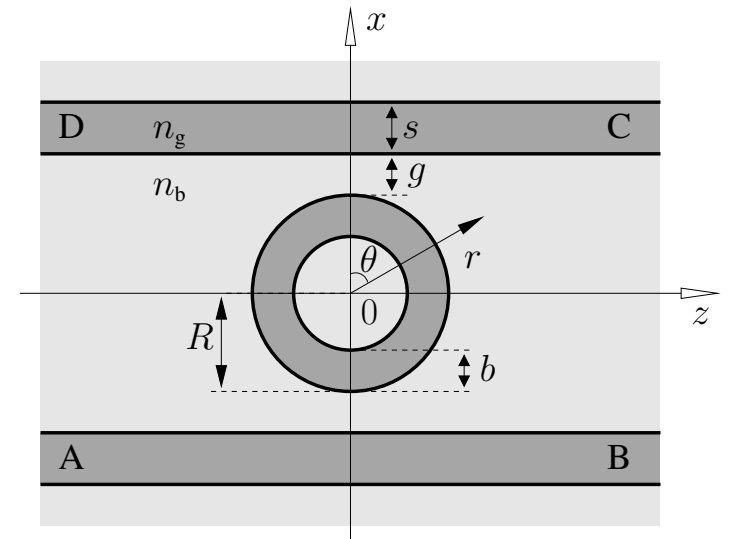
• • • • •



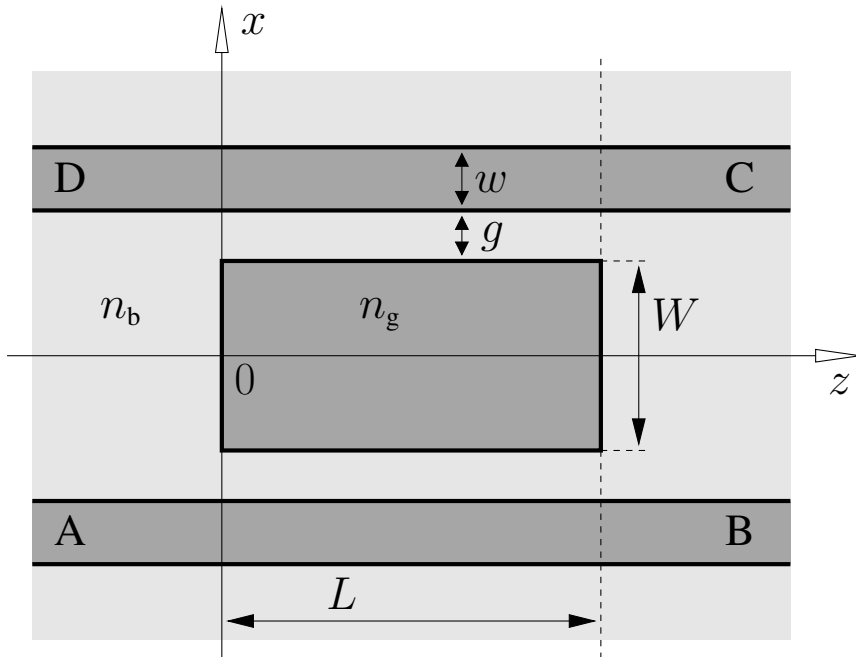
Circular traveling wave resonators



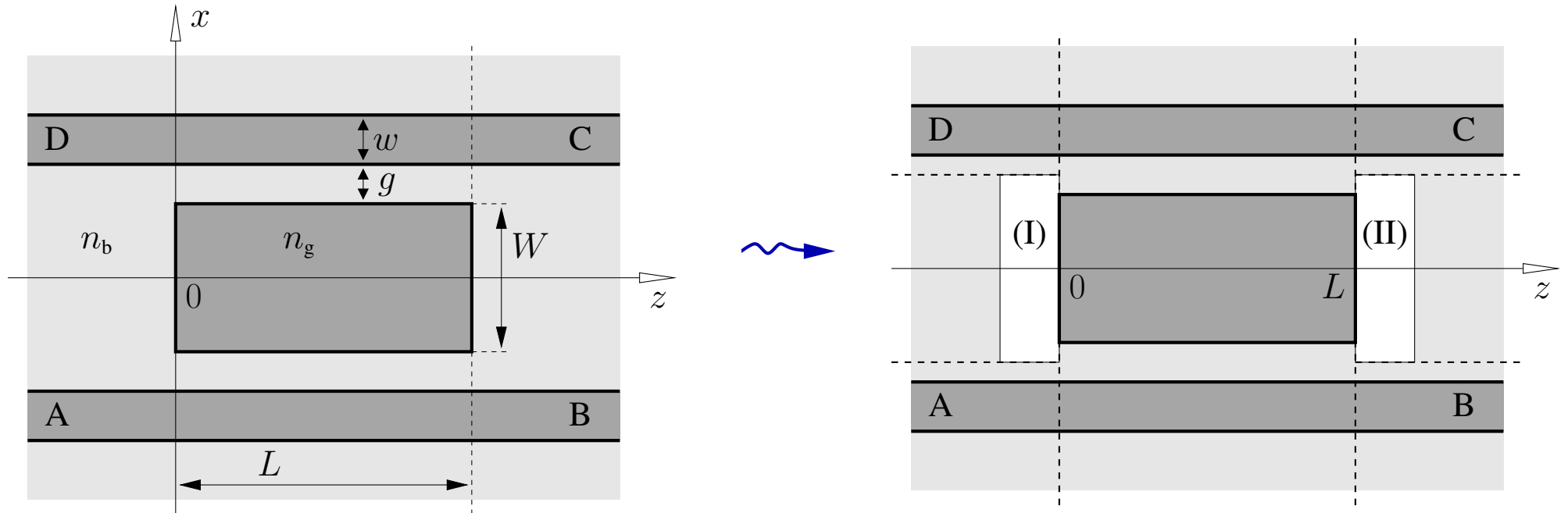
Rectangular standing wave resonators



Rectangular Resonator: Abstract model

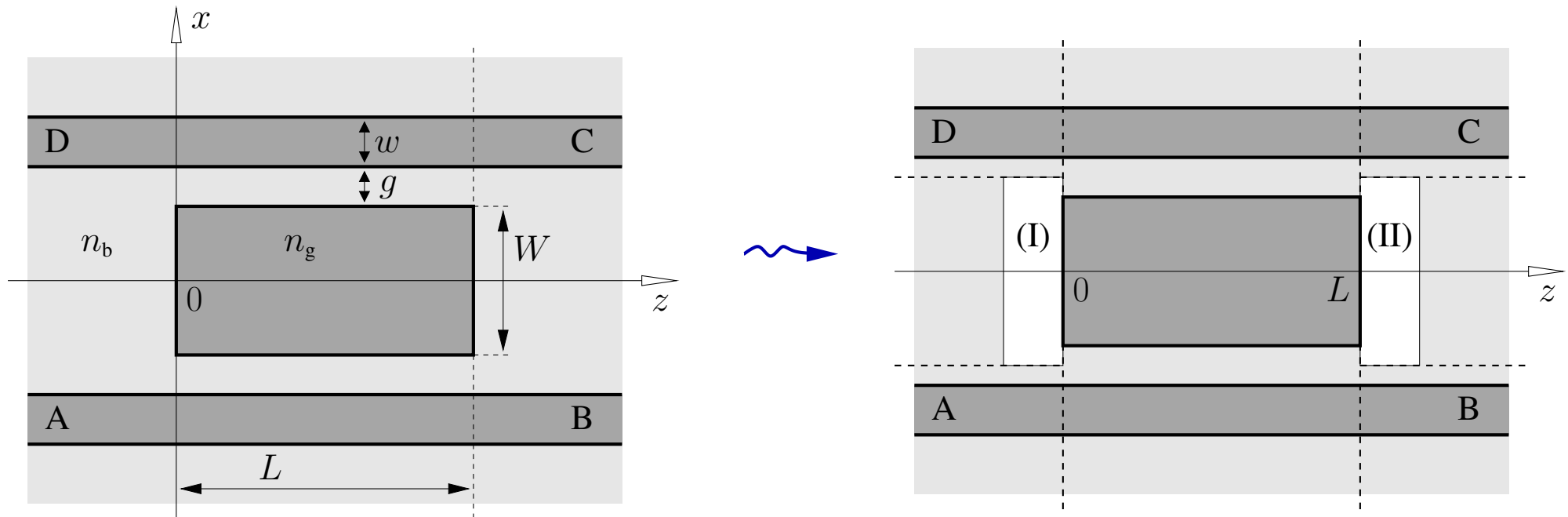


Rectangular Resonator: Abstract model



- Resonator \approx central cavity segment + 2 facets

Rectangular Resonator: Abstract model

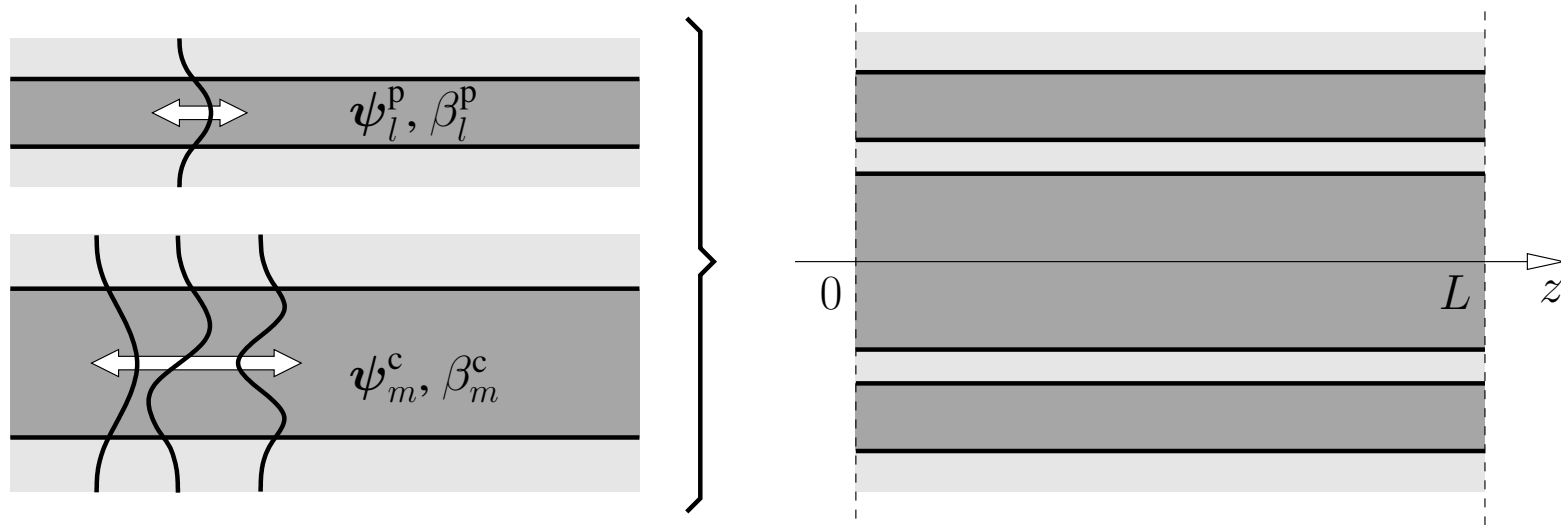


- Resonator \approx central cavity segment + 2 facets
- CW description: $\mathbf{E}, \mathbf{H} \sim e^{i\omega t}$, $\omega = kc$, $k = 2\pi/\lambda$.

Central coupler segment: Basis fields & transfer matrix

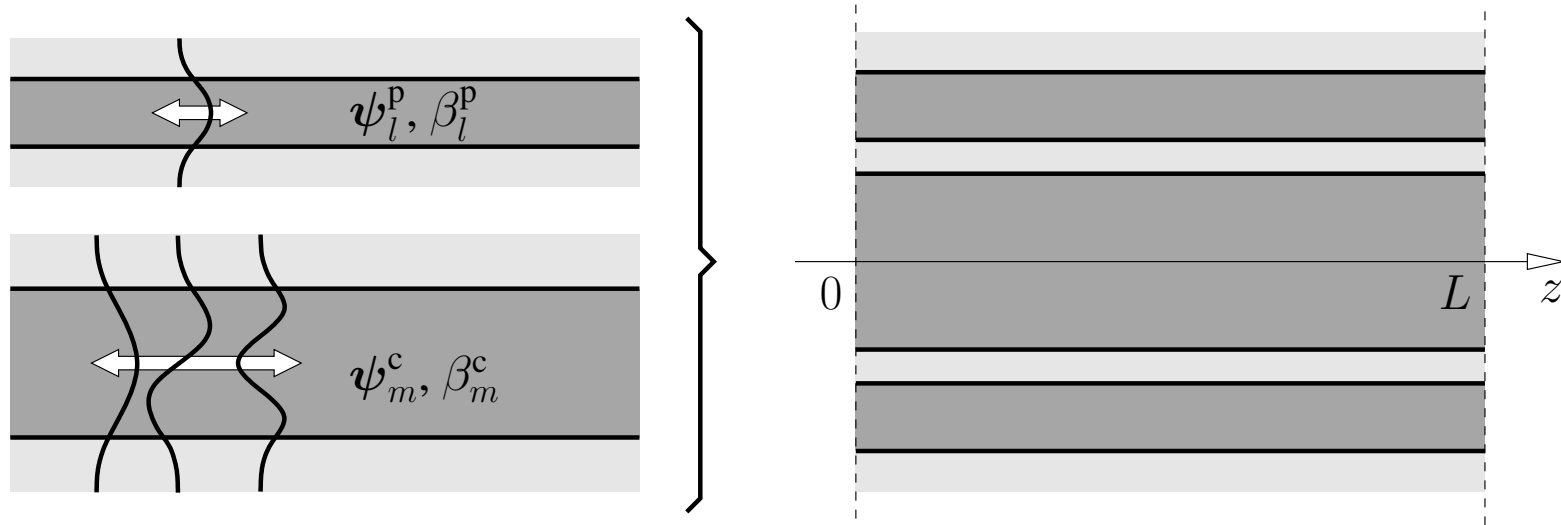


Central coupler segment: Basis fields & transfer matrix



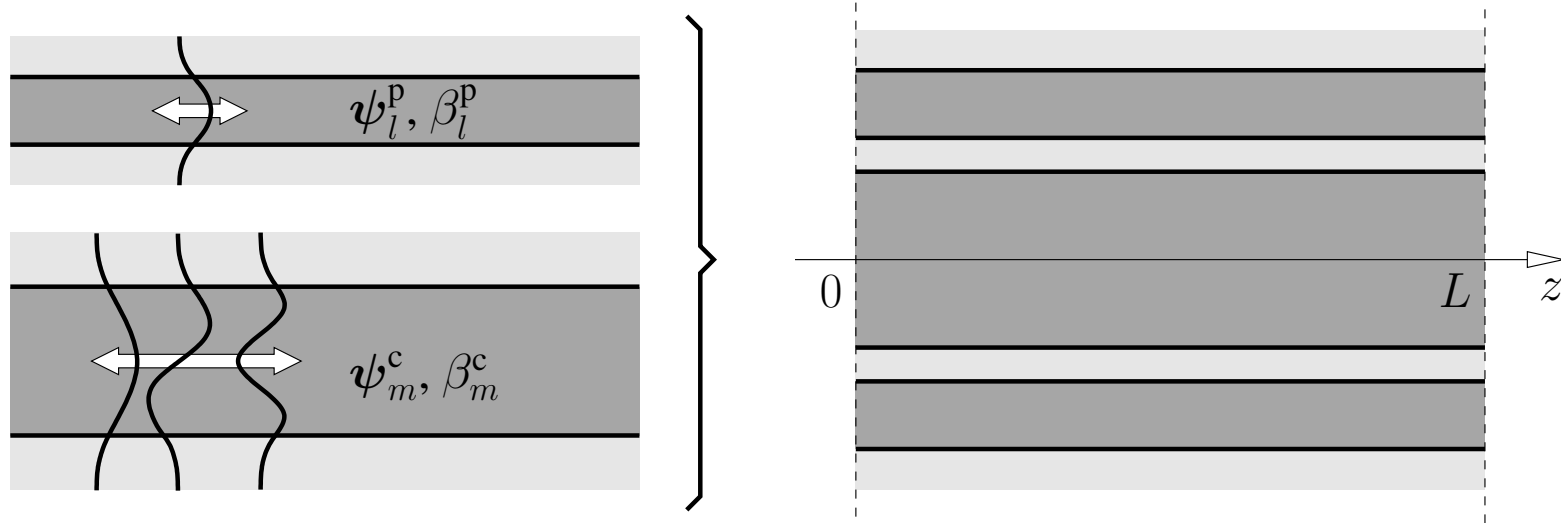
- Basis: Guided fields ψ_l^p , ψ_m^c , and propagation constants β_l^p , β_m^c , of port and cavity cores.

Central coupler segment: Basis fields & transfer matrix



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- F , B : Amplitudes of forward and backward copies of the basis modes.

Central coupler segment: Basis fields & transfer matrix

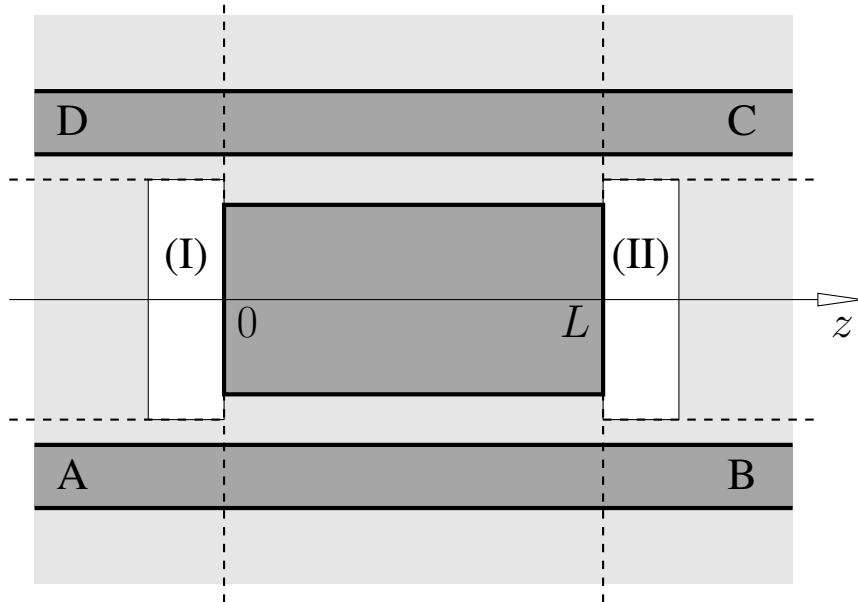


- Basis: Guided fields ψ_l^p , ψ_m^c , and propagation constants β_l^p , β_m^c , of port and cavity cores.
- F , B : Amplitudes of forward and backward copies of the basis modes.
- Propagation along the cavity segment:

$$F(L) = \mathsf{T} F(0), \quad B(0) = \mathsf{T} B(L),$$

T : Cavity transfer matrix.

Facets: Multimode reflection

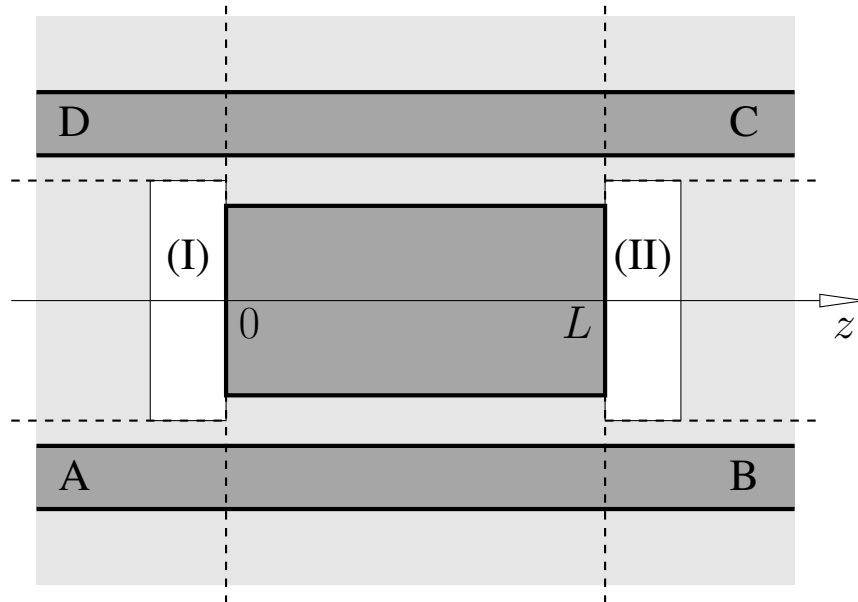


Facets:

\approx no effect on ψ_l^p ,
strong effect on ψ_m^c .

$$\mathbf{F} = \begin{pmatrix} F_p \\ F_c \end{pmatrix}, \quad \mathbf{B} = \begin{pmatrix} B_p \\ B_c \end{pmatrix}.$$

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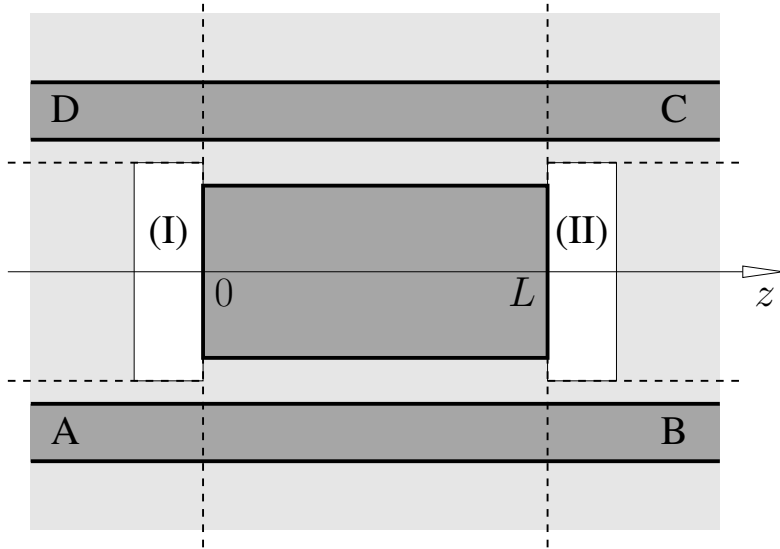
↪ Guided wave reflection at the facet:

$$\mathbf{B}_c(L) = \mathbf{R} \mathbf{F}_c(L),$$

$$\mathbf{F}_c(0) = \mathbf{R} \mathbf{B}_c(0),$$

\mathbf{R} : Facet reflectivity matrix.

Output amplitudes & power



Cavity transfer matrix

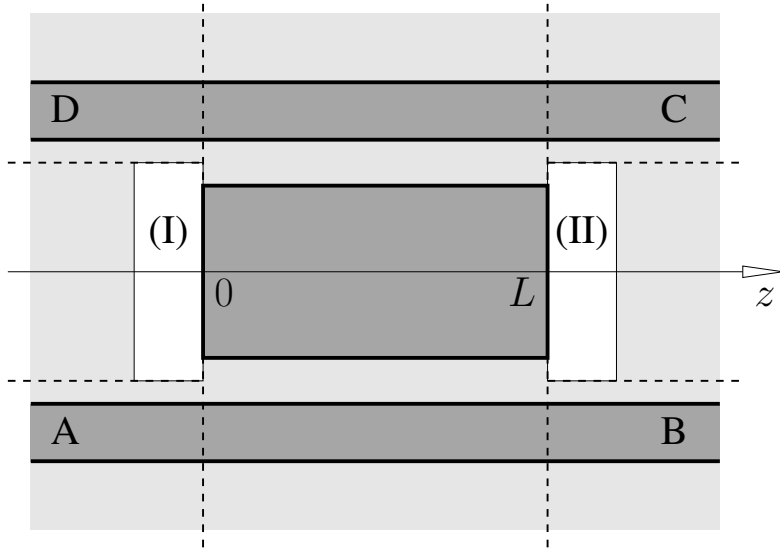
$$T = \begin{pmatrix} T_{pp} & T_{pc} \\ T_{cp} & T_{cc} \end{pmatrix}$$

+ Facet reflectivity matrix R

+ External input amplitudes

$$F_p(0) = \begin{pmatrix} 1 \\ 0 \end{pmatrix}, \quad B_p(L) = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

Output amplitudes & power



Cavity transfer matrix

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External output amplitudes :

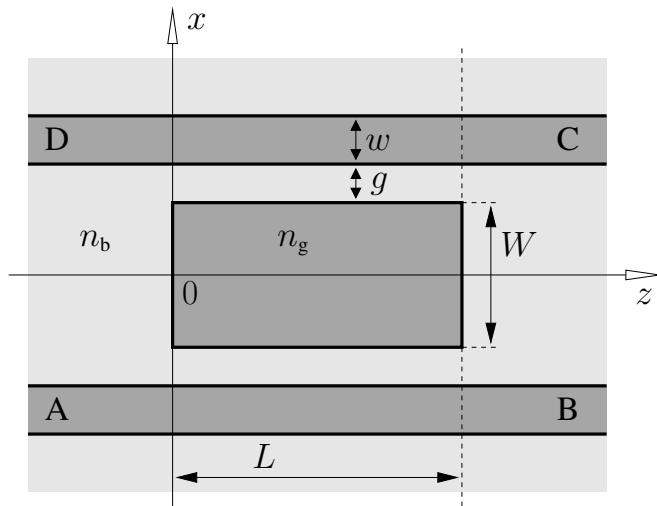
$$\mathbf{F}_p(L) = (\mathbf{T}_{pp} + \mathbf{T}_{pc}\mathbf{R}\Omega^{-1}\mathbf{T}_{cc}\mathbf{R}\mathbf{T}_{cp})\mathbf{F}_p(0),$$

$$\mathbf{B}_p(0) = \mathbf{T}_{pc}\mathbf{R}\Omega^{-1}\mathbf{T}_{cp}\mathbf{F}_p(0),$$

$$\Omega = \mathbf{1} - \mathbf{T}_{cc}\mathbf{R}\mathbf{T}_{cc}\mathbf{R}.$$

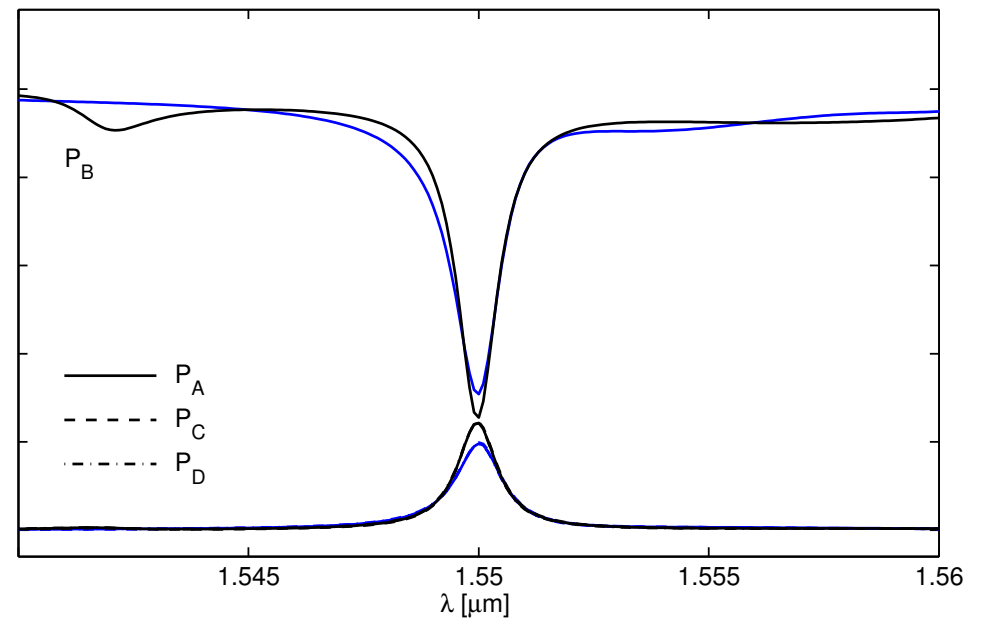
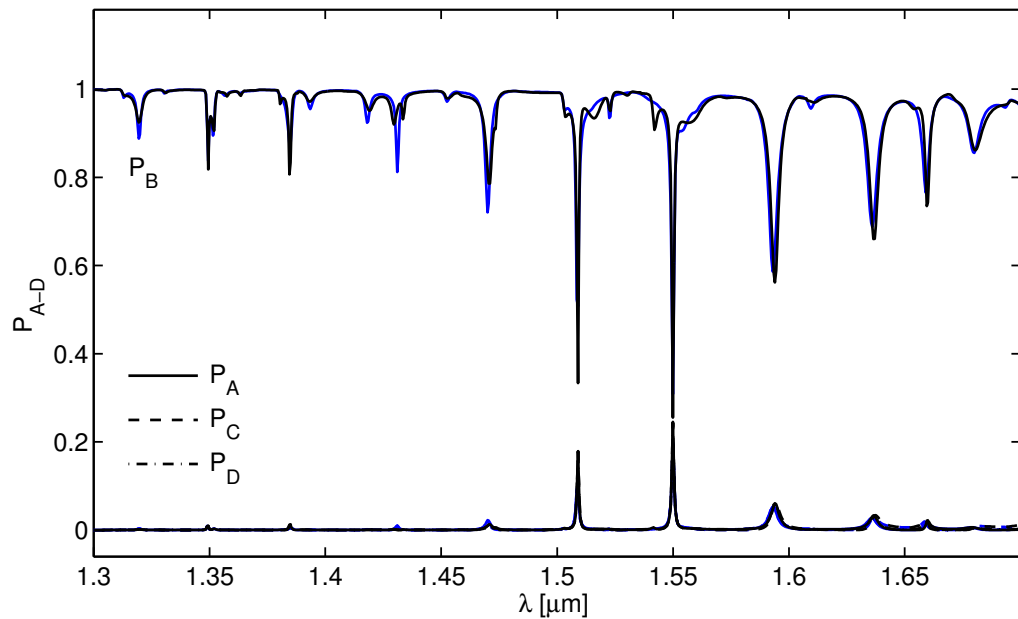
$$P_A = |B_{p,1}(0)|^2, \quad P_B = |F_{p,1}(L)|^2, \quad P_C = |F_{p,2}(L)|^2, \quad P_D = |B_{p,2}(0)|^2.$$

Spectral response



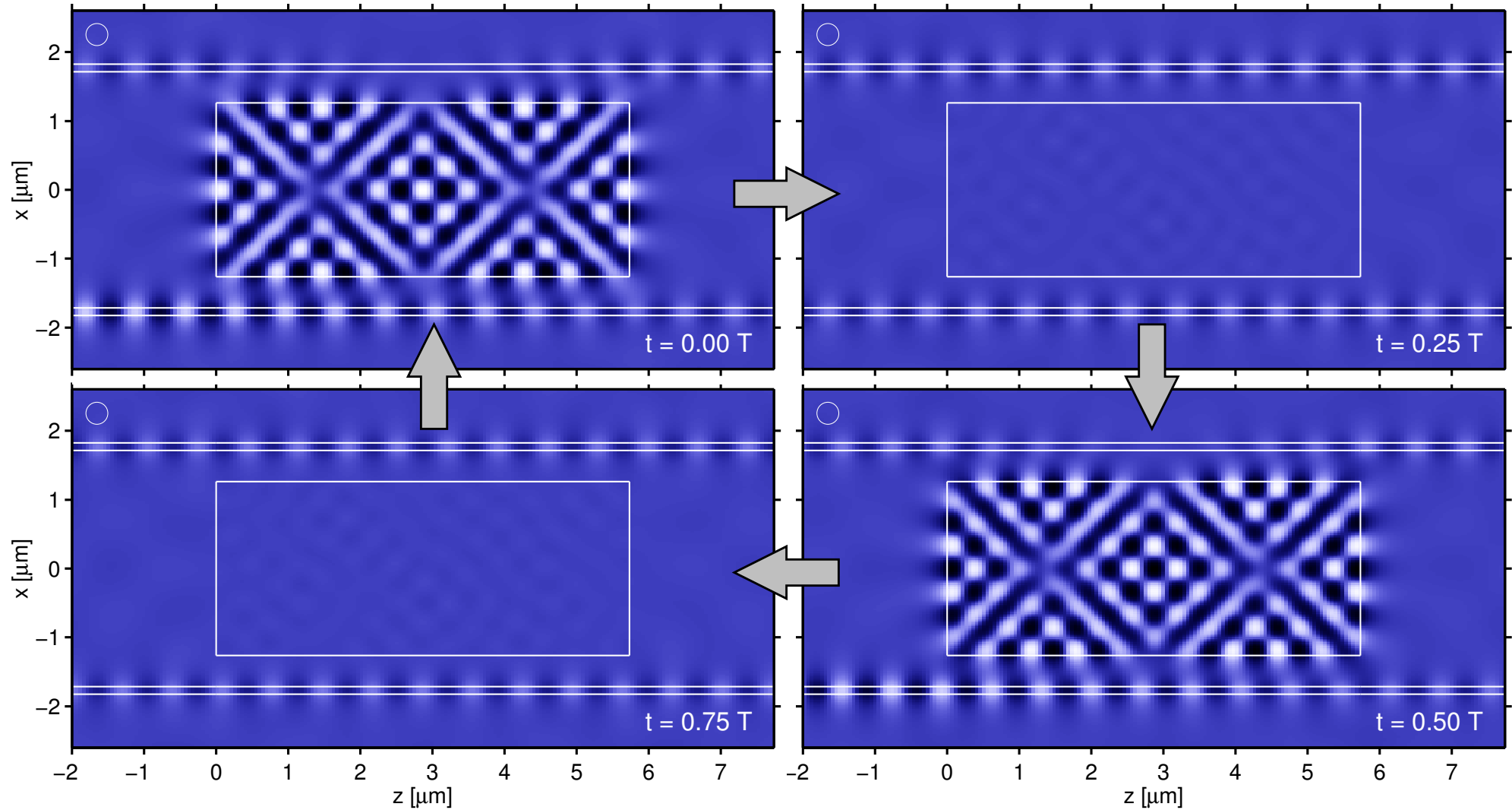
$W = 2.524 \mu\text{m}$, $L = 5.738 \mu\text{m}$,
 $w = 0.112 \mu\text{m}$, $g = 0.450 \mu\text{m}$,
 $n_b = 1.45$, $n_g = 3.40$; TE.

— CMT,
 — Rigorous simulations (BEP).



Resonant field pattern

$\mathcal{E}_y(x, z, t)$:



$\lambda = 1.55 \mu\text{m}$, $T = 5.17 \text{ fs}$.

Detaching the cavity

- Resonances \leftrightarrow Singularities in Ω .

Detaching the cavity

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- The cavity amplifies a field $\mathbf{F}_c(L) = \mathbf{v}$ that corresponds to a large eigenvalue a of Ω^{-1} : $\Omega^{-1}\mathbf{v} = a\mathbf{v}$, $\Omega\mathbf{v} = (1/a)\mathbf{v}$, amplification $A = |a|^2$.

Resonant configurations:

- $\Omega = 1 - T_{cc}RT_{cc}R$ has a zero eigenvalue.
- $T_{cc}RT_{cc}R$ has an eigenvalue 1:

$$\mathbf{F}_c(L) \xrightarrow{R} \mathbf{B}_c(L) \xrightarrow{T_{cc}} \mathbf{B}_c(0) \xrightarrow{R} \mathbf{F}_c(0) \xrightarrow{T_{cc}} \mathbf{F}_c(L).$$

- $T_{cc}R$ has an eigenvalue $\mu = +1$ or $\mu = -1$.

Amplification for a field \mathbf{v} with $T_{cc}R\mathbf{v} = \mu\mathbf{v}$, $\mu = r e^{i\chi}$:

$$A = \frac{1}{|\mu^2 - 1|^2} = \frac{1}{1 + r^4 - 2r^2 \cos(2\chi)}.$$

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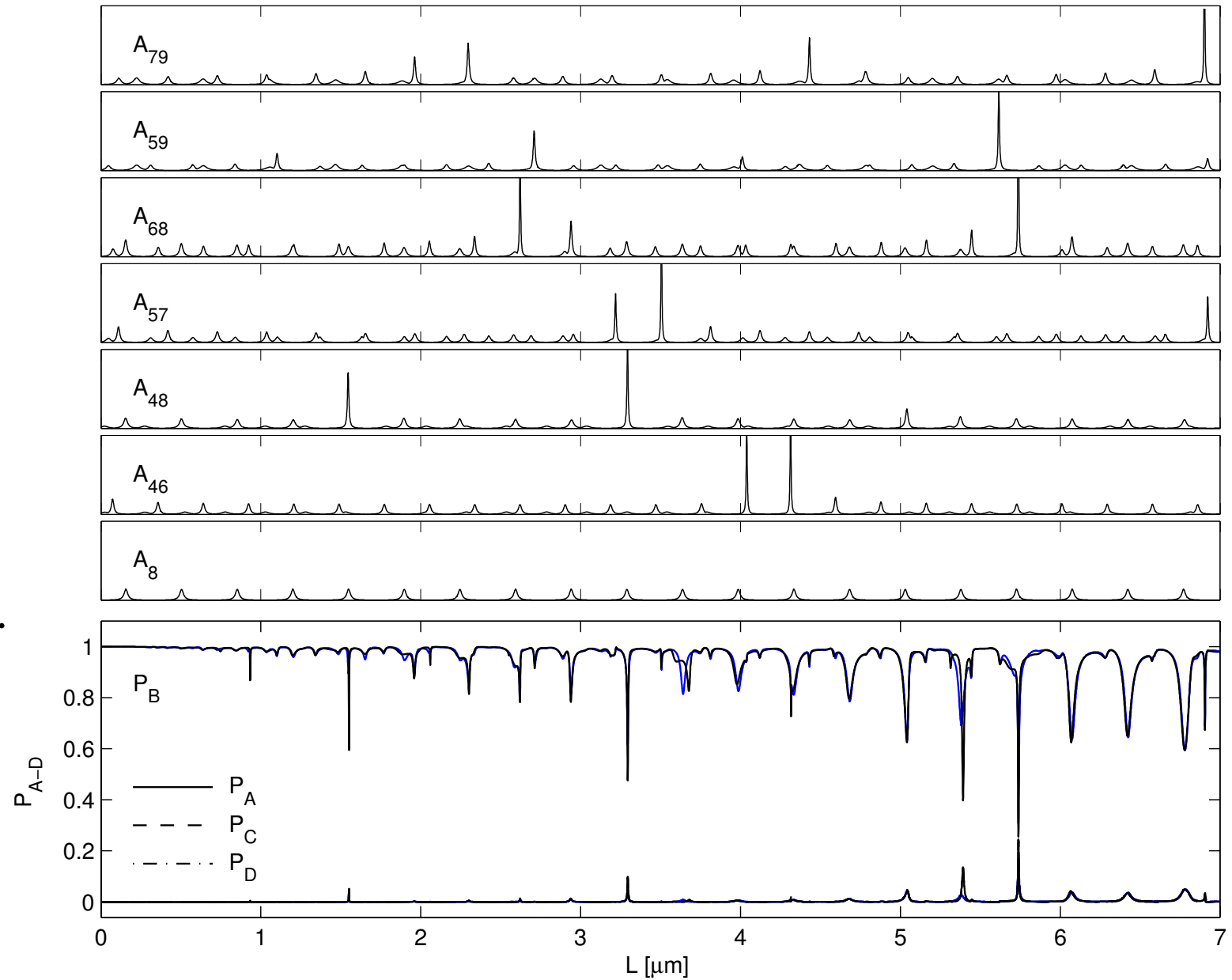
$$A = \frac{1}{|\mu^2 - 1|^2} = \frac{1}{1 + r^4 - 2r^2 \cos(2\chi)}.$$

- Isolated cavity:

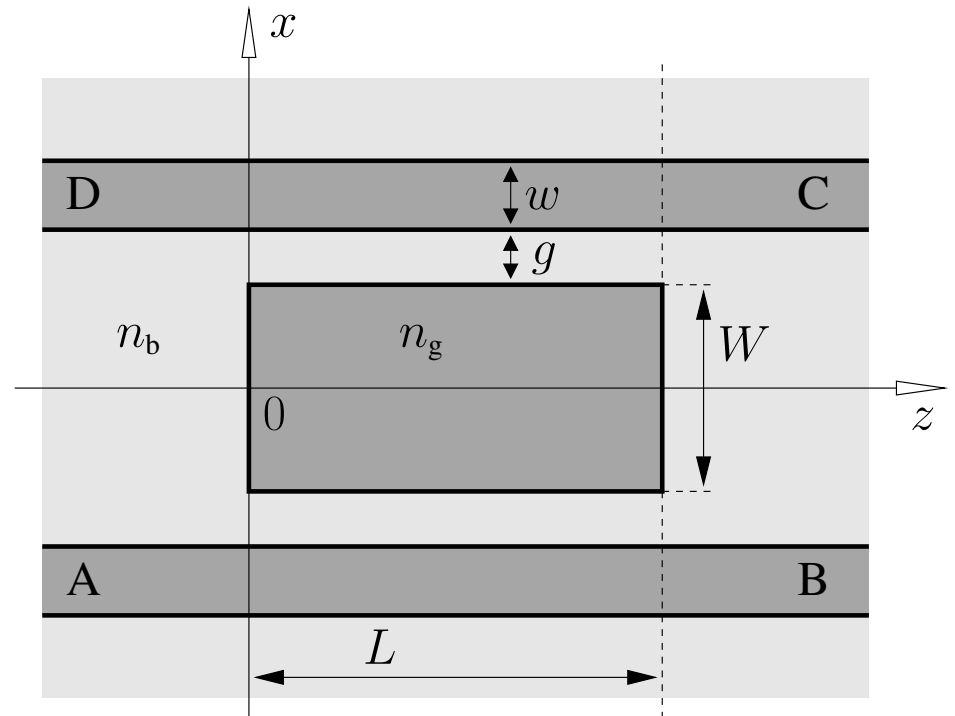
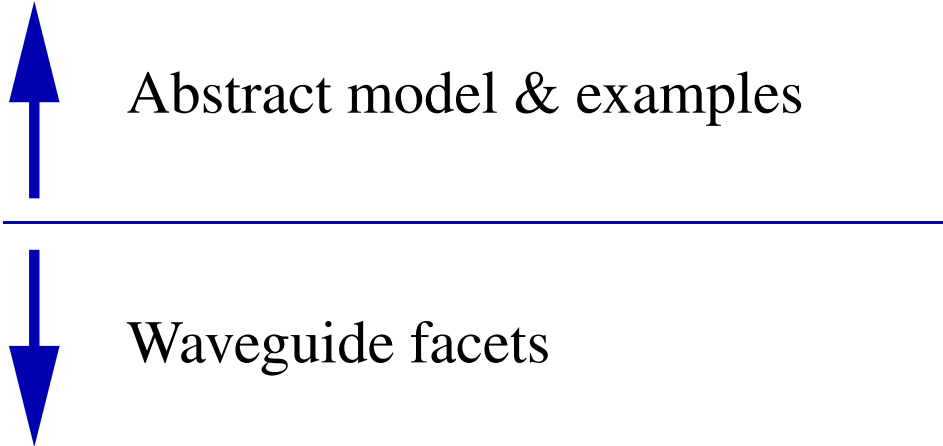
$$T_{cc} \xrightarrow{g \rightarrow \infty} \text{diag} \left(e^{-i\beta_1^c L}, \dots, e^{-i\beta_N^c L} \right).$$

Resonant configurations, CMT model

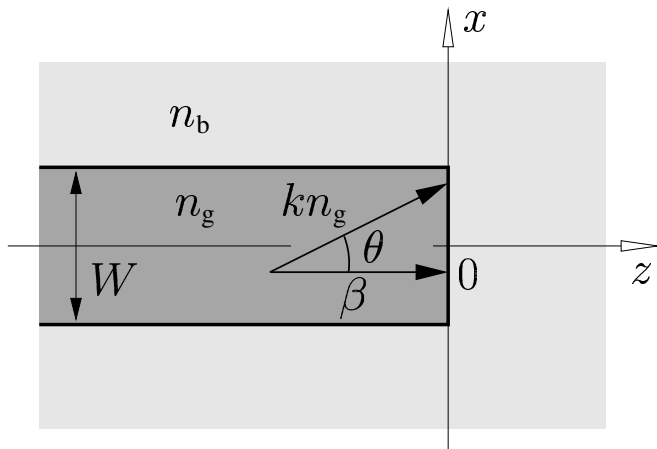
$A_m, A_{m,l}$:
cavity modes
 m or $m \& l$.
↪ classification
of resonances.



...

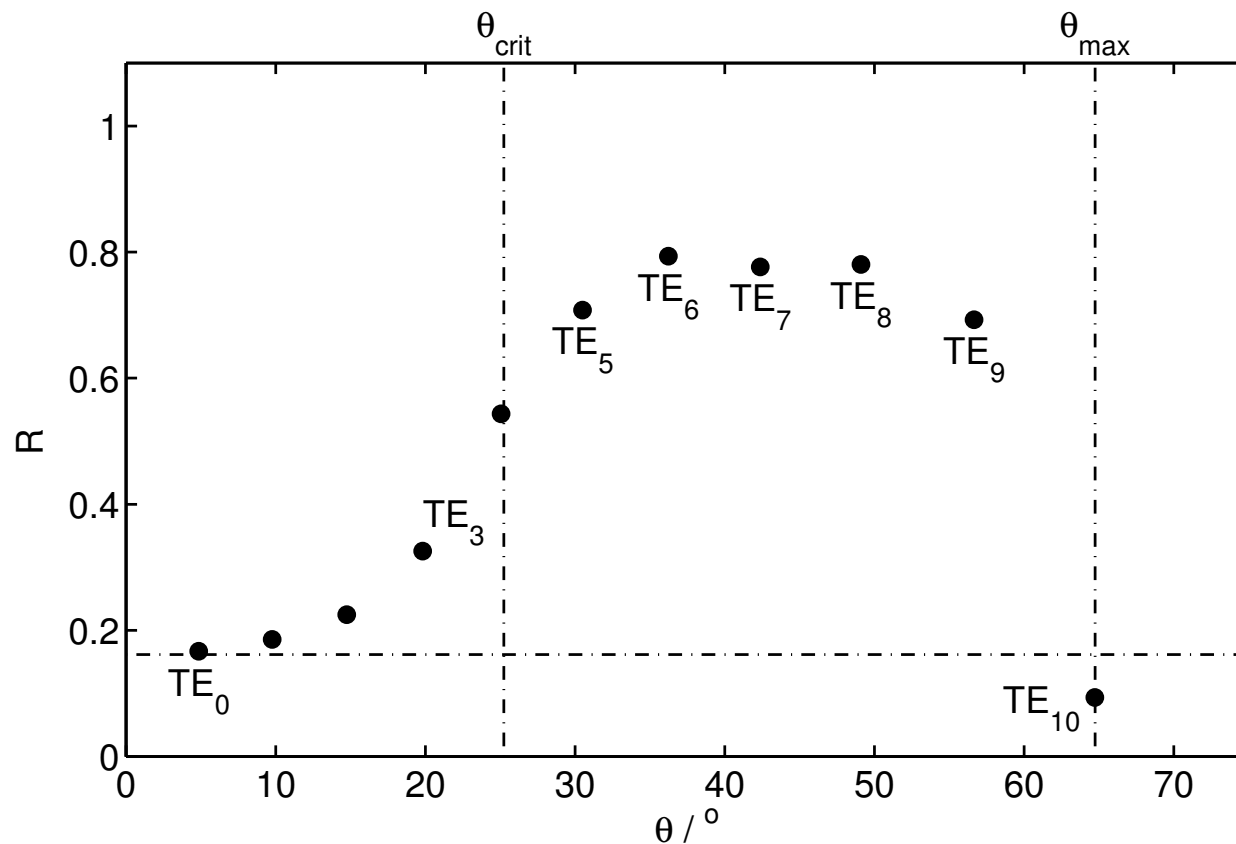


Multimode facet reflectivity



$$\sin \theta_{\text{crit}} = n_b / n_g, \quad \sin \theta_{\text{max}} = \sqrt{1 - n_b^2 / n_g^2},$$

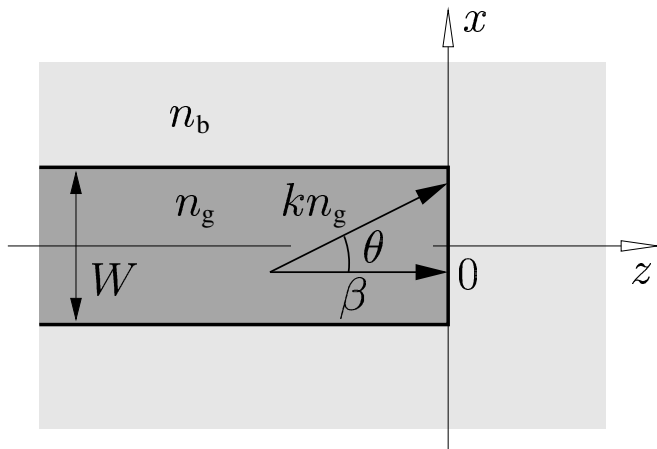
$$\theta > \theta_{\text{crit}} \leftrightarrow n_g > \sqrt{2} n_b.$$



• Single mode reflectivity

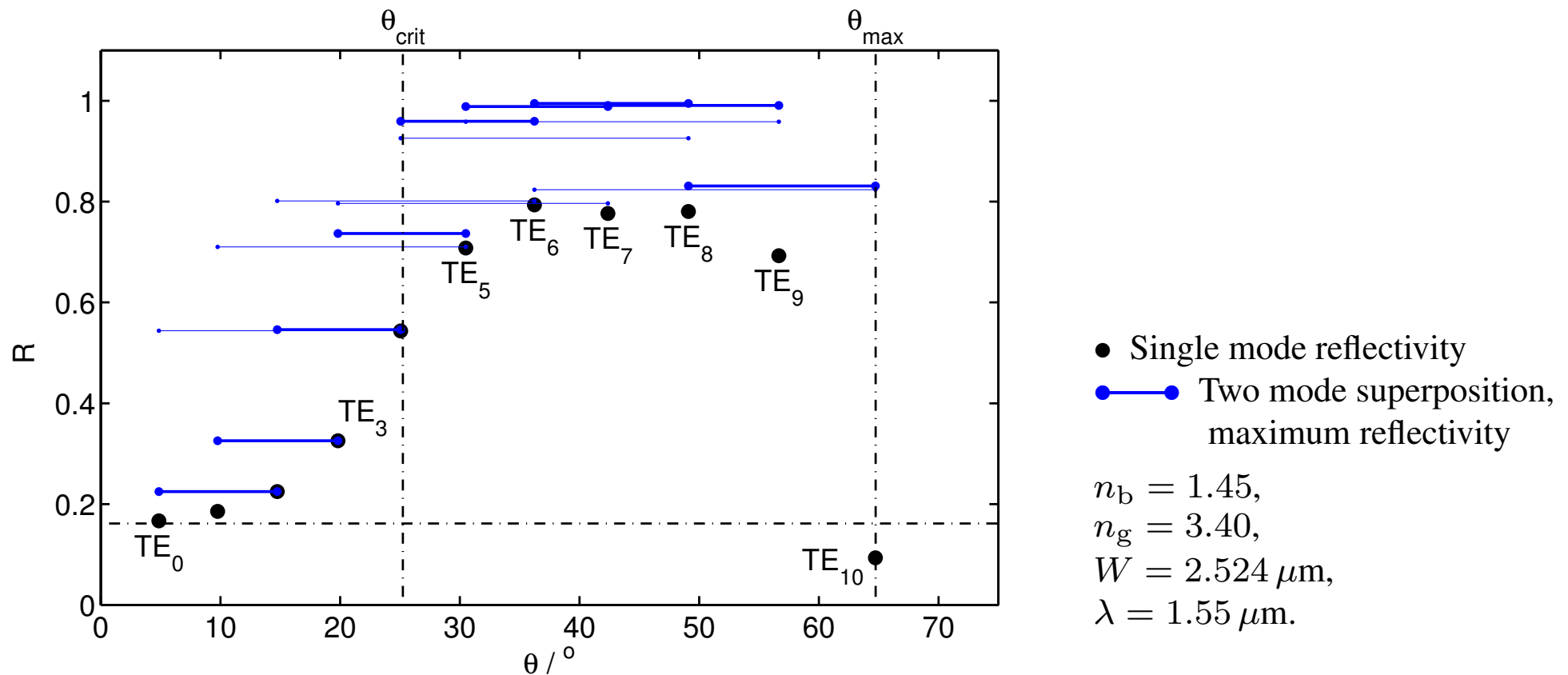
$n_b = 1.45,$
 $n_g = 3.40,$
 $W = 2.524 \mu\text{m},$
 $\lambda = 1.55 \mu\text{m}.$

Multimode facet reflectivity

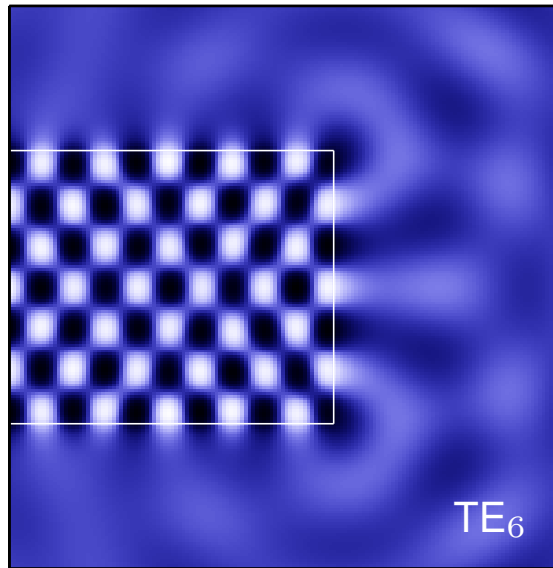


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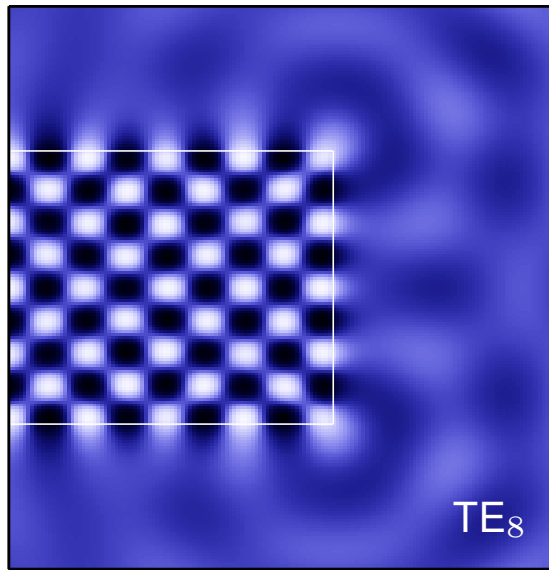
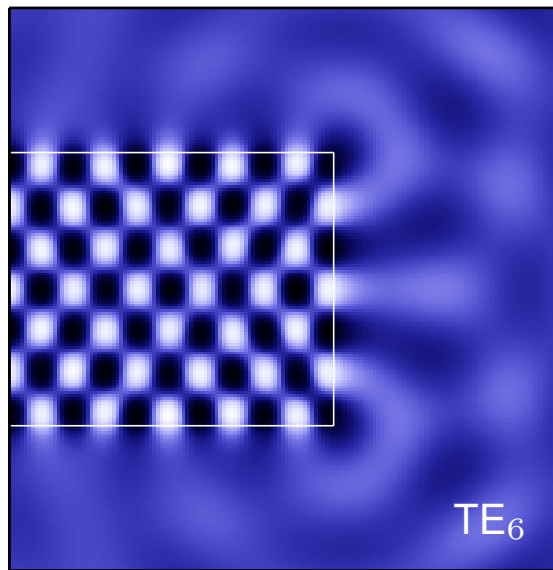


Single- and bimodal reflections



$$R_6 = 0.79$$

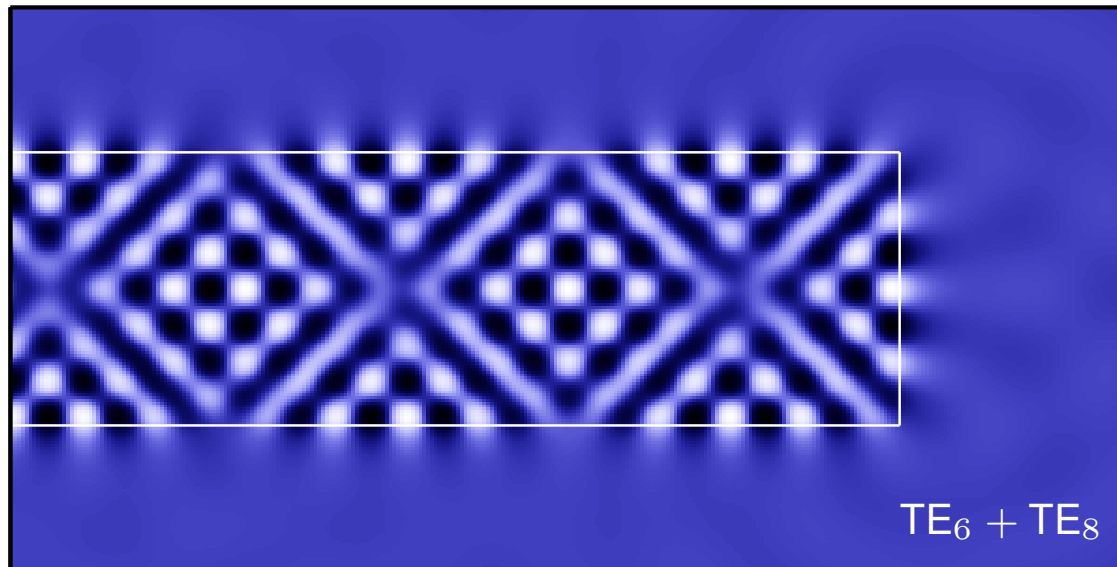
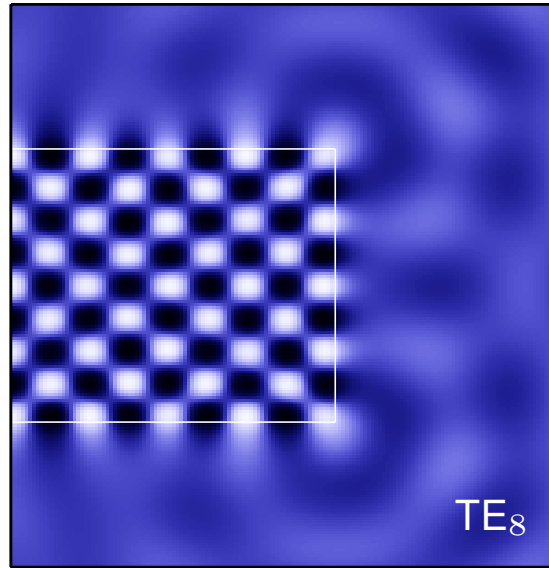
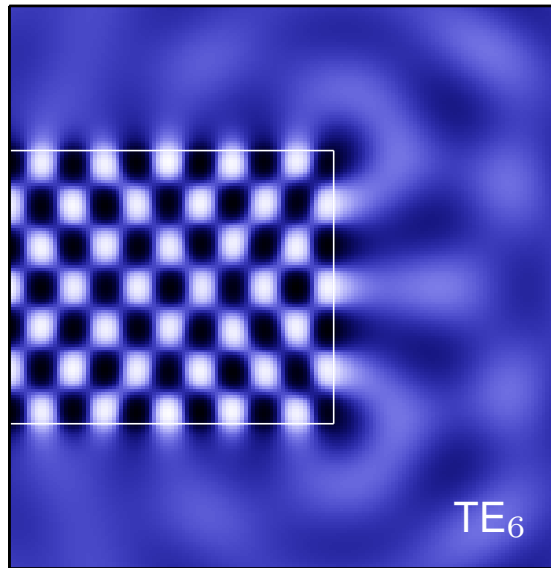
Single- and bimodal reflections



$$R_6 = 0.79$$

$$R_8 = 0.78$$

Single- and bimodal reflections

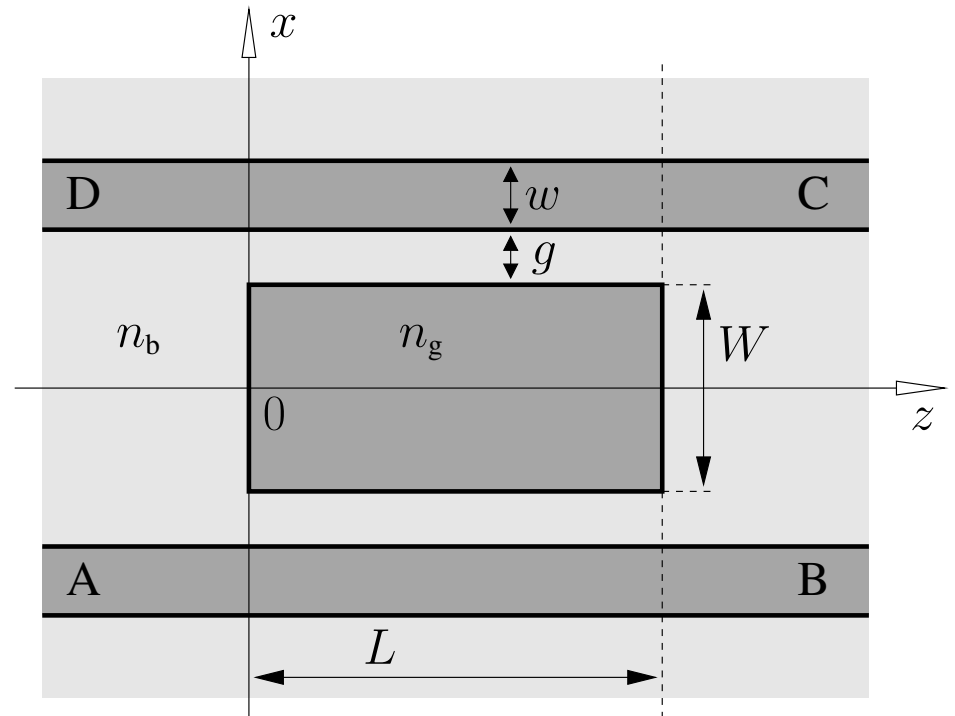
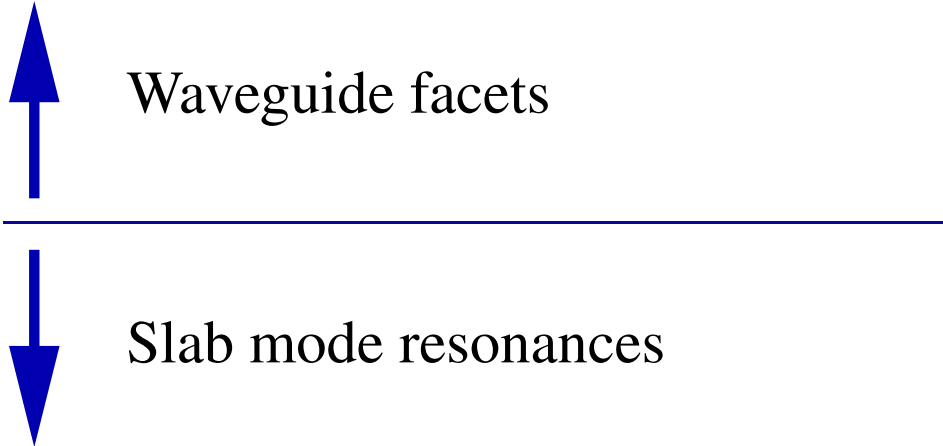


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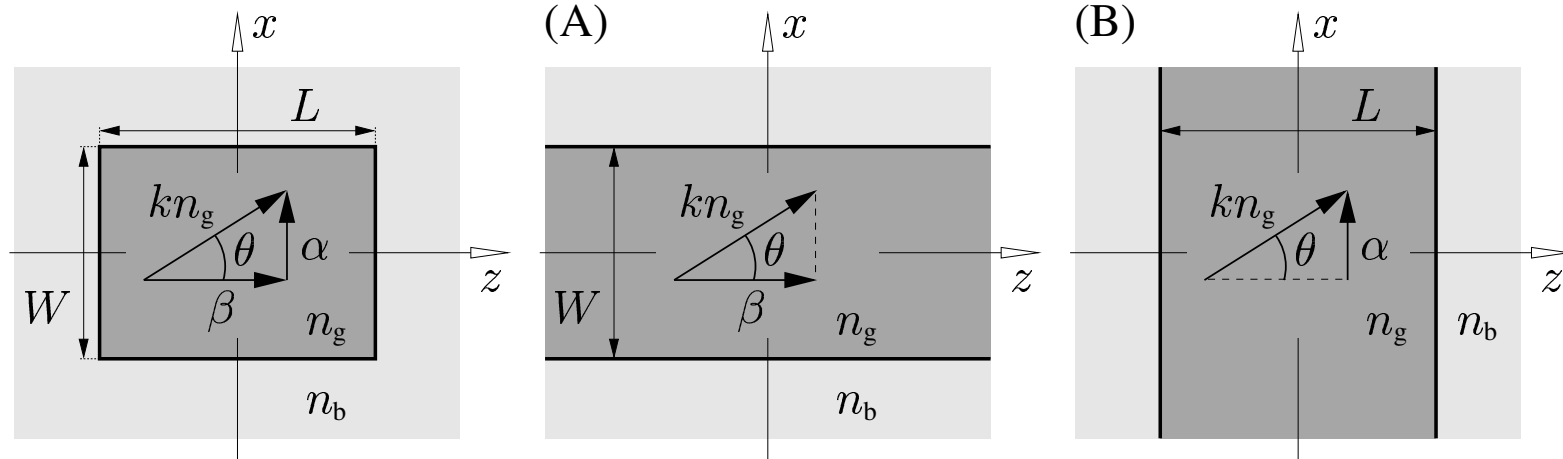
$$R_8 = 0.78$$

$$R_{6,8} > 0.99$$

...



Resonances, slab mode reasoning



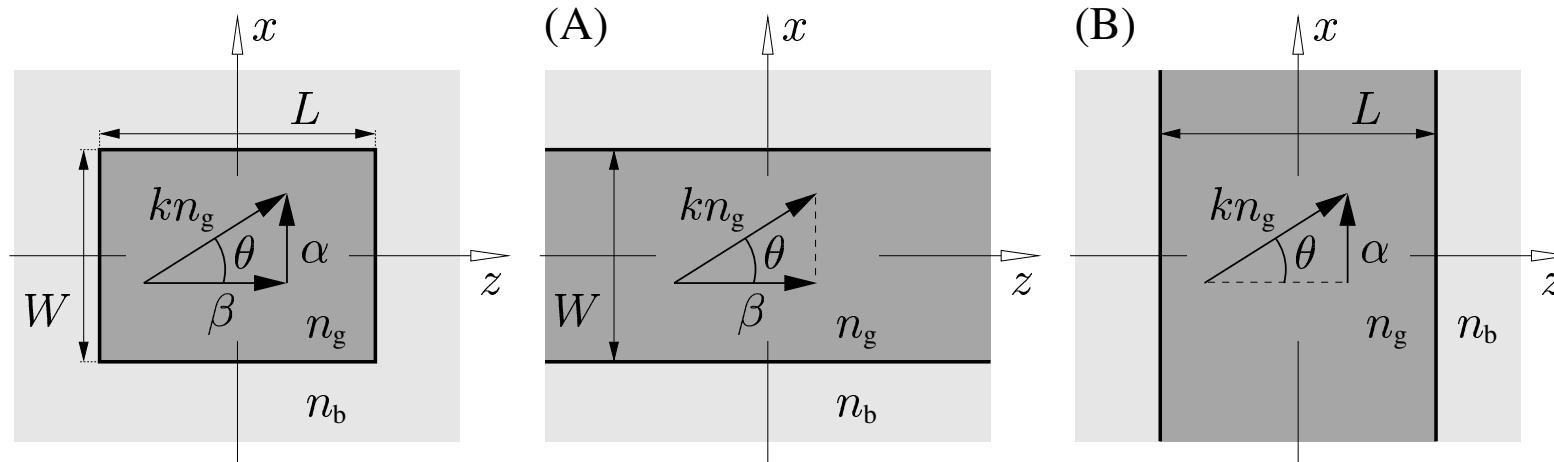
Field in $-W/2 < x < W/2$, $-L/2 < z < L/2$:

$$(A) \quad E_y(x, z) = E_0 \phi(x) (e^{-i\beta z} + b e^{i\beta z}), \quad \phi(x) = e^{-i\alpha x} \pm e^{i\alpha x},$$

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Resonances, slab mode reasoning



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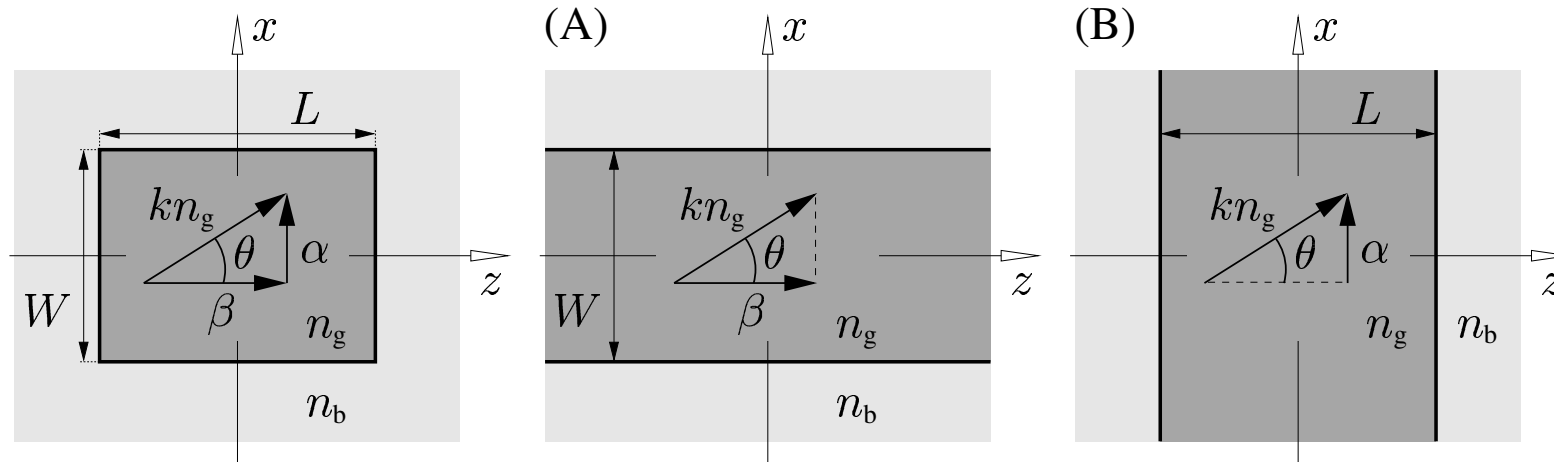
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↪ Resonant configurations W, L for given $\lambda = 2\pi/k$, n_g, n_b :

The slab waveguide of thickness W supports a mode with angle θ , while the slab of thickness L guides a field with angle $\pi/2 - \theta$.

Resonances, slab mode reasoning



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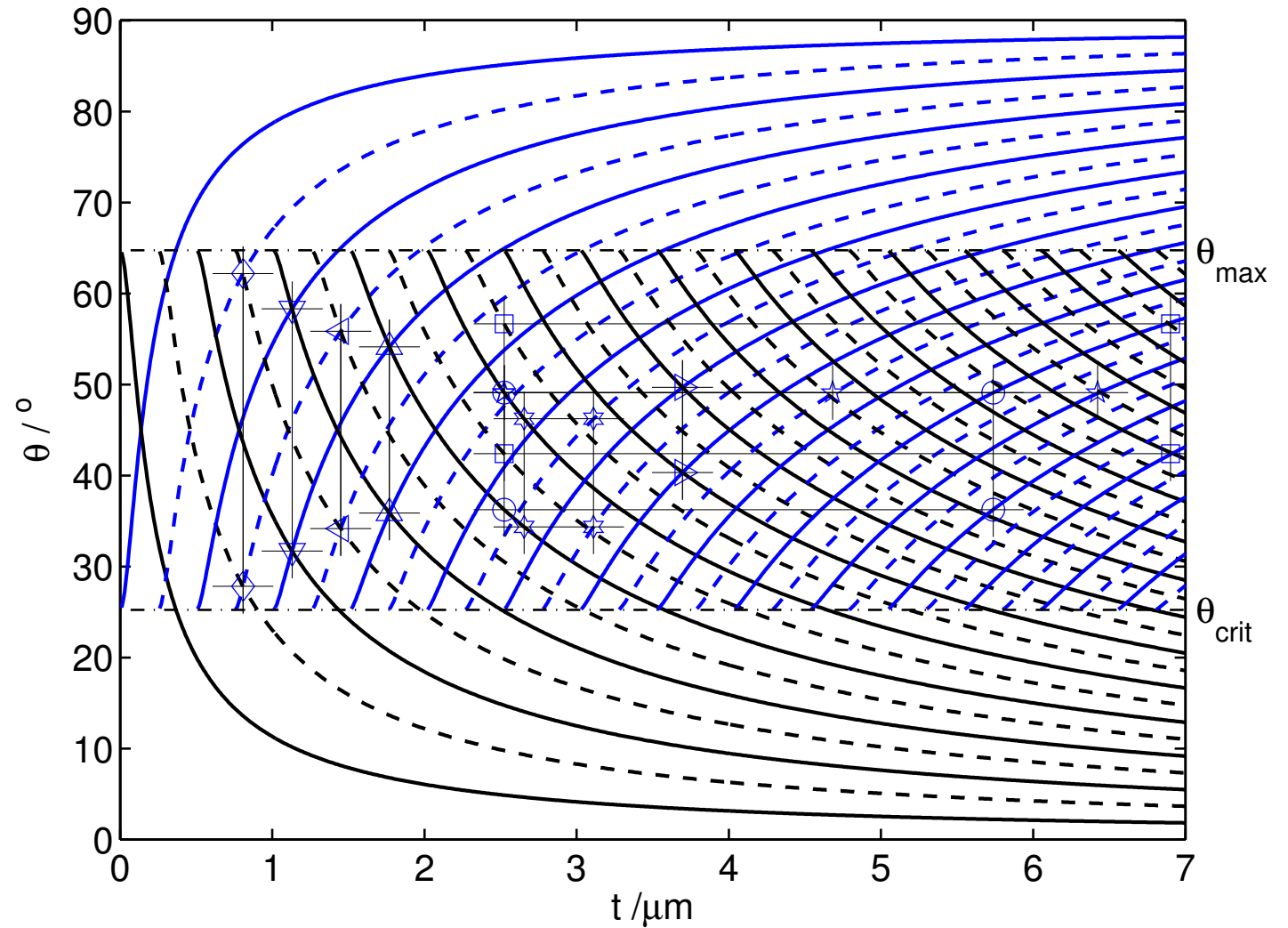
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Bimodal resonance: Two pairs of modes with proper symmetry (\leftrightarrow facet edges) satisfy the conditions simultaneously.

Looking up resonant configurations

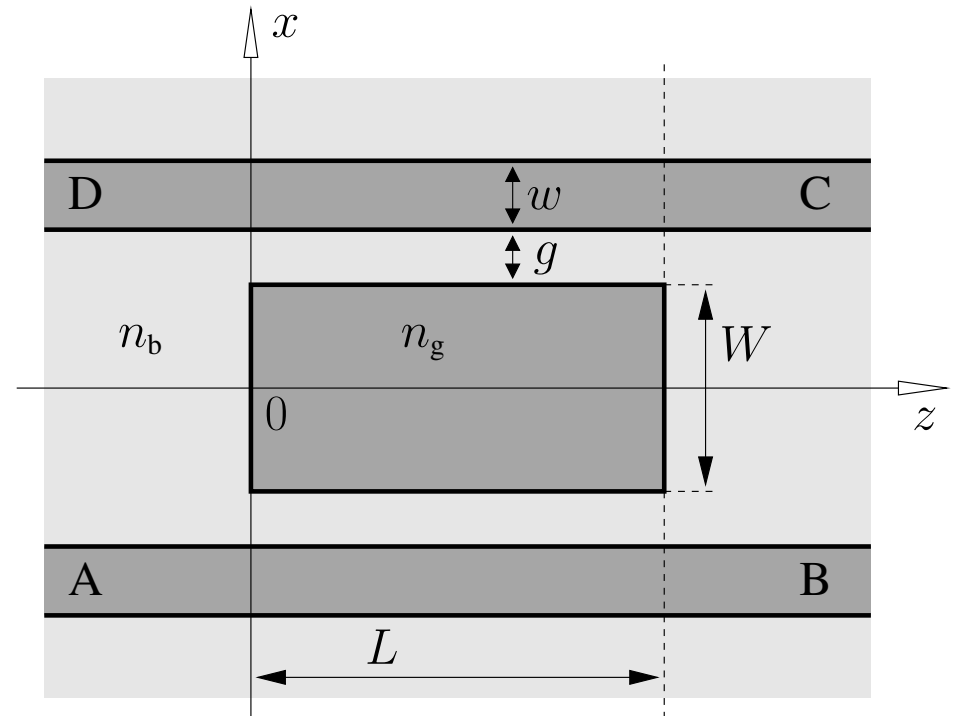
... in a plot
mode angle θ
vs. slab thickness t :



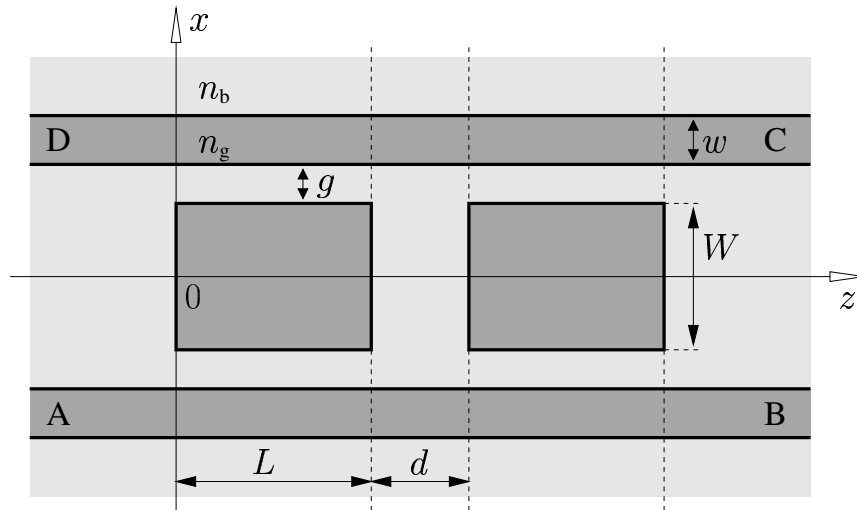
...

↑ Slab mode resonances

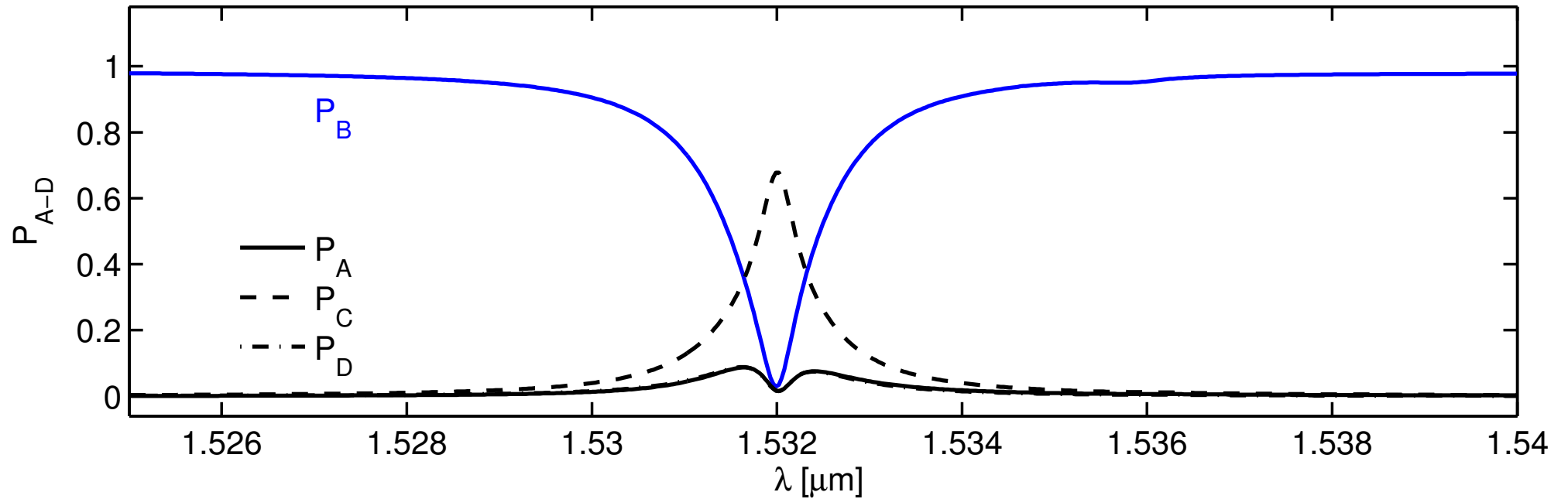
↓ Extensions



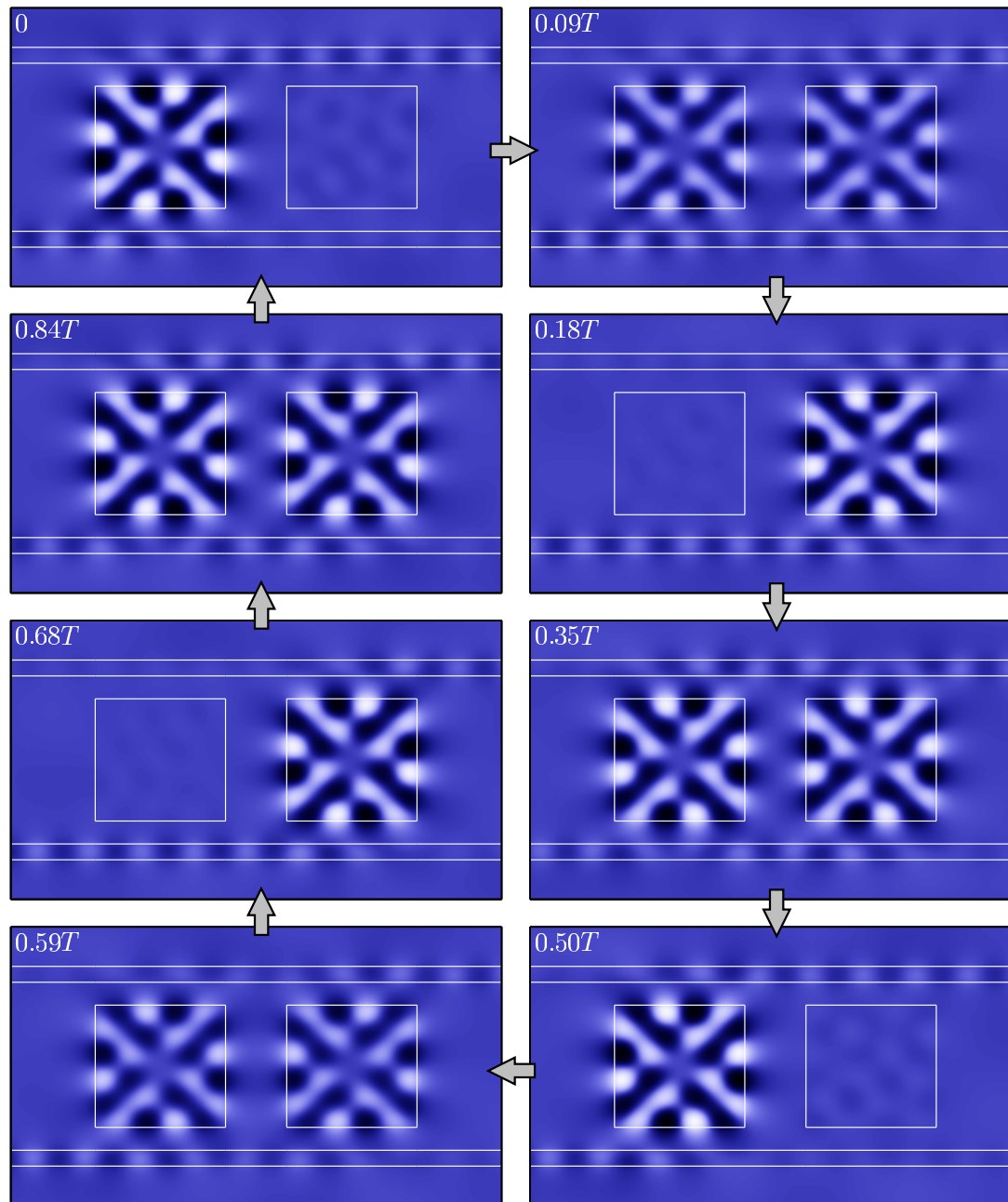
Filter device based on rectangular cavities



$w = 0.20 \mu\text{m}$, $g = 0.29 \mu\text{m}$,
 $W = L = 1.54 \mu\text{m}$, $d = 0.72 \mu\text{m}$,
 $n_b = 1.0$, $n_g = 3.2$; 2D, TE.



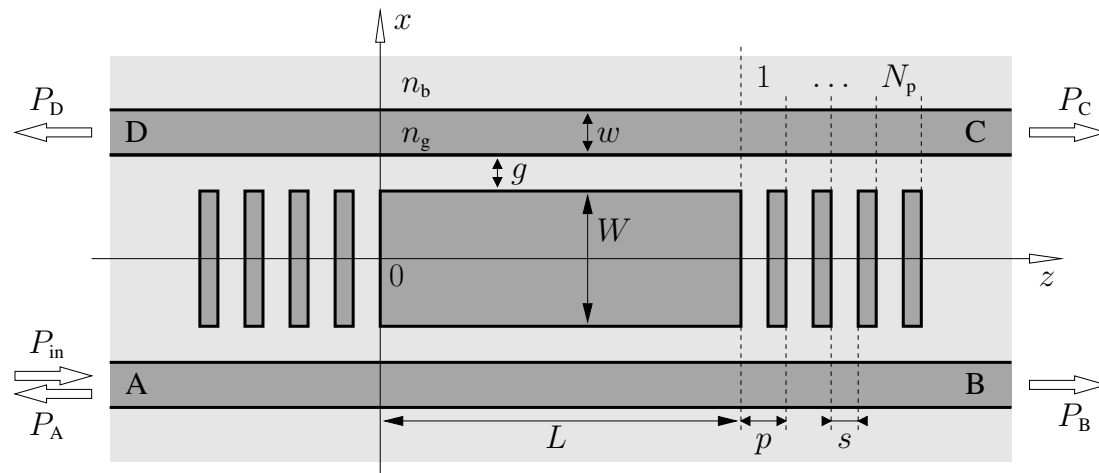
Filter: Resonant field pattern



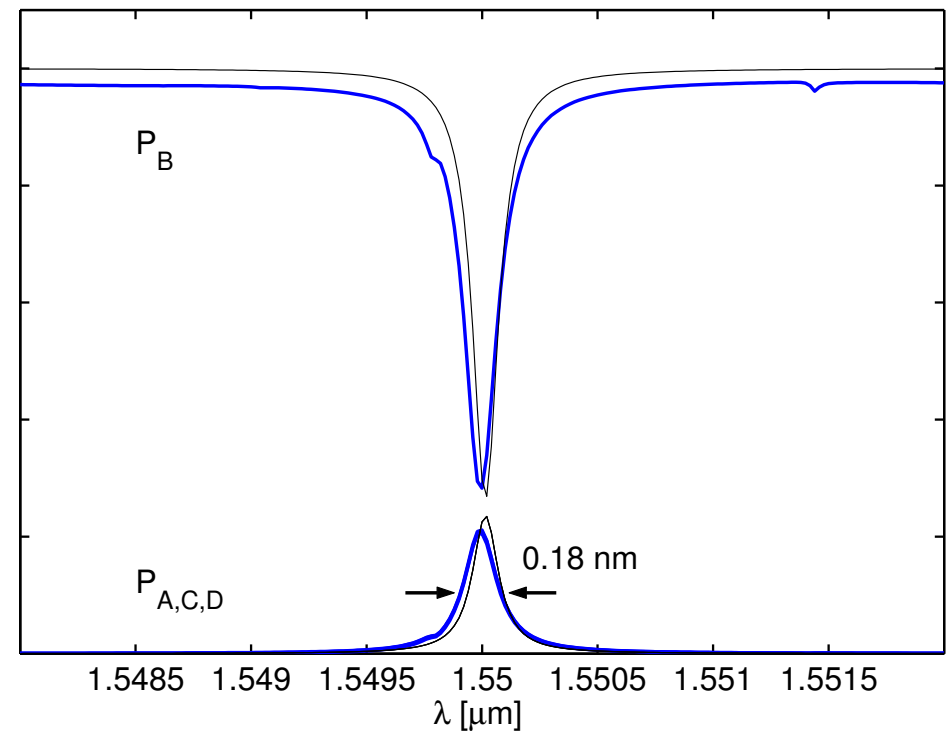
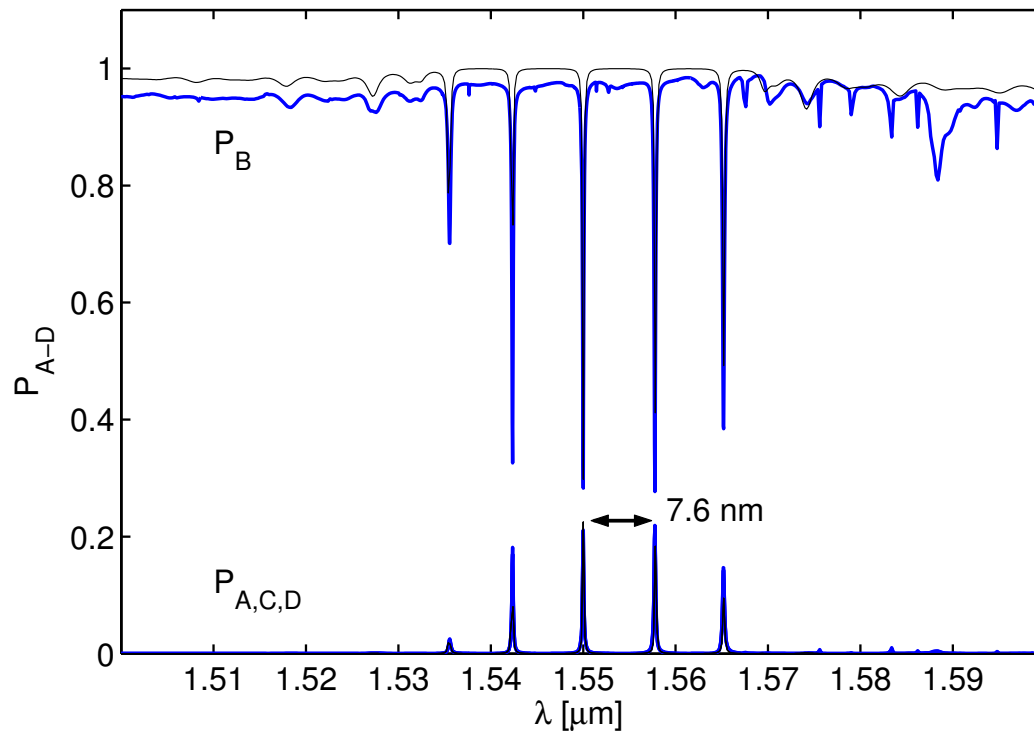
$\lambda = 1.532 \mu\text{m},$
 $T = 5.11 \text{ fs}.$

$P_D = 0.02, P_C = 0.68,$
 $P_A = 0.02, P_B = 0.03.$

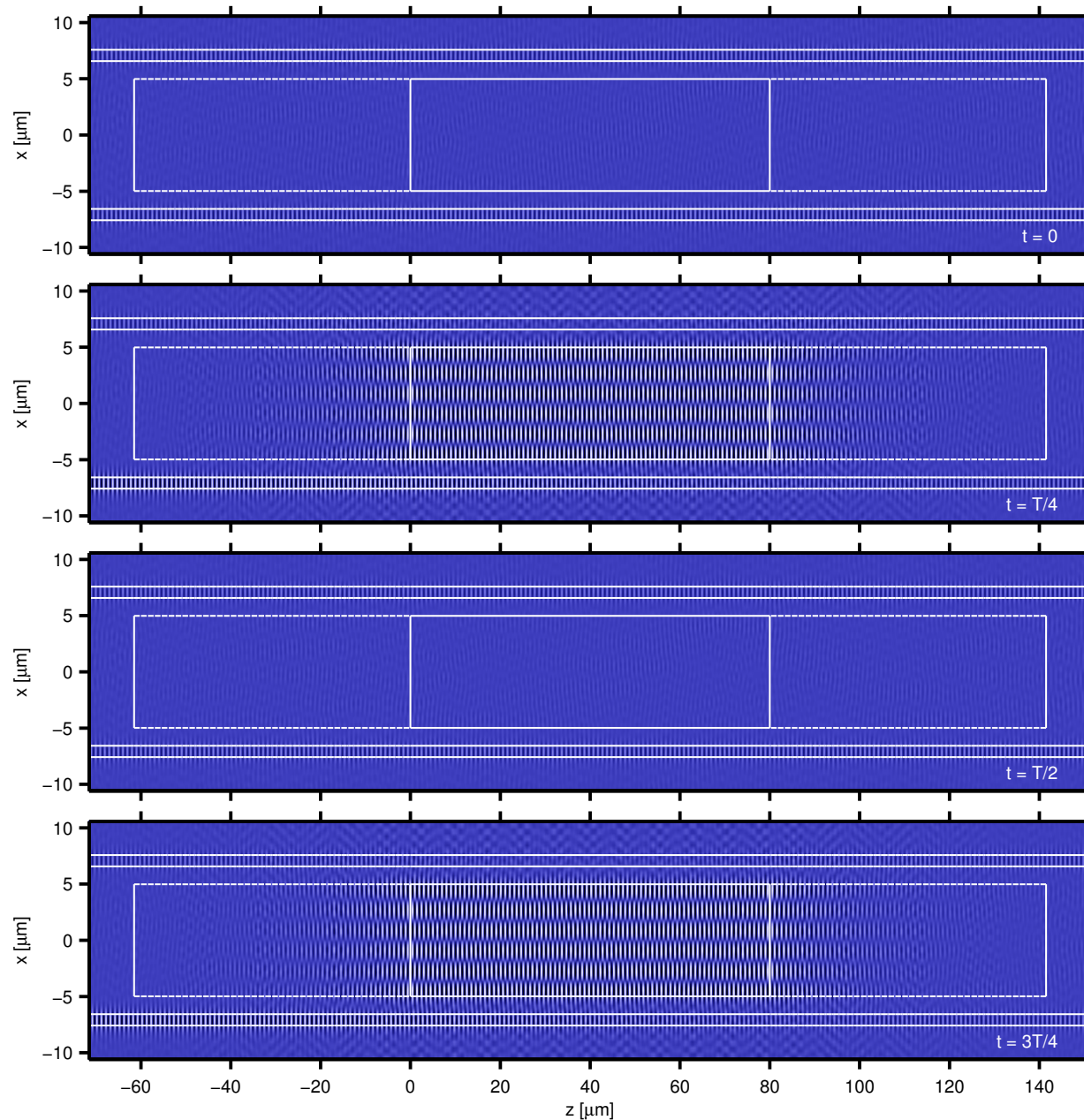
Grating assisted resonator



$w = 1.0 \mu\text{m}$, $g = 1.6 \mu\text{m}$,
 $W = 9.955 \mu\text{m}$, $L = 79.985 \mu\text{m}$,
 $p = 1.538 \mu\text{m}$, $s = 0.281 \mu\text{m}$, $N_p = 40$,
 $n_b = 1.45$, $n_g = 1.60$; 2D, TE.



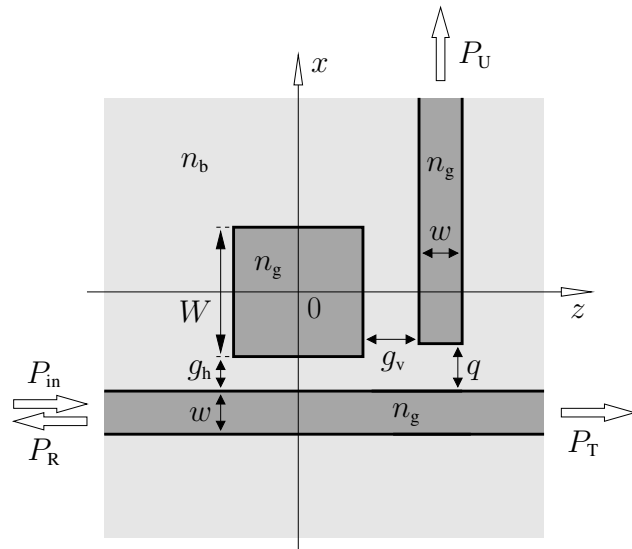
Grating assisted resonator: Resonant field pattern



$$\lambda = 1.55 \mu\text{m},$$
$$T = 5.17 \text{ fs}.$$

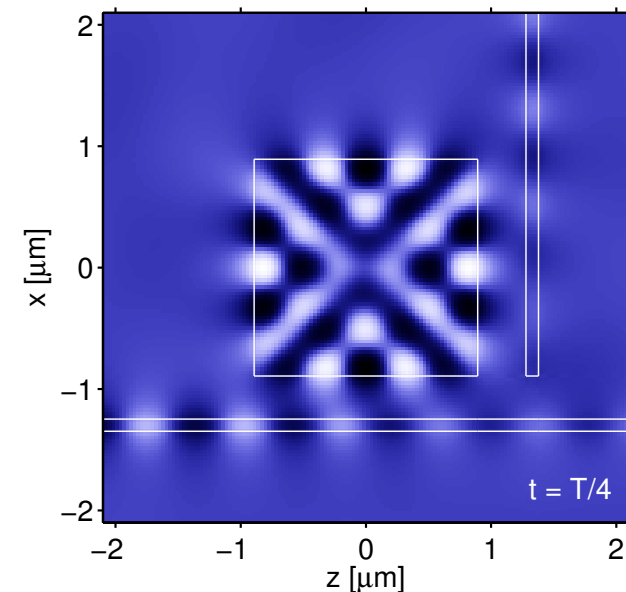
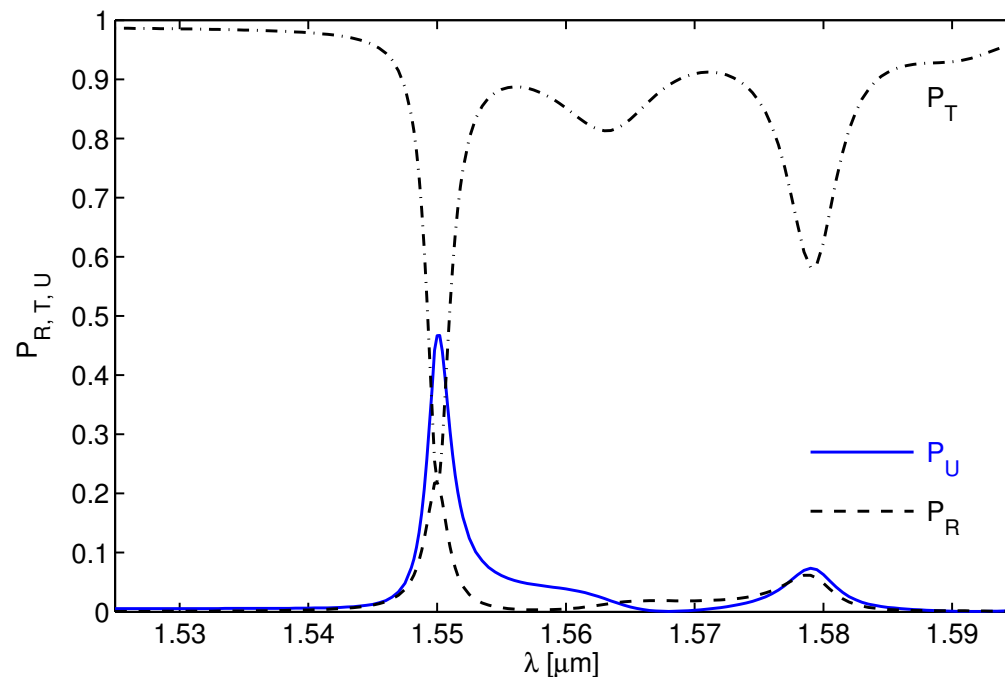
$$P_D = 0.21, P_C = 0.21,$$
$$P_A = 0.21, P_B = 0.28.$$

Resonator with perpendicular ports



$W = 1.786 \mu\text{m}$, $w = 1.0 \mu\text{m}$,
 $g_h = q = 0.355 \mu\text{m}$, $g_v = 0.385 \mu\text{m}$,
 $n_b = 1.0$, $n_g = 3.4$; 2D, TE.

$\lambda = 1.55 \mu\text{m}$: $P_R = 0.22$, $P_T = 0.22$, $P_U = 0.46$.

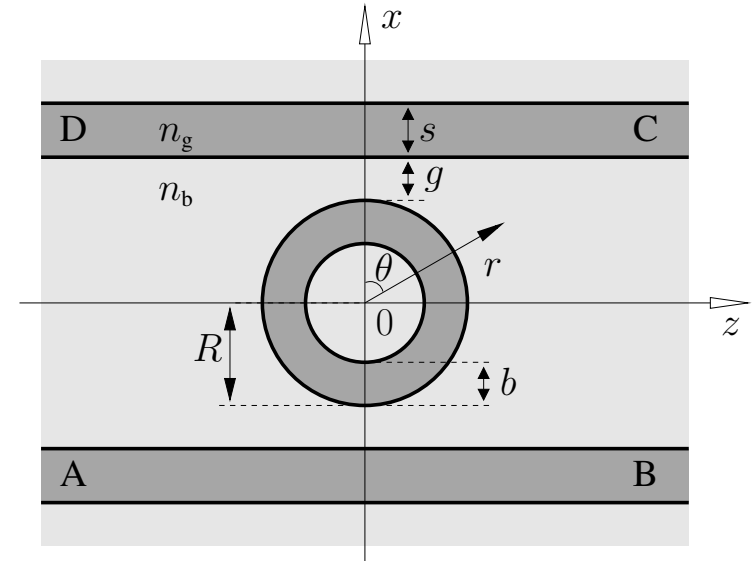


Concluding remarks

Analytical approaches to optical microresonators:

Circular traveling wave resonators

- Alternative viewpoint:
Time-domain gallery modes

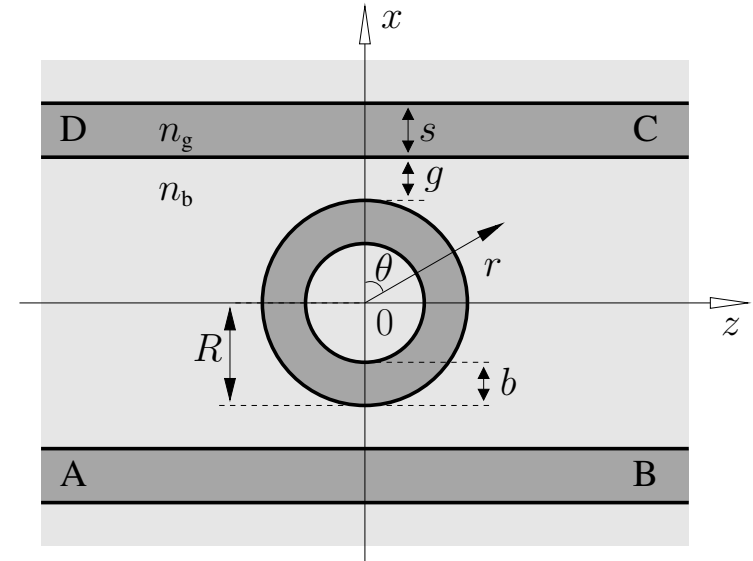


Concluding remarks

Analytical approaches to optical microresonators:

Circular traveling wave resonators

- Alternative viewpoint:
Time-domain gallery modes
- Extension to 3D:
Straightforward, if ...

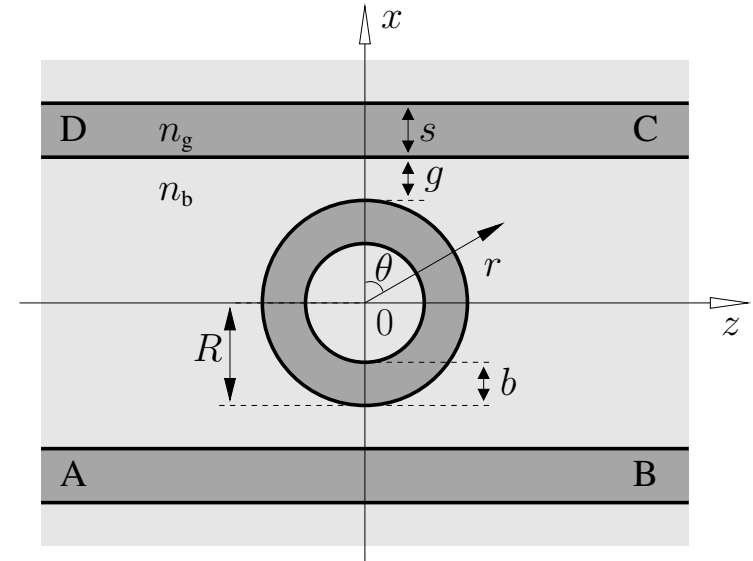


Concluding remarks

Analytical approaches to optical microresonators:

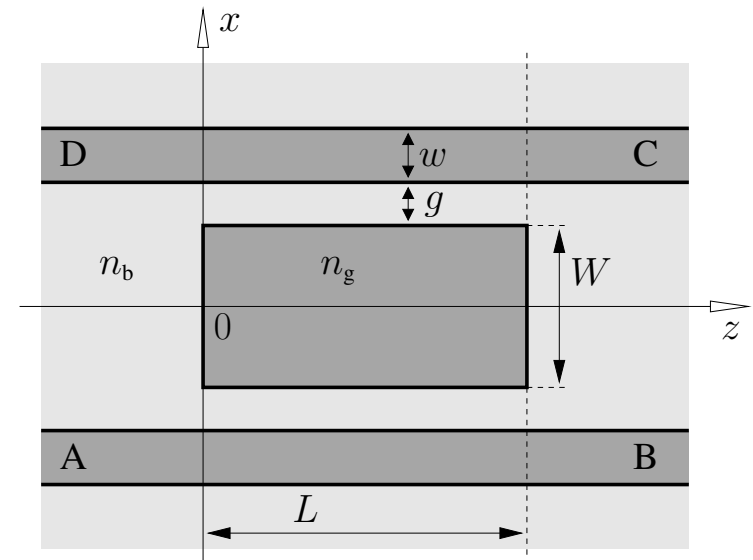
Circular traveling wave resonators

- Alternative viewpoint:
Time-domain gallery modes
- Extension to 3D:
Straightforward, if ...



Rectangular standing wave resonators

- Speculative.
So far 2D models exist.

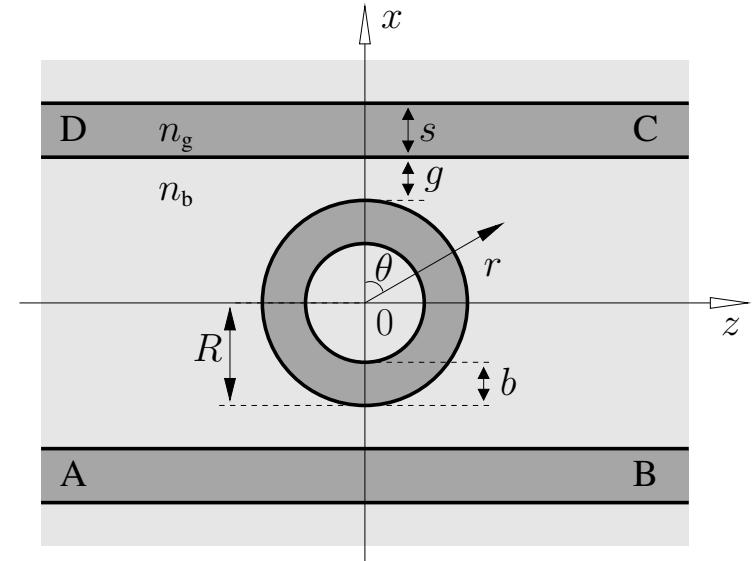


Concluding remarks

Analytical approaches to optical microresonators:

Circular traveling wave resonators

- Alternative viewpoint:
Time-domain gallery modes
- Extension to 3D:
Straightforward, if ...



Rectangular standing wave resonators

- Speculative.
So far 2D models exist.
- Standing wave phenomena
... in small rings ?

